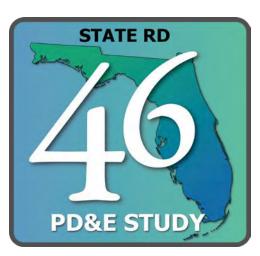
LOCATION HYDRAULICS REPORT



SR 46 PD&E Study

from SR 415 to CR 426

Seminole County, Florida

FPN 240216-4-28-01

April 2014







PROFESSIONAL ENGINEER CERTIFICATE

I hereby certify that I am a registered professional engineer in the State of Florida practicing with URS Corporation, a corporation, authorized to operate as an engineering business, Certificate of Authorization No. 000002, by the State of Florida, Department of Business and Professional Regulation, Board of Professional Engineers, and that I have reviewed or approved the evaluation, findings, opinions, conclusions, or technical advice hereby reported for:

| Project: | SR 46 PD&E Study from SR 415 to CR 426 | | |
|-----------|--|--|--|
| EDNI- | 240216 4 20 04 | | |
| FPN: | 240216-4-28-01 | | |
| Location: | Seminole County, Florida | | |
| Client: | Seminole County and FDOT – District Five | | |

This Location Hydraulics Report includes a summary of data collection efforts and conceptual drainage analyses prepared for conceptual analyses for the SR 46 PD&E Study from SR 415 to CR 426. I acknowledge that the procedures and references used to develop the results contained in this report are standard to the professional practice of civil engineering as applied through design standards and criteria set forth by the federal, state, and local regulatory agencies as well as professional judgment and experience.

| Name: | Danh Lee, P.E. | | |
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APPENDICES

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1.0 INTRODUCTION

Seminole County and the Florida Department of Transportation (FDOT) District 5 have initiated a Project Development and Environment (PD&E) Study to widen State Road 46 (SR 46) from a two lane rural roadway to a four lane divided facility from East of SR 415 to CR 426 in Seminole County, Florida. The purpose of the proposed improvements is to improve the mobility in the SR 46 corridor to accommodate future projected traffic demand in the Design Year (2035) safely and efficiently. Exhibit 1 shows the project location and study limits.



Exhibit 1 – Project Location Map

2.0 PURPOSE

According to the executive order 11988 "Floodplain Management", USDOT Order 5650.2 "Floodplain Management and Protection" and Federal Aid Policy Guide 23 CFR 650A, floodplains and floodways protection is required. The intent of these regulations is to avoid or minimize highway encroachments within the 100-year (base) floodplains where practicable and to avoid supporting land use development, which is incompatible with floodplain values. Where encroachment is unavoidable, the regulations require the FDOT to take appropriate measures to minimize impacts.

This Location Hydraulics Report has been prepared for Seminole County and the FDOT District 5 to assess potential impacts as a result of widening SR 46 on base floodplains and regulatory floodways if any to comply with the above regulations and 23 CFR 771.

This report is consistent with the FDOT guideline and procedure identified in the FDOT Drainage Manual, Storm Water Management Facility Handbook, Drainage Handbook of Hydrology, Storm Drains, and Cross Drains and FDOT PD&E Manual, and also the St. Johns River Water Management District (SJRWMD) Manual.

Information concerning floodplains, basin delineation, basin area, culvert data and locations used in the preparation of this report were obtained from the following sources:

- Federal Emergency Management Agency (FEMA) Flood Insurance Rate Maps (FIRM) for Seminole County
- United State Geological Survey (USGS) Maps (Osteen and Geneva)
- USDA Natural Resources Conservation Service (NRCS) Soil Survey of Seminole County and Volusia County
- FDOT Construction Plans of SR 46, Financial Project ID No(s). 240163-1-52-01, 240216-2-52-01, 417178-1-52-01, and 7704-105.
- FDOT Construction Plans of SR 415, Financial Project ID No(s). 407355-1-52-0
- FDOT Straight Line Diagram of Road Inventory (Appendix B)
- Centex Homes Construction Plans of Sterling Meadows, SJRWMD Permit No. 4-117-51666-2
- Seminole County GIS Lidar Data, 1 foot contours
- Field investigation

3.0 PROJECT DESCRIPTION

SR 46 is classified as a Rural Principal Arterial within the project limits. The portion of SR 46 included in this Location Hydraulic Report (LHR) has limits from SR 415 to CR 426 in Seminole County, a distance of approximately 7.4 miles. The project limits encompass USGS quad maps T19S-R31E, T20S-R31E, and T20S-R32E (See Exhibit 2A & 2B).

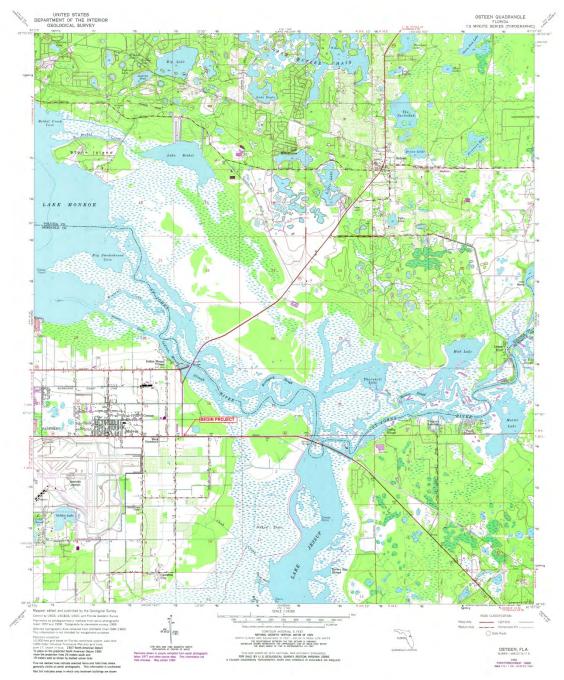


Exhibit 2A – USGS Quad Map Osteen FL 1980

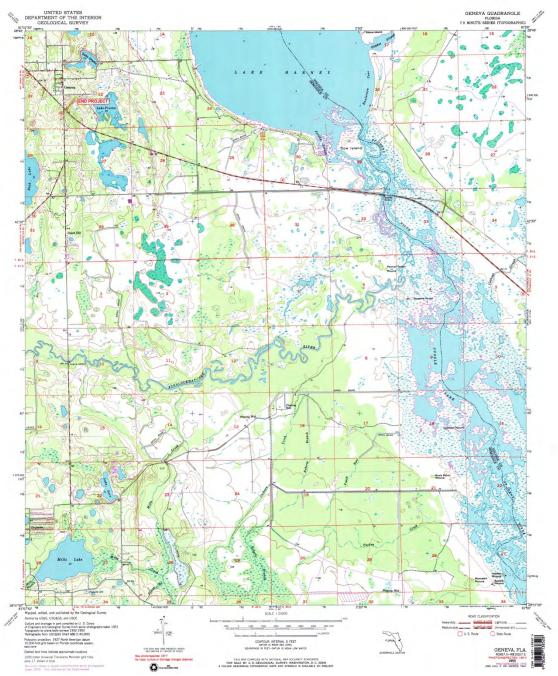


Exhibit 2B – USGS Quad Map Geneva FL 1977

Within the project limits, the existing typical roadway section of SR 46 (See Exhibit 3A) consists of a rural section with two 12-foot lanes and 6-foot (4-foot paved) outside shoulders.

For the purposes of analyzing build alternatives, the project was split into four segments as follows:

• Segment 1 – SR 415 to the west end of the Lake Jesup/St. Johns River Bridge

- Segment 2 The Lake Jesup/St. Johns River Bridge
- Segment 3 The east end of the Lake Jesup/St. Johns River Bridge to Hart Rd
- Segment 4 Hart Road to CR 426

Two typical sections, rural and suburban, were analyzed for the widening of SR 46 between SR 415 and Hart Road and an urban typical section is proposed for the widening of SR 46 from Hart Road to CR 426. For the rural and suburban typical sections, a widen north and a widen south option was explored.

The rural typical section includes two 12-foot lanes in each direction with eightfoot (two-foot paved) inside shoulders and 10-foot (five foot paved) outside shoulders, which serve as undesignated bicycle lanes. A 40-foot median separates the travel lanes. Conveyance swales are provided on each side of the roadway within the 36-foot clear zone. The design speed of the rural typical section is 60 mph and it requires a minimum of 188 feet of right-of-way (See Exhibits 3B and 3C).

The suburban typical section includes two 12-foot lanes in each direction with four-foot inside shoulders and 6.5-foot outside shoulders, which serve as undesignated bicycle lanes. A 30-foot median separates the travel lanes and type E curb and gutter is proposed on both the inside and outside edges of pavement. Within the 30-foot clear zone are a 10-foot asphalt shared-use-path on the north side of the roadway and a five-foot concrete sidewalk on the south side. The design speed of the suburban typical section is 55 mph and it requires a minimum of 148 feet of right-of-way (See Exhibits 3D and 3E).

The urban typical section includes one 12-foot lane and one 11-foot lane in each direction with four-foot outside shoulders, which serve as designated bicycle lanes. A 22-foot median separates the travel lanes with type E curb and gutter proposed on the inside edge of pavement and type F curb and gutter proposed on the outside edge of pavement. Within the 12-foot border width is an eight-foot sidewalk on the north side of the roadway and a six-foot concrete sidewalk on the south side. The design speed of the suburban typical section is 45 mph and it requires a minimum of 100 feet of right-of-way (See Exhibit 3F).

In addition to the three proposed alternative typical sections, there will also be construction of a new bridge, parallel to the existing bridge over Lake Jesup. Two bridge typical sections were developed, one with a shared use path and one without. Both bridge typical sections retain the existing bridge as the future eastbound lanes. The proposed westbound lanes, to be built upon the alignment of the old bridge and causeway that was removed during the construction of the existing bridge, provides two 12-foot lanes, a six-foot inside shoulder and a 10-foot outside shoulder. The typical section without the shared-use path is intended for use with the rural roadway typical section, and maintains the 40-foot median (See Exhibit 3G). The typical section, and maintains a 30-foot median (See Exhibit

3H). The shared use path is barrier-separated from the travel lanes and is 10 feet wide.

The existing and proposed typical sections are shown in Exhibit 3A thru Exhibit 3H.

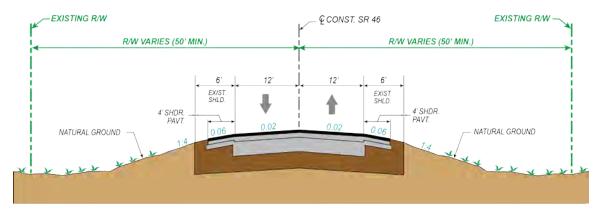


Exhibit 3A - Existing Typical Section

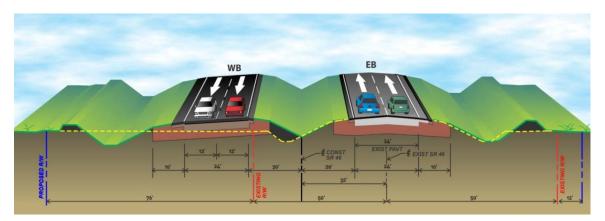


Exhibit 3B-Rural Typical Section-Widen to the North

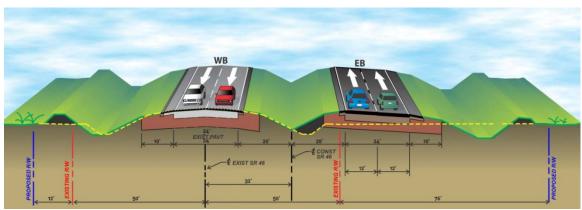


Exhibit 3C-Rural Typical Section-Widen to the South

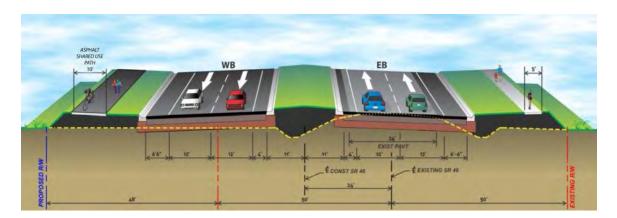


Exhibit 3D-Suburban Typical Section-Widen to the North

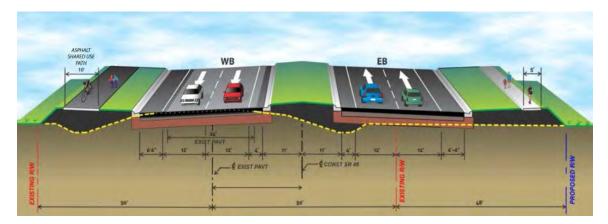


Exhibit 3E-Suburban Typical Section-Widen to the South

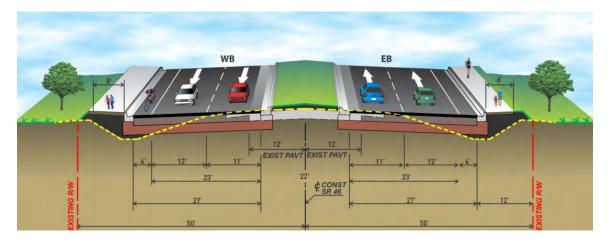


Exhibit 3F-Urban Typical Section-Centered Widening

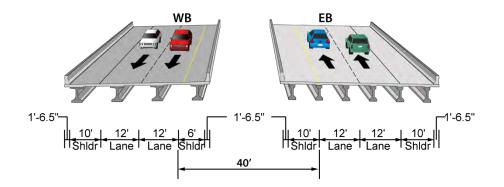


Exhibit 3G-Bridge Typical Section without Shared Use Path

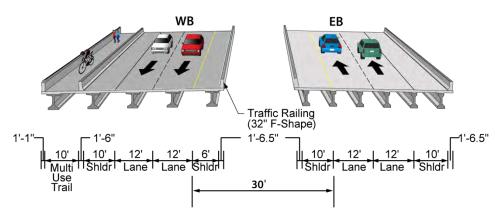


Exhibit 3H-Bridge Typical Section with Shared Use Path

Once the typical sections were identified, typical section alternatives were selected by segment.

Segment 1

In order to minimize impacts to existing conservation easements both north and south of SR 46 within this segment, only the suburban typical sections will be considered for Segment 1. Alternative 1 uses the Suburban – Widen North typical section and Alternative 2 uses the Suburban – Widen South typical section.

Segment 2

Segment 2 is the bridge typical section and is dependent on the typical section selected for Segment 3 as indicated above. The Bridge with Shared Use Path typical section is compatible with the suburban typical section and the Bridge without Shared Use Path is compatible with the rural typical section.

Segment 3

Both the rural and suburban typical sections are appropriate for use within Segment 3. Both typical sections will be evaluated and vary between north and south widening in order to minimize impacts to both the natural, physical and social environments. These combinations of north and south widening are known as the Rural Best Fit and Suburban Best Fit alternatives.

Segment 4

Only the urban typical section is being analyzed for Segment 4 in order to minimize right-of-way acquisition to the commercial land uses in the downtown Geneva area.

Full Build Alternatives can be developed from the alternatives listed for each segment. The bridge with the shared use path is compatible with the Suburban Best Fit Alternative, and the bridge without the shared use path is compatible with the Rural Best Fit Alternative. The Segment 1 typical section alternatives are interchangeable and the Segment 4 typical section alternative works with either the Suburban or Rural Best Fit alternatives. Exhibit 4 lists the potential Build Alternatives and associated pond right-of-way acreage for the widening of SR 46.

| Build Alternative | Segment 1 | Segment 2 | Segment 3 | Segment 4 | Required Pond R/W (ac) |
|----------------------|-------------------|------------------------|----------------------|-----------|------------------------------|
| 1 | Suburban North | Bridge with Path | Suburban Best Fit | Urban | 65.7 |
| 2 | Suburban South | Bridge with Path | Suburban Best Fit | Urban | 65.7 |
| 3 | Suburban North | Bridge without Path | Rural Best Fit | Urban | 59.0 |
| 4 | Suburban South | Bridge without Path | Rural Best Fit | Urban | 59.0 |

Exhibit 4 – Build Alternatives Table

4.0 EXISTING DRAINAGE CHARACTERISTICS

SR 46 is located within the jurisdiction of the SJRWMD. According to the USGS quadrangle maps, the approximate ground surface elevation within the project limits range from as low as approximately +5 feet to high as approximately +75 feet. The elevations are based on 1929 National Geodetic Vertical Datum (NGVD). The project limits lie within the Middle St. Johns River Basin of which Lake Jesup is a tributary. The Middle St. Johns River Basin is considered an open basin that discharges to the St. Johns River, which is not considered an Outstanding Florida Waters (OFW). However, the Florida Department of Environmental Protection (FDEP) has adopted Total Maximum Daily Loads (TMDL) for both nitrogen and phosphorus for any basin discharging to the St. Johns River above Lake Monroe, Lake Jesup near St. Johns River, and the St. Johns River above Lake Jesup. Also, 100-year floodplains are found within the project limits with the majority being located around the bridge over Lake Jesup.

In general, stormwater discharged from SR 46 is not treated within the project limits. The existing typical section of SR 46 is crowned and the travel lanes and outside shoulders slope to the outside into existing roadside ditches. The roadside ditches then convey the stormwater runoff to several existing cross drains. The cross drains then conveys the runoff into various wetland areas found within the project limits, which ultimately discharge to the St. Johns River.

The only area currently treated is within the limits of the bridge replacement project, over Lake Jesup, which was constructed in 2009. The new bridge and approaches are being treated by existing stormwater treatment wet detention pond(s) 1 and 2. The ponds are located west and east of the bridge, respectively. Stormwater runoff from the high point of the bridge to the west end of the project is collected and conveyed to existing Pond 1 by a series of shoulder gutter inlets and ditch bottom inlets. Stormwater runoff from the high point of the bridge to the bridge to the bridge to the east end of the project is collected and conveyed to existing Pond 2 by a series of bridge scuppers, shoulder gutter inlets, and ditch bottom inlets. The bridge scuppers are connected to fiber reinforced concrete pipes that hang beneath the south side of the bridge.

5.0 PROPOSED DRAINAGE DESIGN

The same four design segments were used to analyze the proposed drainage design as follows:

- Segment 1 SR 415 to the west end of the Lake Jesup/St. Johns River Bridge
- Segment 2 The Lake Jesup/St. Johns River Bridge
- Segment 3 The east end of the Lake Jesup/St. Johns River Bridge to Hart Rd
- Segment 4 Hart Road to CR 426

Segment 1

In order to minimize impacts to existing conservation easements both north and south of SR 46 within this segment, only the suburban typical sections will be considered for Segment 1. The stormsewer system will be designed to collect stormwater runoff from the new lanes by a series of curb and gutter inlets and convey it to proposed Pond A for both the widen north and widen south typical sections. If the widen north alternative is selected, existing Pond 1 will be impacted; therefore, the pond will be modified to accommodate the reduction in treatment volume within this pond. Also, Floodplain Compensation Pond 1 is proposed within this segment to compensate for 100-year floodplain impacts. The ponds have been designed to provide water quality, quantity and compensation for any loss of floodplain volumes.

Segment 2

Segment 2 is the bridge typical section and is dependent on the typical section selected for Segment 3. Both existing Pond 1 and Pond 2 will be modified to provide additional treatment and attenuation of stormwater runoff from the new parallel bridge. The basin limits for existing Pond 1 and Pond 2 will remain the same as delineated in the bridge replacement project. The Pond 1 stormsewer system will be designed to collect stormwater runoff from Station 75+40 to the high point of the new and existing bridge by a series of curb and gutter inlets. The Pond 2 stormsewer system will be designed to collect stormwater to collect stormwater runoff from the high point of the new and existing bridge to Station 158+15 by a series of bridge scuppers and curb and gutter inlets, if a suburban typical section is selected for Segment 3. Shoulder gutter inlets and ditch bottom inlets will replace the curb and gutter inlets, if a rural typical section is selected for Segment 3. Also, 100-year floodplain impacts within this segment will be compensated by Floodplain Compensation Pond 1, mentioned previously, and Floodplain Compensation Pond 2, which will be mentioned in Segment 3.

Segment 3

Both the suburban and rural typical sections are appropriate for use within Segment 3. If the suburban typical section is selected, stormwater runoff will be treated and attenuated by modified existing Pond 2 and proposed Pond(s) B through G. The stormsewer system will be designed to collect stormwater runoff from the new lanes by a series of curb and gutter inlets and convey it to the proposed Ponds within this segment. If a rural typical section is selected, roadside treatment swales will replace proposed Pond(s) E through G. Also, the curb and gutter inlets proposed for the stormsewer system will be replaced with ditch bottom inlets for conveyance. In addition, 100-year floodplain impacts within this segment will be compensated by Floodplain Compensation Pond 2 and proposed ditches.

Segment 4

Only the urban typical section is being analyzed for Segment 4 in order to minimize right-of-way acquisition to the commercial land uses in the downtown Geneva area. The stormsewer system will be designed to collect stormwater runoff from the new lanes by a series of curb and gutter inlets and convey it to proposed Pond H for this segment.

6.0 CROSS DRAINS

There are a total of 9 cross drains within the limits of this project ranging from 18" RCP to double 8' X 3' CBC (See Exhibit 5). All the existing cross drains have been numbered and are shown on the Pond Alternatives Location Plans (See Appendix A). There is also one existing bridge over Lake Jesup that was recently constructed in 2009. As part of the proposed roadway improvements, a parallel bridge will be constructed on the north side of the existing bridge.

According to the FDOT Maintenance Department, all of the cross drains are in good physical condition; however, there are two locations where there has been record of flooding problems on the downstream side of the cross drains. The first location being in the vicinity of CD-4, north of SR 46 and east of Mullet Lake Park Road. The FDOT Maintenance Department believes that the flooding problem exists in this area due to the lack of positive drainage grading located through downstream private properties and the ultimate outfall of the conveyance system leading into the St. Johns River. The second location being in the vicinity of CD-5, north of SR 46 and east of Mockingbird Lane. The FDOT Maintenance Department believes that the flooding problem exists in this area due to the lack of positive drainage grading located within the downstream private property into which the cross drain discharges before entering the wetland located within this property. The FDOT Maintenance Department does not believe that the existing cross drains are undersized in these locations, but the problems exist due to the lack of positive drainage grading within downstream private properties and that the problems cannot be fixed without some type of drainage easement. (Appendix F shows records of telephone conversations). The fact that the flooding occurs on the downstream side of the existing cross drains would indicate that the size of the existing cross drains are most likely not the cause of the flooding.

Field investigation was also conducted for all the existing cross drains within the project limits. Field inspection revealed a discrepancy with the FDOT Straight Line Diagram of Road Inventory for CD-4. The inventory shows this cross drain as a double 8' X 2' CBC, but field measurements indicate this cross drain is actually a double 8' X 3' CBC (Appendix C show photos of all cross drains). Several of the cross drains contain PVC liners due to minor leaking at the joints according to the FDOT Maintenance Department. The FDOT Maintenance Department also stated that replacement of the existing cross drains should be examined to meet the design service life projected within this PD&E Study.

West of the St. Johns River Bridge, in Segment 1, there is only one cross drain (CD-1) which will be eliminated once the proposed improvements are complete at the intersection of SR 415 and SR 46 under the FDOT FPID 240216-2-52-01 project.

East of the St. Johns River Bridge, in Segment 3, the existing cross drains (CD-2 thru CD-8) were analyzed based on the worst case scenario only, which is the Rural Best Fit Option. The Rural Best Fit Option will require a greater extension length of the cross drains as compared to the Suburban Best Fit Option. The rural typical section will require the proposed length of the cross drains to be approximately 170 feet in length and will also result in a lower outside edge of pavement elevation due to the widening of SR 46. As a result, several of the cross drains will need to be upsized to maintain an allowable headwater elevation. The remaining cross drains, in Segment 3, will be replaced in kind to meet the design service life projected within this PD&E Study.

Between Hart Road to CR 426, in Segment 4, there is only one cross drain (CD-9) that was analyzed based on the urban typical section. The urban typical section will require the proposed length of the cross drains to be approximately 104 feet in length and will also result in a lower outside edge of pavement elevation due to the widening of SR 46. As a result, this cross drain will need to be upsized to maintain an allowable headwater elevation.

All proposed cross drains will be sized to ensure an allowable headwater elevation. The allowable headwater elevation was determined from an evaluation of land use upstream of the culvert and the proposed roadway elevation. The following factors were also considered in determining the allowable headwater elevation:

- Non-damaging or permissible upstream flooding elevations (e.g. existing buildings or Flood Insurance Regulations).
- State Regulatory Constraints (e.g. Water Management District).
- No encroachment into the proposed elevation of the outside edge of travel lane.

The cross drains were analyzed using FHWA's HY-8 program and the discharges were calculated using FDOT's velocity method. A summary of existing cross drains are shown in Exhibit 5 and Appendix D shows the cross drain analysis for both existing and proposed structures.

| | SUMMARY OF EXISTING CROSS DRAINS | | | | | |
|------------------|----------------------------------|------------------|-----------|--------------------------------|---------------------------------|----------|
| Structure No. | Station | Туре | Size | Flow Line Left (ft) NAVD | Flow Line Right (ft) NAVD | Comments |
| CD-1 | 9+24 | RCP | 24" | 12.56 | 10.72 | Removed |
| CD-2 | 188+62 | RCP w/ PVC Liner | 24" | 13.70 | 13.00 | |
| CD-3 | 201+61 | RCP w/ PVC Liner | 24" | 14.00 | 13.80 | |
| CD-4 | 226+60 | CBC | (2) 8'x3' | 13.00 | 13.20 | |
| CD-5 | 276+60 | RCP w/ PVC Liner | (2) 24" | 20.20 | 20.40 | |
| CD-6 | 296+64 | RCP w/ PVC Liner | 24" | 20.50 | 20.00 | |
| CD-7 | 310+52 | RCP w/ PVC Liner | 24" | 20.00 | 20.10 | |
| CD-8 | 326+73 | RCP w/ PVC Liner | 24" | 25.10 | 31.60 | |
| CD-9 | 384+60 | RCP w/ PVC Liner | 18" | 58.50 | 58.40 | |

Exhibit 5-Summary of Cross Drains

7.0 LAND USE

Existing land use along the project corridor west of the bridge and north of SR 46, the Bergmann Tract land is zoned vacant (other). West of the bridge and south of SR 46, the land is zoned agricultural, residential, and conservation. Existing land use along the project corridor east of the bridge is primarily residential single family. The parcels owned by the City of Sanford (Site 10) east of the bridge and south of SR 46 are zoned agricultural. Commercial land uses are clustered around the intersections of SR 46 with SR 415 and CR 426. Existing land use is shown on Exhibit 6A. The future land use for the project area is shown on Exhibit 6B. This project is consistent with the future land use identified in the Seminole County Comprehensive Plan.

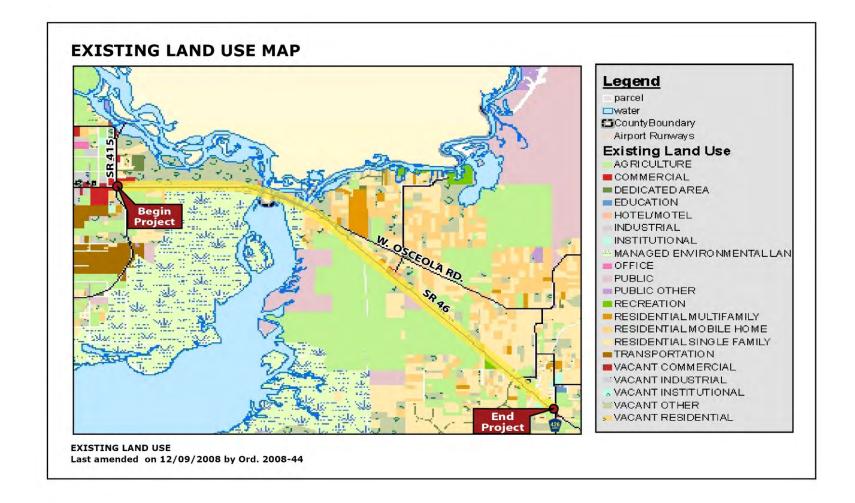


Exhibit 6A – Existing Land Use

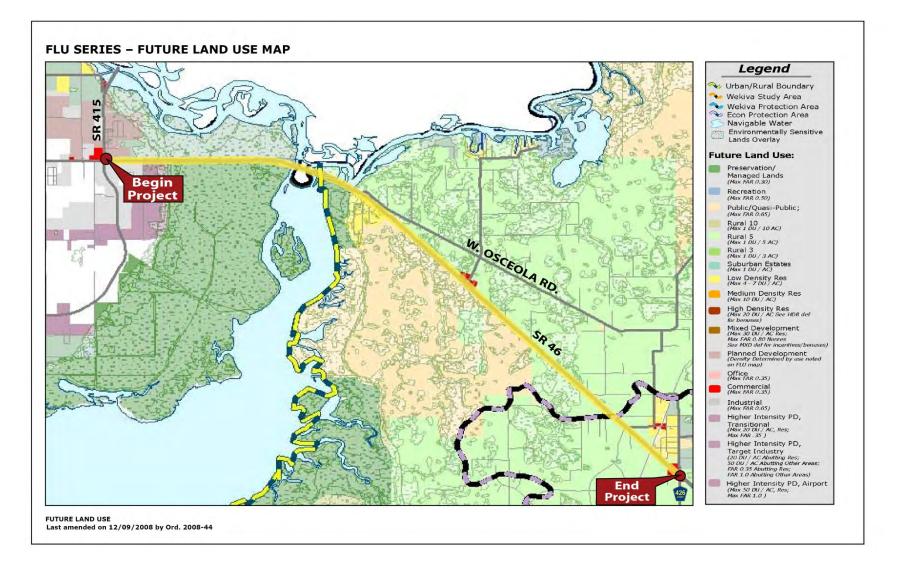


Exhibit 6B – Future Land Use

8.0 SOILS

Geotechnical information reviewed for this report included the 1990 Soil Survey for Seminole County, Florida, as prepared by the U.S. Department of Agriculture Natural Resources Conservation Service. Exhibit 7A lists the soils present in the project area and corresponds to the figures presented in Exhibits 7B and 7C.

| Symbol | Soil Type | |
|--------|---------------------------------------|--|
| 3 | Arents, 0 to 5% slopes | |
| 9 | Basinger and Delray fine sands | |
| 10 | Basinger, Samsula and Hontoon soils, | |
| 10 | depressional | |
| 11 | Basinger and Smyrna fine sands, | |
| 11 | depressional | |
| 12 | Canova and Terra Ceia mucks | |
| 13 | EauGallie and Immokalee fine sands | |
| 15 | Felda and manatee mucky fine sands, | |
| 15 | depressional | |
| 16 | Immokalee sand | |
| 17 | Brighton, Samsula and Sanibel mucks | |
| 18 | Malabar fine sand | |
| 19 | Manatee, Floridana and Holopaw soils, | |
| 19 | frequently flooded | |
| 20 | Myakka and EauGallie fine sands | |
| 21 | Nittaw mucky fine sand, depressional | |
| 22 | Nittaw muck, occasionally flooded | |
| 23 | Nittaw, Okeelanta and Basinger soils, | |
| 23 | frequently flooded | |
| 25 | Pineda fine sand | |
| 26 | Udorthents, excavated | |
| 27 | Pomello fine sand, 0 to 5% slopes | |
| 29 | St. Johns and EauGallie fine sands | |
| 33 | Terra Ceia muck, frequently flooded | |
| 35 | Wabasso fine sand | |
| 99 | Water | |

Exhibit 7A – Existing Soils Table

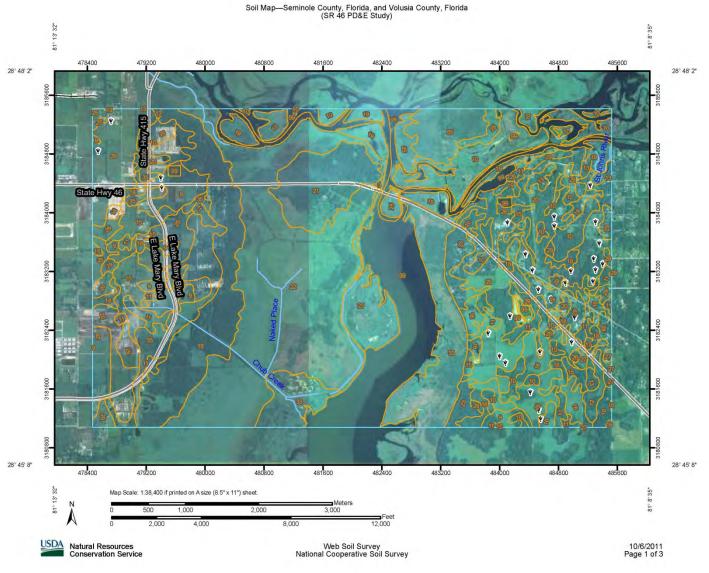


Exhibit 7B-Existing Soils Map (1 of 2)

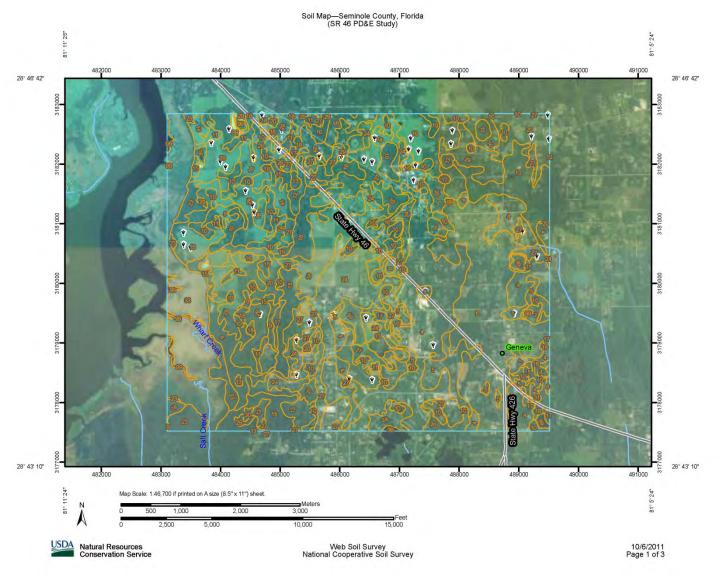


Exhibit 7C-Existing Soils Map (2 of 2)

9.0 FLOODPLAINS ANALYSIS

The original construction of SR 46 crosses several floodplain areas longitudinally. The floodplain locations were determined using the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Maps (FIRM) for Seminole County, Florida and incorporated areas. The following Community-Panel Numbers were used in reference:

- 12117C0090F
- 12117C0095F
- 12177C0185F
- 12117C0205F

FEMA FIRM identified three floodplain zones present within the limits of this project. These zones are defined as follows:

- Zone AE Base flood elevation determined (Elev. 9.0 ft, NAVD)
- Zone AE Base flood elevation determined (Elev. 29.0 ft, NAVD)
- Zone A No base flood elevation determined

Effective dates of these panels are September 28, 2007 (See Exhibit 8).

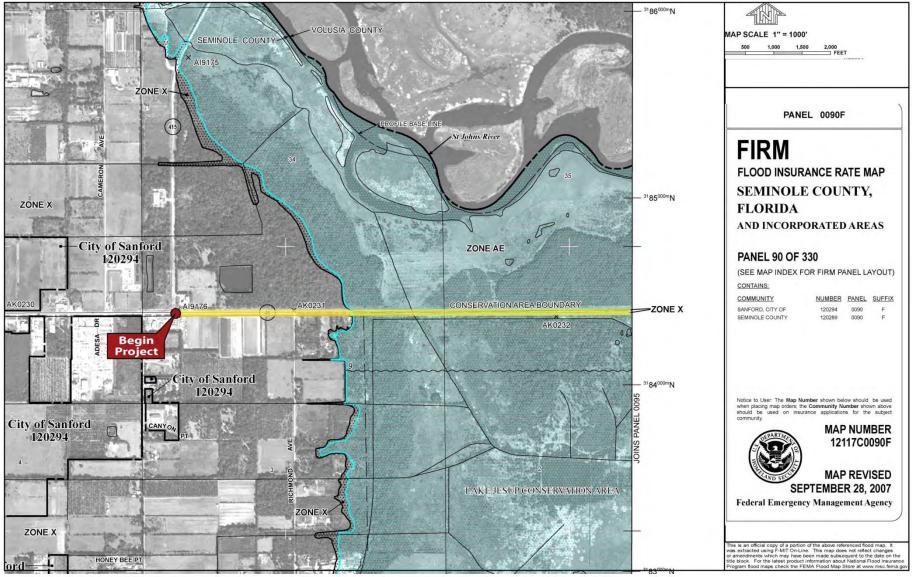


Exhibit 8 – FEMA FIRM Maps (1 of 5)

Floodplain Analysis

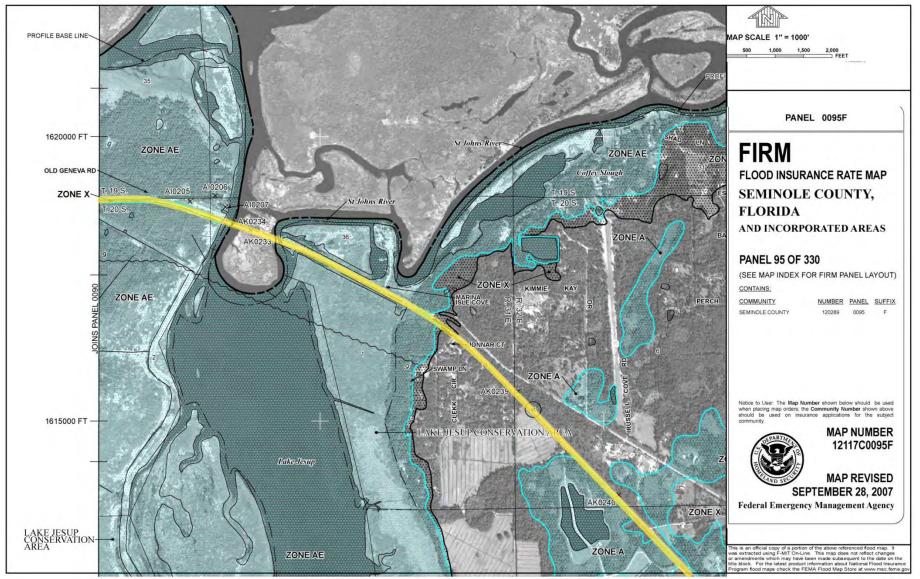


Exhibit 8-FEMA FIRM Maps (2 of 5)

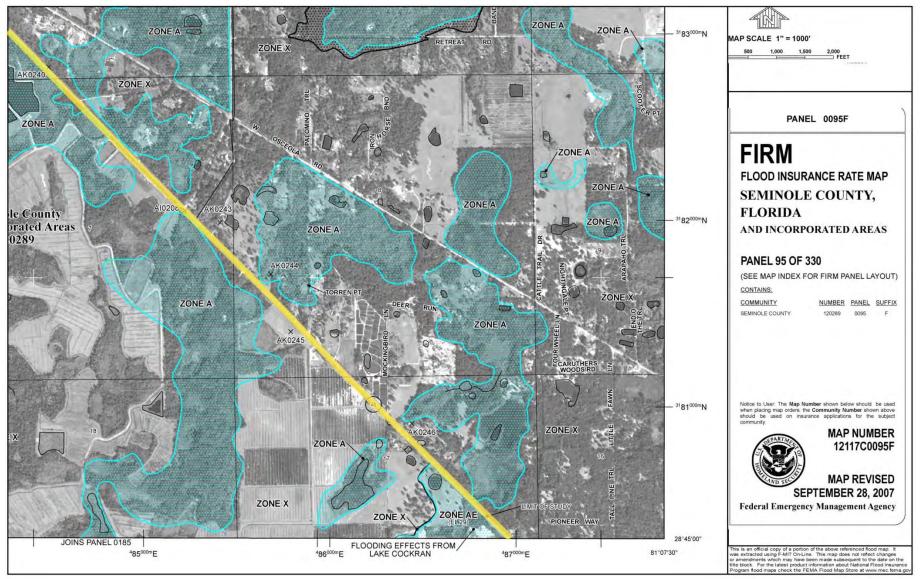


Exhibit 8 – FEMA FIRM Maps (3 of 5)

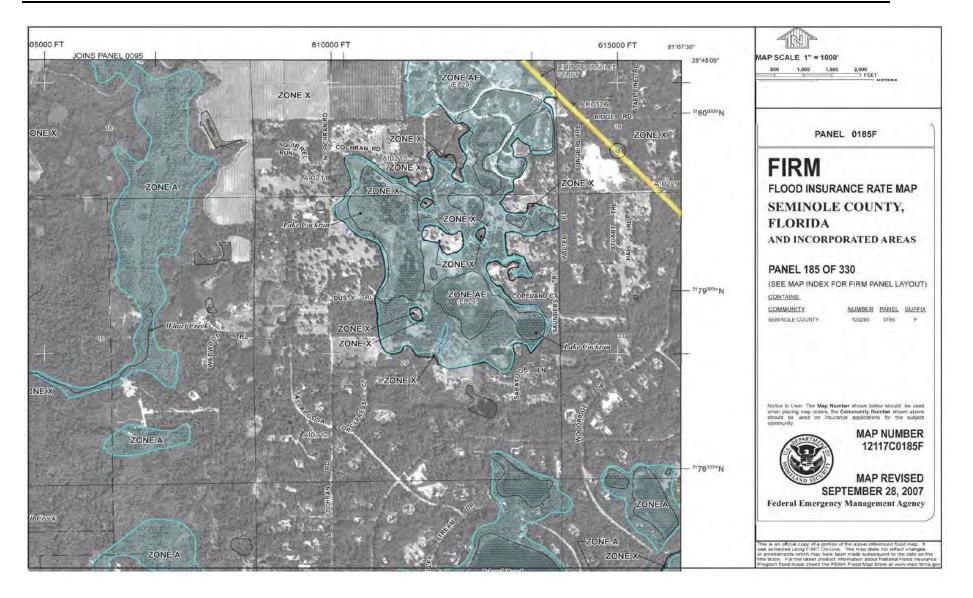


Exhibit 8 – FEMA FIRM Maps (4 of 5)

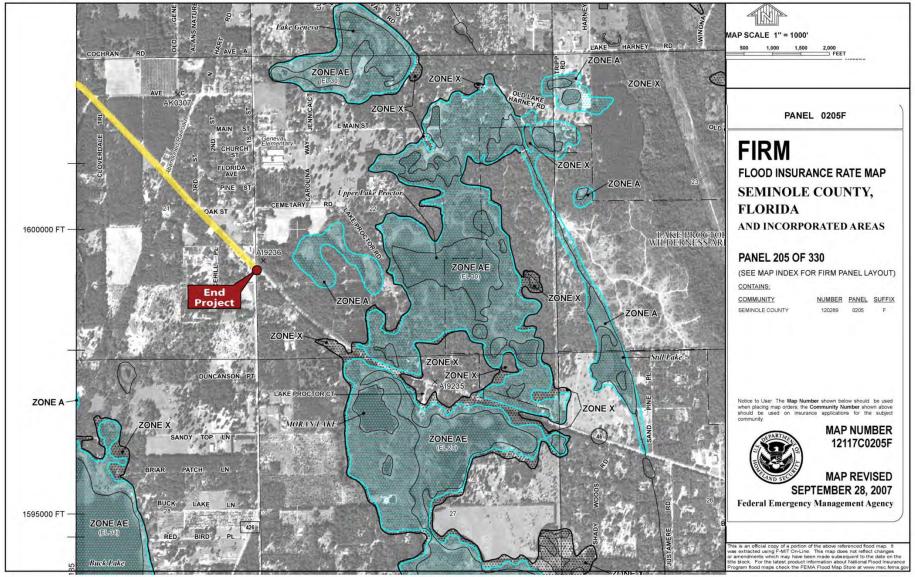


Exhibit 8 – FEMA FIRM Maps (5 of 5)

SR 46 within the limits of this project was constructed on fill and according to available information it appears that the highway is above the 100-year floodplain. An evaluation of 100-year floodplain conditions for this project has been performed to determine the impacts from the embankment required for the proposed widening and proposed ponds. By superimposing the FEMA FIRM maps onto the preferred roadway build alternative, the 100- year floodplain encroachment locations have been determined.

The 100-year floodplain impacts and compensation analysis will be based on the preferred roadway alternative and preferred stormwater treatment ponds. The analysis identified five floodplain boundary encroachments within the project limits. The following provides details regarding floodplain impact locations, conditions, and the method used for floodplain calculations are discussed below.

Floodplain No. 1

According to the FEMA FIRM maps, the limits of Floodplain No. 1 begin at STA 30+32 and ends at STA 143+21. This floodplain is classified as Zone AE, where the base floodplain elevation has been determined to be 9.0 ft NAVD. The roadway embankment required for the proposed widening of SR 46, construction of the new bridge, and proposed ponds will result in impacts to this floodplain. Floodplain impacts will be based on any fill volume above the ESHWT elevation or natural ground, whichever is higher, to the 100-year floodplain elevation.

In order to quantify volumetric floodplain impacts due to the proposed widening of SR 46, preliminary roadway cross sections have been developed using the proposed Suburban Typical Section (widen south and best fit) and Lidar data for Seminole County was used to determine existing ground conditions. In addition, estimated seasonal high water table (ESHWT) elevations from the Bridge Replacement project were used to establish ground water conditions, from STA 77+00 to STA 148+00. The Bridge Replacement project datum is NGVD, therefore a conversion factor of 1 foot has been used to convert from NGVD to NAVD, with NAVD elevations being lower. From STA 22+00 to STA 30+00, a conservative approach will be used to define volumetric floodplain impacts as any fill above the existing ground elevation to the 100-year floodplain elevation. From STA 31+00 to STA 76+00, the ESHWT elevation will be based on the highest existing ground elevation on the north side of SR 46. This approach is conservative and consistent with typical ESHWT elevations that occur within wetlands as well as the preliminary pond boring taken for proposed Pond A.

Based on the preliminary roadway cross sections, floodplain impact (fill) area(s) were quantified per cross section and the average end method was used to determine the volumetric floodplain impacts due to the proposed widening of SR 46.

Floodplain impacts due to the construction of the new bridge were considered minimal and were not calculated as part of this floodplain analysis.

Floodplain impacts due to the construction of the ponds were determined by calculating the average fill height between the 100-year floodplain elevation and the ESHWT elevation per location. Then the pond area required to tie down the proposed pond berm elevation to the ESHWT elevation was measured in CADD. However, in some cases only a portion of the pond is within the floodplain boundary. In such cases, only those areas were measured to determine the floodplain impacts. In order to determine the volumetric floodplain impact created by the pond berms, the impact area(s) were multiplied by the average fill height.

Floodplain compensation for Floodplain No. 1 will be achieved by the construction of Floodplain Compensation Pond(s) 1 and 2. Floodplain compensation will be based on any cut volume between the 100-year floodplain elevation and the ESHWT elevation at each pond location.

Floodplain Compensation Pond 1 is located north of SR 46, adjacent to the Sterling Meadows subdivision. Once wetland delineation was performed by EMD, the original pond area was revised to avoid impacts to the wetland. However, the preliminary pond boring performed by Ardaman & Associates, Inc. was taken within the limits of this wetland and showed the ESHWT elevation at the ground surface. Additional borings are recommended to be performed within the revised pond location during the design phase of this project. For the purposes of this study, the geotechnical boring information from the Sterling Meadows subdivision Pond 101 (SJRWMD Permit No. 4-117-51666-2), was used to establish the ESHWT elevation for Floodplain Compensation Pond 1. The borings indicate that the average ESHWT elevation is 1.5 ft below the existing ground surface elevation. According to Lidar data, the ESHWT elevation would be approximately 7.5 ft NAVD. The Sterling Meadows subdivision Pond 101 is located just west of proposed Floodplain Compensation Pond 1. The northeast corner of this pond creates minor floodplain impacts and has been calculated by the method described above.

Floodplain Compensation Pond 2 is located east of Lake Jesup and north of SR 46, adjacent to modified Pond 2. The preliminary pond boring performed by Ardaman & Associates, Inc. indicates that the ESHWT elevation is 1 ft below the existing ground surface elevation. According to Lidar data, the ESHWT elevation from Ardaman & Associates, Inc. would be approximately 11.5 ft NAVD which appears to be relatively high considering the 100-year floodplain elevation is 9.0 ft NAVD and the permitted ESWHT elevation used for adjacent Pond 2, constructed during the bridge replacement project, is 8.0 ft NGVD which converts to 7.0 ft NAVD. Therefore an estimate of 8.0 ft NAVD will be used as the ESHWT elevation within the proposed pond area for the floodplain compensation

calculations. The northwest corner of this pond creates minor floodplain impacts and has been calculated by the method described above.

| Proposed Condition | Floodplain Impact Volume (ac-ft) | Floodplain Compensation Volume (ac-ft) |
|------------------------------------|--|--|
| SR 46 Widening | 29.17 | NA |
| Floodplain Comp Pond 1 | 0.04 | 11.09 |
| Pond A3 | 2.14 | NA |
| Modified Pond 1 | 0.82 | NA |
| Floodplain Comp Pond 2 | 0.08 | 24.27 |
| Floodplain No. 1 Project Total: | 32.25 | 35.36 |

The following table summarizes the 100-year floodplain impacts and compensation associated with Floodplain No. 1. For detailed calculations of the values shown, please refer to Appendix E.

Floodplain No. 2

According to the FEMA FIRM maps, the limits of Floodplain No. 2 begin at STA 199+59 and ends at STA 211+48 within the proposed right-of-way required for the proposed widening of SR 46. This floodplain is located on the north side of SR 46 and is classified as Zone A, where the base floodplain elevation has not been determined. In order to establish the 100-year floodplain elevation, the FEMA floodplain area was digitized and overlaid upon the one-foot Lidar contours and compared to one another. Through this process, a preliminary estimate for the 100-year floodplain elevation was determined to be 16.5 ft NAVD. Due to the proximity and similar soil type, the ESWHT elevation from the preliminary pond boring for proposed Pond B will be used to establish the ESHWT elevation for Floodplain No. 2 calculations. According to Lidar Data, the existing ground elevation at the boring is 15.0 ft NAVD, which puts the ESHWT elevation at 14.5 ft NAVD. The roadway embankment required for the proposed widening of SR 46 will result in impacts to this floodplain. Floodplain impacts will be based on any fill volume above the ESHWT elevation or natural ground, whichever is higher, to the 100-year floodplain elevation.

Floodplain compensation for Floodplain No. 2 will be achieved by the construction of roadside ditches. Floodplain compensation will be based on any cut volume between the 100-year floodplain elevation and the ESHWT elevation.

The following table summarizes the 100-year floodplain impacts and compensation associated with Floodplain No. 2. For detailed calculations of the values shown, please refer to Appendix E.

| Proposed Condition | Floodplain Impact Volume (ac-ft) | Floodplain Compensation Volume (ac-ft) |
|------------------------------------|--|--|
| SR 46 Widening | 0.69 | 0.69 |
| | | |
| Floodplain No. 2 Project Total: | 0.69 | 0.69 |

Floodplain No. 3

According to the FEMA FIRM maps, the limits of Floodplain No. 3 begin at STA 198+77 and ends at STA 204+99 within the proposed right-of-way required for the proposed widening of SR 46. This floodplain is located on the south side of SR 46 and is classified as Zone A, where the base floodplain elevation has not been determined. In order to establish the 100-year floodplain elevation, the FEMA floodplain area was digitized and overlaid upon the one-foot Lidar contours and compared to one another. Through this process, a preliminary estimate for the 100-year floodplain elevation was determined to be 16.5 ft NAVD. Due to the proximity and similar soil type, the ESWHT elevation from the preliminary pond boring for proposed Pond B will be used to establish the ESHWT elevation for Floodplain No. 3 calculations. According to Lidar Data, the existing ground elevation at the boring is 15.0 ft NAVD, which puts the ESHWT elevation at 14.5 ft NAVD. The roadway embankment required for the proposed widening of SR 46 will result in impacts to this floodplain. Floodplain impacts will be based on any fill volume above the ESHWT elevation or natural ground, whichever is higher, to the 100-year floodplain elevation.

Floodplain compensation for Floodplain No. 3 will be achieved by the construction of roadside ditches. Floodplain compensation will be based on any cut volume between the 100-year floodplain elevation and the ESHWT elevation.

The following table summarizes the 100-year floodplain impacts and compensation associated with Floodplain No. 3. For detailed calculations of the values shown, please refer to Appendix E.

| Proposed Condition | Floodplain Impact Volume (ac-ft) | Floodplain Compensation Volume (ac-ft) |
|------------------------------------|--|--|
| SR 46 Widening | 0.19 | 0.22 |
| | | |
| Floodplain No. 3 Project Total: | 0.19 | 0.22 |

Floodplain No. 4

According to the FEMA FIRM maps, the limits of Floodplain No. 4 begin at STA 295+18 and ends at STA 313+10. This floodplain is located on the south side of SR 46 and is classified as Zone AE, where the base floodplain elevation has been determined to be 29.0 ft NAVD.

The existing roadway profile within this area ranges from 25.0 ft to 28.5 ft NAVD. By digitizing the FEMA floodplain area and overlaying it upon the proposed roadway alignment, it appears as though the widening would encroach upon this floodplain. However, while developing preliminary roadway cross sections with use of one-foot Lidar contours for this area, there appears to be an existing land berm which contains the 100-year floodplain from encroaching into SR 46. The fact that there has been no record of flooding issues in this area would further reinforce this assumption.

During the design phase of this project, it would be prudent to gather additional survey to define the limits of the existing land berm to ensure that the 100-year floodplain would not encroach into the proposed widening of SR 46. In addition, if any proposed improvements impact the existing land berm, replacement of the berm at an elevation higher than 29.0 ft NAVD will be required.

Floodplain No. 5

According to the FEMA FIRM maps, the limits of Floodplain No. 5 begin at STA 295+35 and ends at STA 296+32 within the proposed right-of-way required for the proposed widening of SR 46. This floodplain is located on the north side of SR 46 and is classified as Zone A, where the base floodplain elevation has not been determined. In order to establish the 100-year floodplain elevation, the FEMA floodplain area was digitized and overlaid upon the one-foot Lidar contours and compared to one another. Through this process, a preliminary estimate for the 100-year floodplain elevation was determined to be 22.5 ft NAVD.

The limits of Floodplain No. 5 only encroach into the proposed 10-foot shareduse-path on the north side of the roadway. Since this encroachment area is so minor, during the design phase of this project the horizontal and vertical placement of the proposed 10-foot shared-use-path should be adjusted to avoid any impacts to Floodplain No. 5.

10.0 PROJECT CLASSIFICATION

The floodplains are located in a low density, non-urbanized area, and the encroachments are classified as "minimal". Minimal encroachments on floodplain occur when there is a floodplain involvement, but the impacts on human life, transportation facilities, and natural and beneficial floodplain values are not significant and can be resolved with minimal efforts. Normally, these minimal efforts to address the impacts will consist of applying the Department's drainage design standards and following the Water Management District's procedures to achieve results that will not increase or significantly change the flood elevations and/or limits.

11.0 RISK EVALUATION

There is no change in flood "Risk" associated with this project. The floodplains are located in a low density, non-urbanized area, and the encroachments are classified as "minimal". Minimal encroachments on floodplain occur when there is a floodplain involvement, but the impacts on human life, transportation facilities, and natural and beneficial floodplain values are not significant and can be resolved with minimal efforts. Normally, these minimal efforts to address the impacts will consist of applying the Department's drainage design standards and following the Water Management District's procedures to achieve results that will not increase or significantly change the flood elevations and/or limits.

12.0 PD&E MANUAL REQUIREMENTS WITH MINIMAL ENCROACHMENTS

Chapter 24 Floodplains of the FDOT's PD&E Manual, Part 2, defines four categories of encroachments as they pertain to the base floodplain involvement; significant, minimal, none and no involvement, and also lists the report criteria corresponding to these encroachment categories. The FDOT has different requirements based on the category of the encroachment. The proposed SR 46 widening project was determined to have minimal encroachments and as a result the requirements for this category are listed as follows:

1. The history of flooding of the existing facility and/or measures to minimize any impacts due to the proposed project improvements.

Response: According to the FDOT Maintenance Department, there are two locations were flooding problems have occurred at the downstream side of the existing cross drains. In both locations, the flooding occurs outside of FDOT right-of-way and within private properties.

The first location being in the vicinity of CD-4, north of SR 46 and east of Mullet Lake Park Road. The FDOT Maintenance Department believes that the flooding problem exists in this area due to the lack of positive drainage grading located within some private properties and the ultimate outfall of the conveyance system leading into the St. Johns River. Currently, Seminole County is evaluating the drainage concerns in this area and maybe developing roadway and drainage plans that may include a stormwater management facility as well as upsizing the conveyance system/pipes which convey stormwater runoff to the St. Johns River.

The second location being in the vicinity of CD-5, north of SR 46 and east of Mockingbird Lane. The FDOT Maintenance Department believes that the flooding problem exists in this area due to the lack of positive drainage grading located within the private property into which the cross drain discharges before entering the wetland located within this property. Currently, the proposed location of alternative stormwater treatment Pond D1 is within this property. If this alternative is selected as the preferred alternative, additional right-of-way will be purchased to ensure positive drainage is achieved from the outfall of the existing cross drain to the wetland by regarding the ditch.

In addition, two floodplain compensation areas will be constructed to mitigate loss of storage in the floodplain due to the project improvements. The project will have no adverse impacts on the existing floodplain conditions.

2. Determination of whether the encroachment is longitudinal or transverse, and if it is a longitudinal encroachment an evaluation and discussion of practicable avoidance alternatives. Response: The proposed increase in the number of travel lanes will result in both longitudinal and transverse impacts to the floodplain. Longitudinal impacts will be minimized by utilizing the maximum allowable roadway embankment slope.

The transverse floodplain impacts from the project occur due to the extension and/or replacement of the existing cross drains and construction of the new bridge. Cross Drain Analysis, found in Appendix D, will show that there will be no net increase in the existing backwater elevations at each proposed cross drain. The Bridge Hydraulic Report (BHR) will show both pre-development and post-development Design High Water (DHW) elevations for construction of the new bridge.

The existing roadway bisects the floodplain. There are no economically feasible avoidance alternatives.

3. The practicability of avoidance alternatives and/or measures to minimize impacts.

Response: This project will take every effort to minimize the floodplain impacts resulting from roadway fill. The maximum allowable roadway embankment slope will be used within the floodplain area to minimize the floodplain impacts. The floodplain impacts will be mitigated by constructing floodplain compensation areas. There are two (2) floodplain compensation ponds identified by this project to mitigate for the floodplain impacts to Floodplain No. 1 and construction of roadside ditches will mitigate for floodplain impacts to Floodplain No.(s) 2 and 3.

4. Impact of the proposed improvement on emergency services and evacuation.

Response: The proposed cross drains and floodplain compensation areas will perform hydraulically in a manner equal to or greater than the existing conditions, and backwater surface elevations are not expected to increase. As a result, there will be no significant change in flood risk, and there will not be a significant change in the potential for interruption or termination of emergency service or in emergency evacuation routes.

5. Impacts of proposed improvement on the base flood, likelihood of flood risk, overtopping, location of overtopping, backwater, etc.

Response: The proposed cross drains and floodplain compensation areas will perform hydraulically in a manner equal to or greater than the existing conditions, and backwater surface elevations are not expected to increase. As a result, there will be no significant change in flood risk or overtopping.

6. Determination of the impact to the proposed improvements on regulatory floodways, if any, and documentation of coordination with FEMA and local agencies to determine the project's consistency with regulatory floodway.

Response: According to the FEMA FIRM Maps, there are no regulatory floodways along the proposed improvements.

7. The impacts on natural and beneficial floodplain values, and measures to restore and preserve these values (this information may also be addressed as part of the wetland impact evaluation and recommendations).

Response: There will not be any impact on natural and beneficial values. Also, please refer to the Wetlands Evaluation Report.

8. Consistency of the proposed improvements with the local floodplain development plan or the land use elements in Comprehensive Plan, and the potential of encouraging development in the 100 year base floodplain.

Response: The project will remain consistent with local floodplain development plans. The project will not support base floodplain development that is incompatible with existing floodplain management programs.

9. A map showing project, location, and impacted floodplains. Provide copies of applicable FIRM maps should be included within the final LHR report appendix.

Response: Please refer to the SR 46 PD&E Location Hydraulic Report.

10. Results of any risk assessments performed.

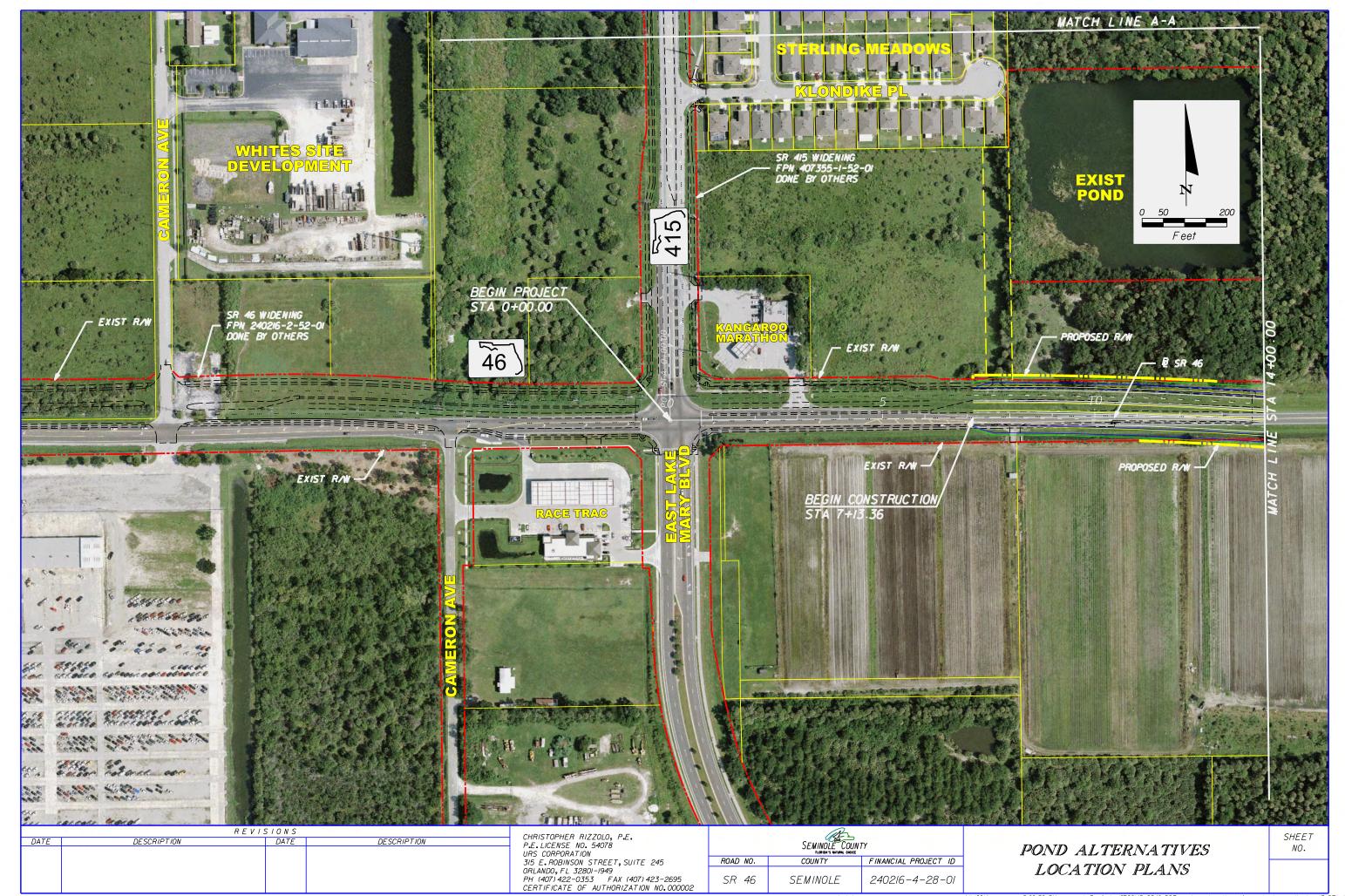
Response: No risk assessments were performed; however, the proposed cross drains and floodplain compensation areas will perform hydraulically in a manner equal to or greater than the existing conditions, and backwater surface elevations are not expected to increase. As a result, there will be no significant change in flood risk.

13.0 CONCLUSION

The modifications to drainage structures included in this project will result in no change in their capacity to carry floodwater. The proposed structures will perform hydraulically in a manner equal to or greater than the existing structure and backwater surface elevations are not expected to increase. Floodplain compensation areas will mitigate for all floodplain impacts associated with the proposed roadway improvements. As a result, there will be no significant adverse impacts on natural and beneficial floodplain values or any significant change in flood risks or damage. There will not be a significant change in the potential for interruption or termination of emergency service or emergency evacuation routes. Therefore, it has been determined that this encroachment is not significant.

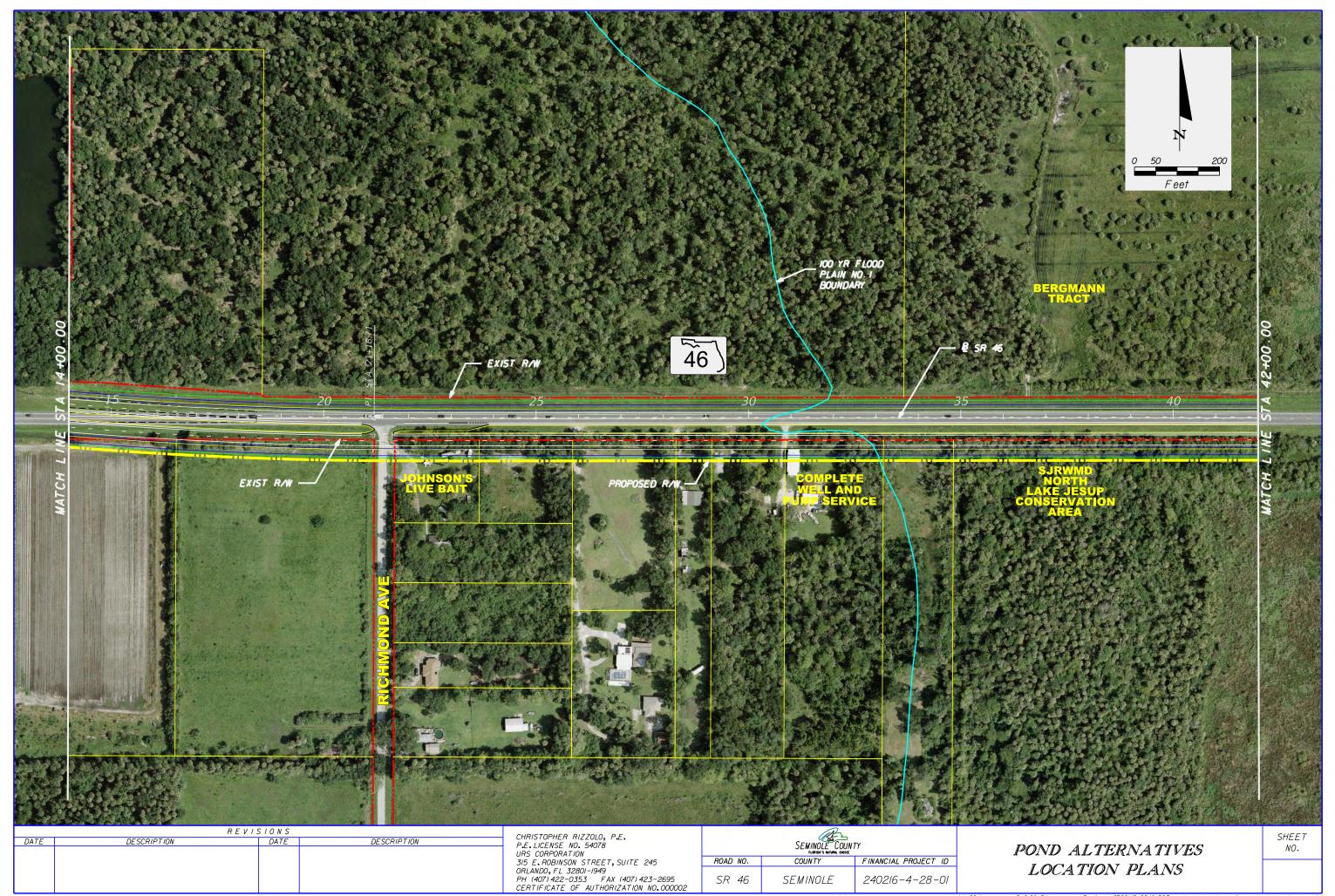
APPENDIX A Pond Alternatives Location Plans

SR 46 PD&E LOCATION HYDRAULICS REPORT

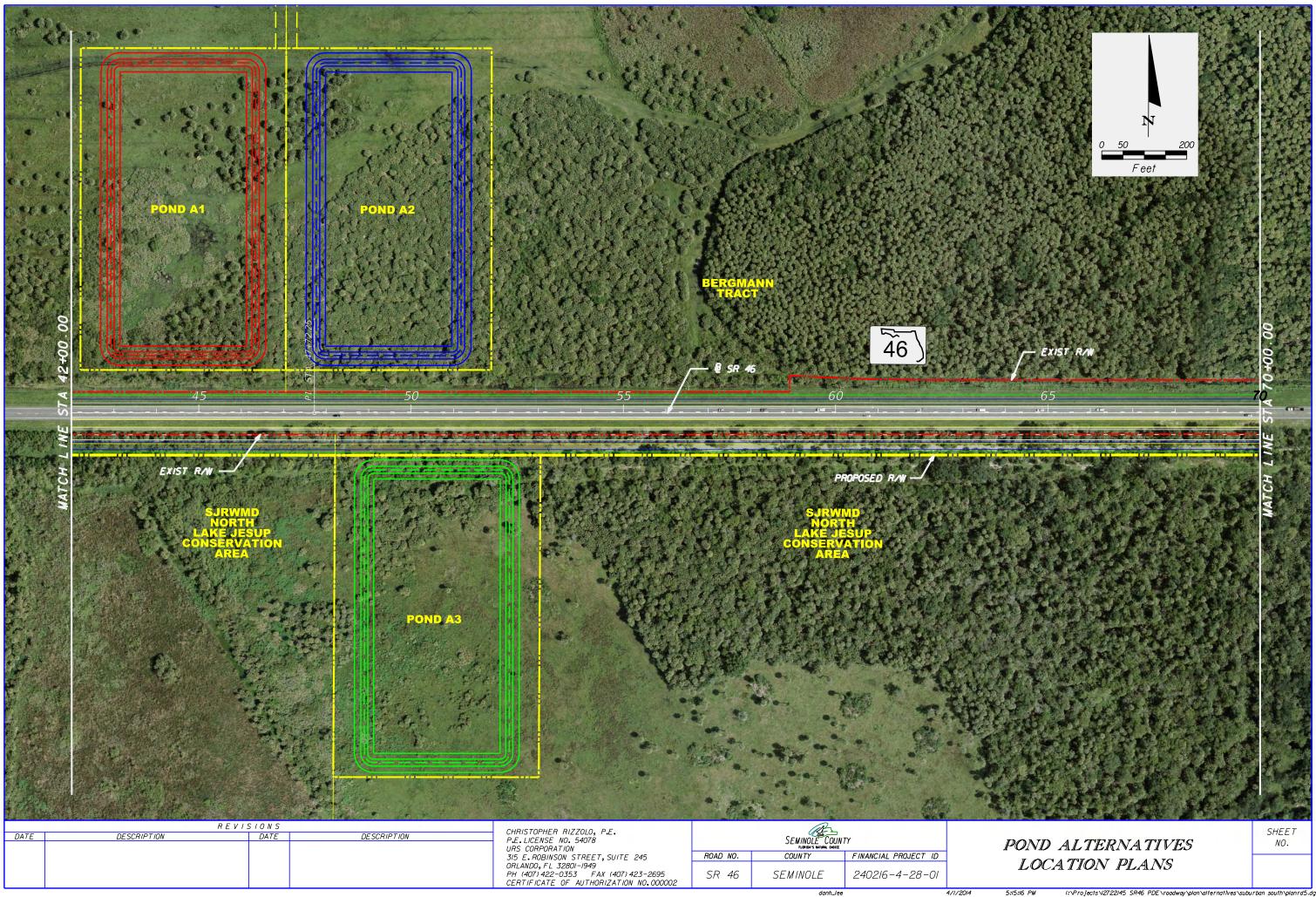


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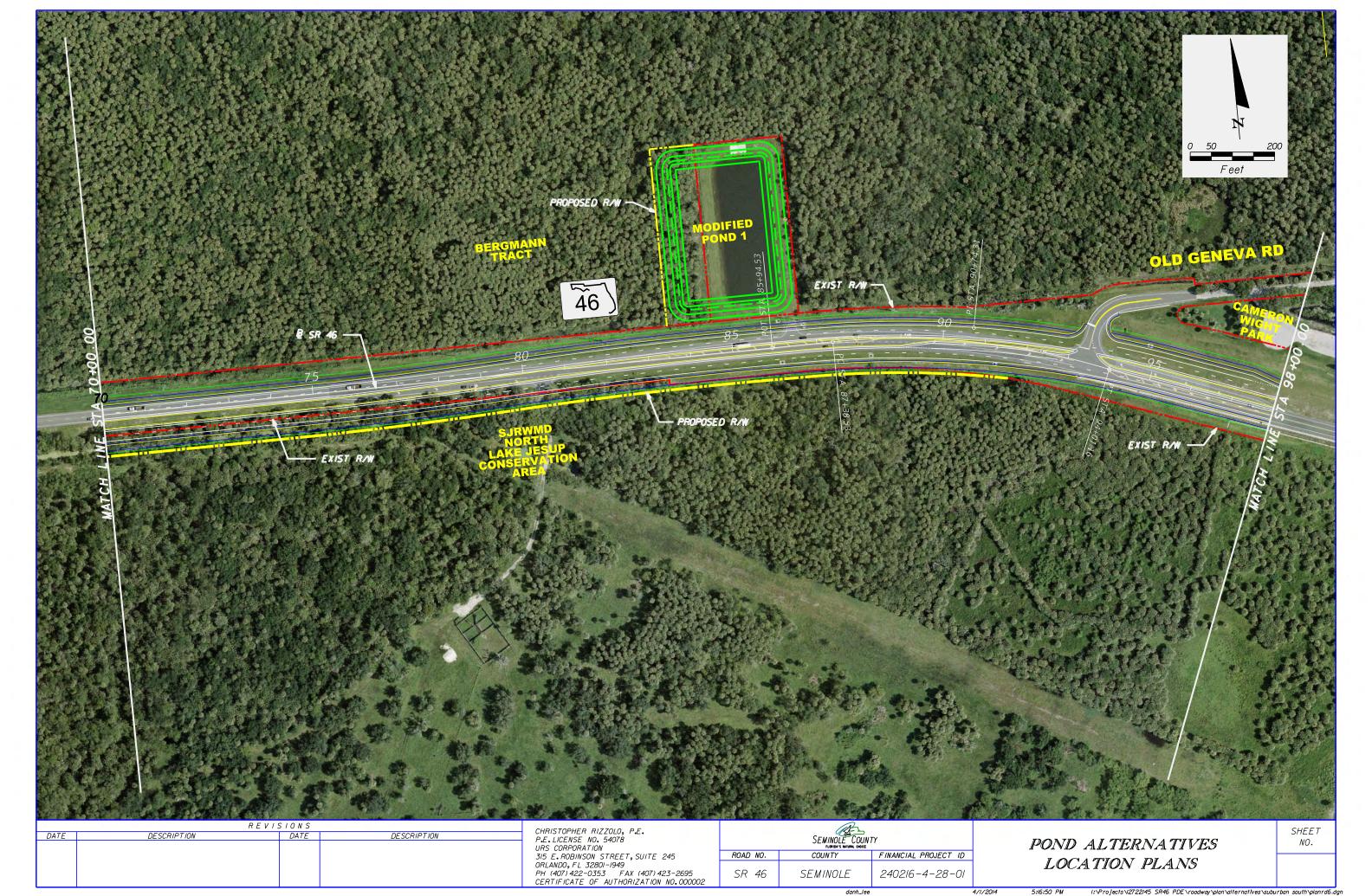


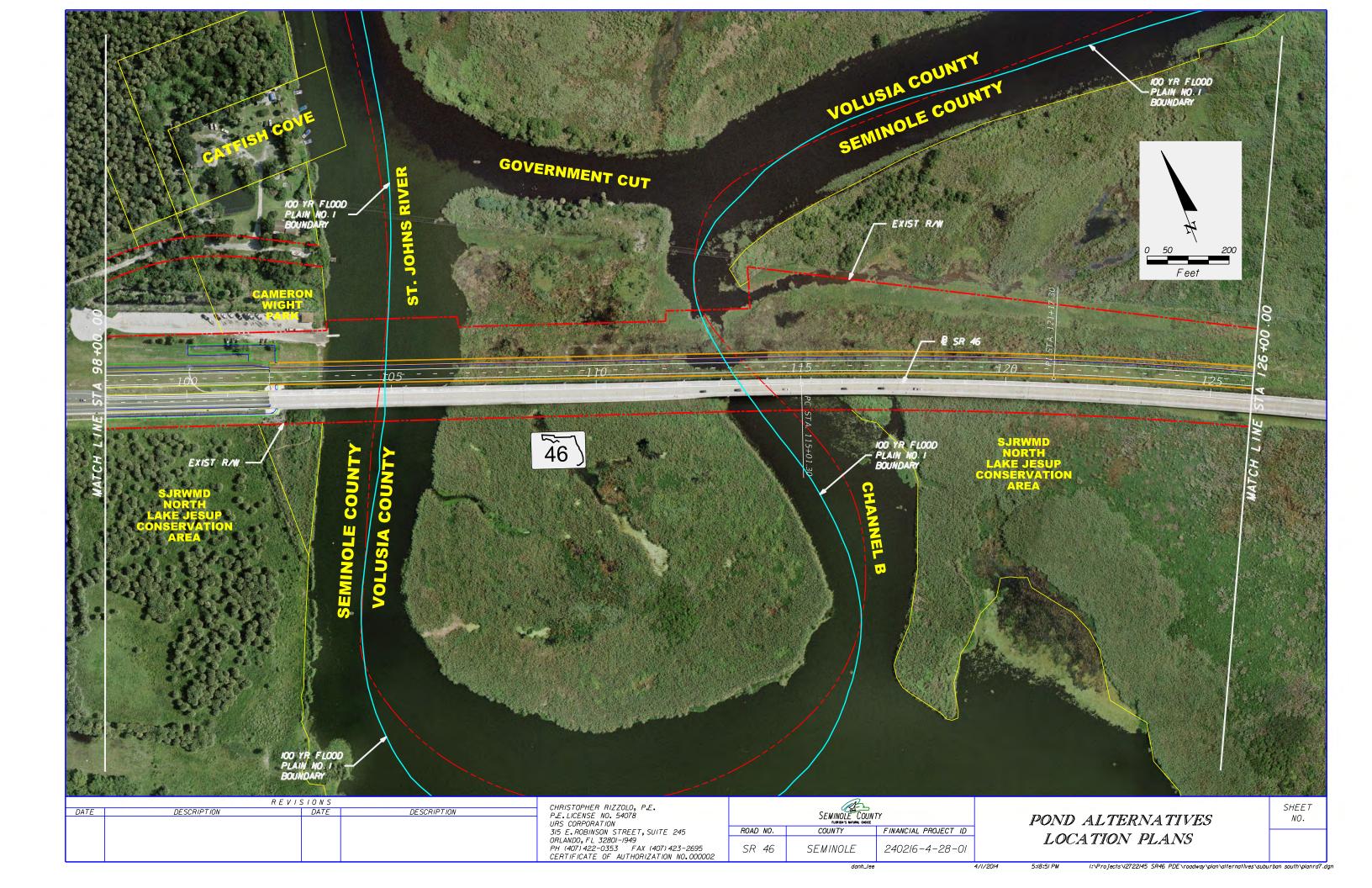
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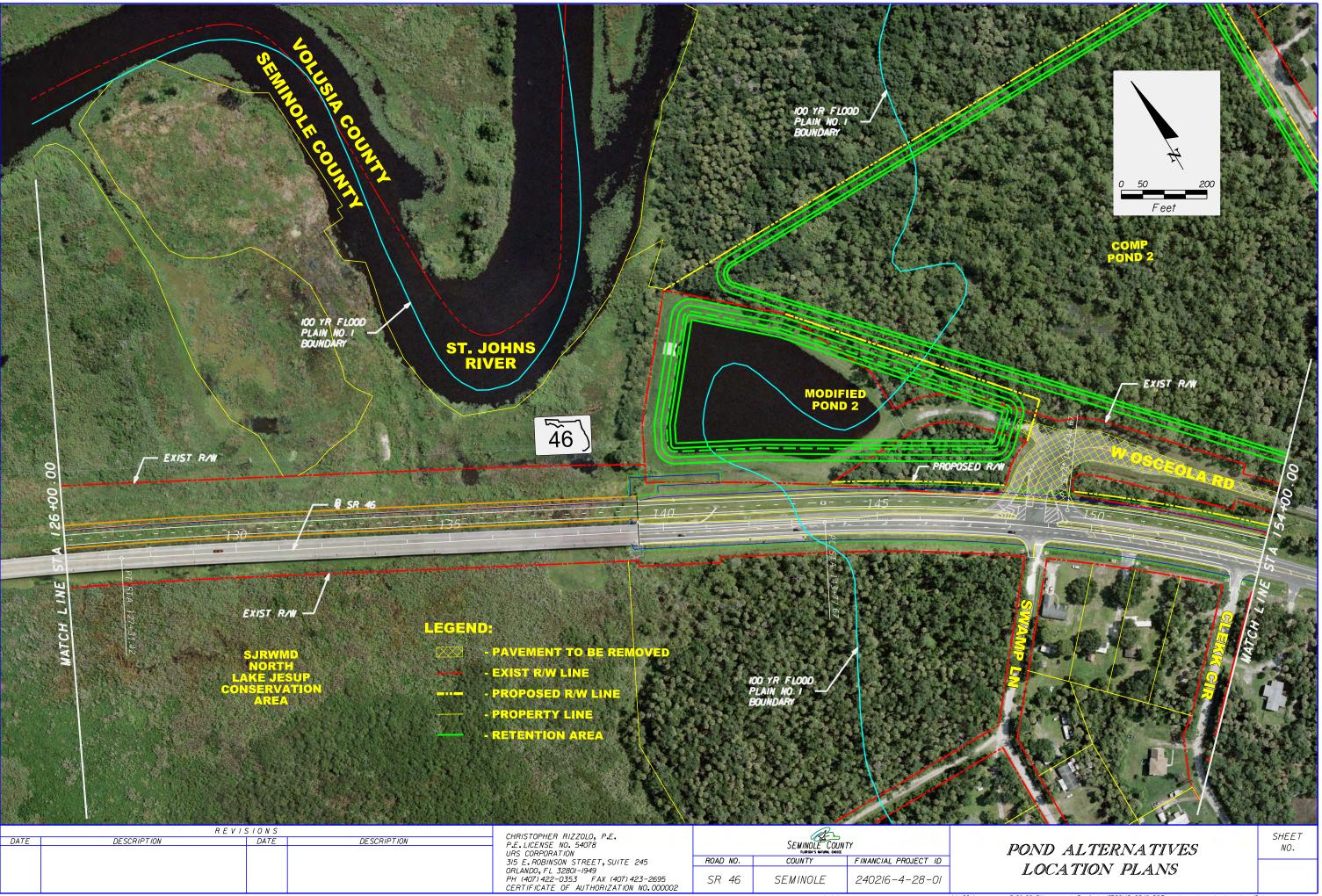


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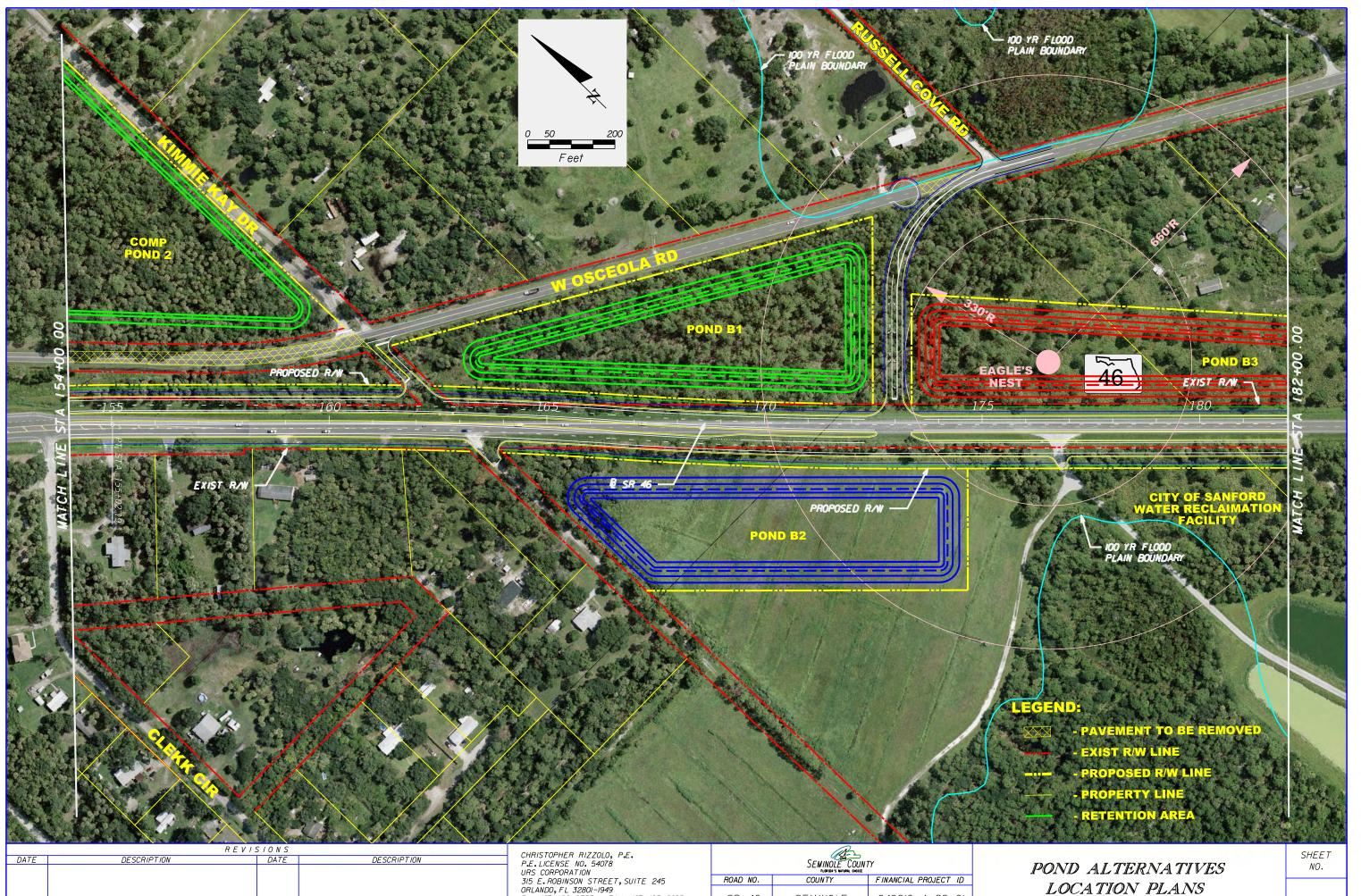
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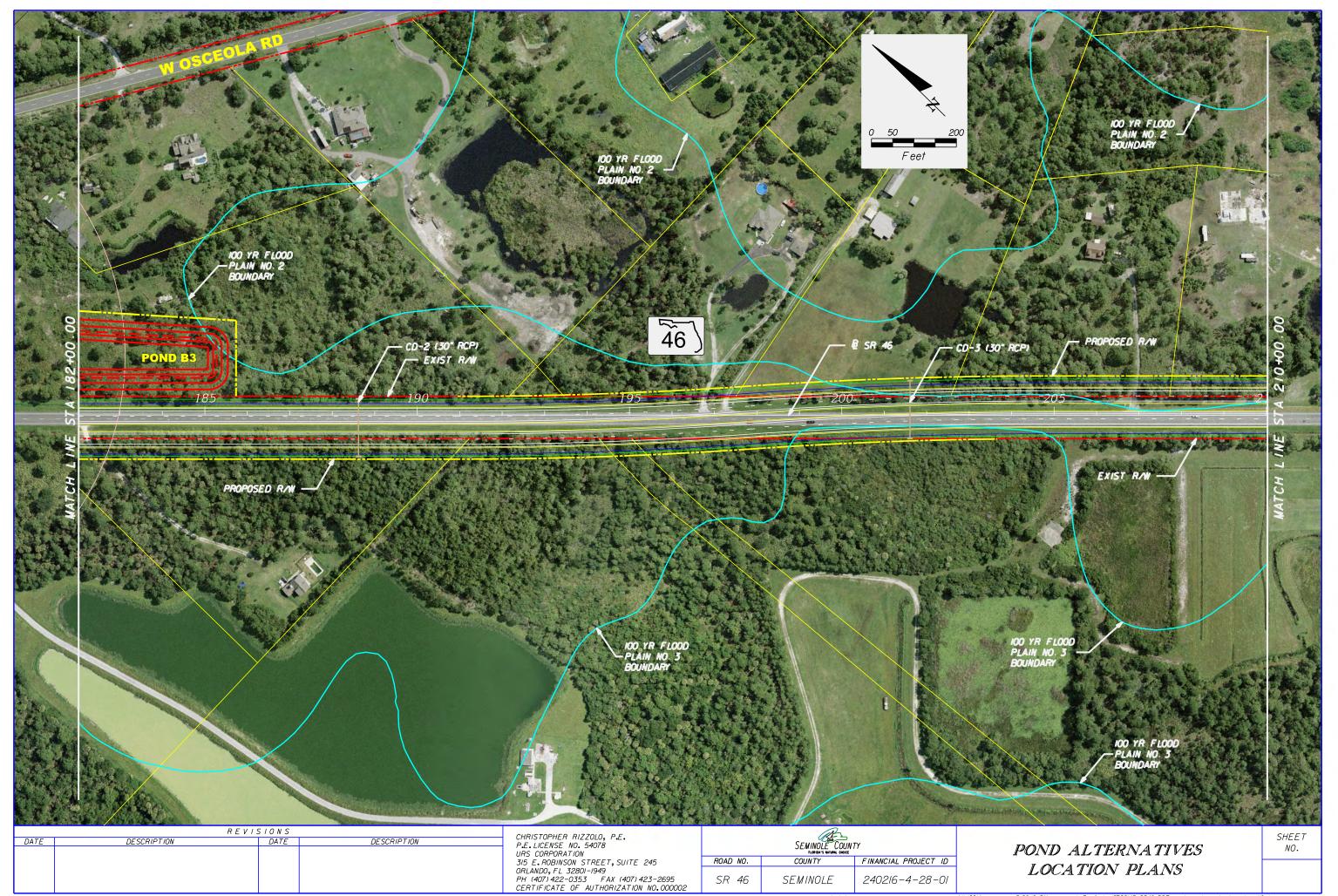
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LOCATION PLANS

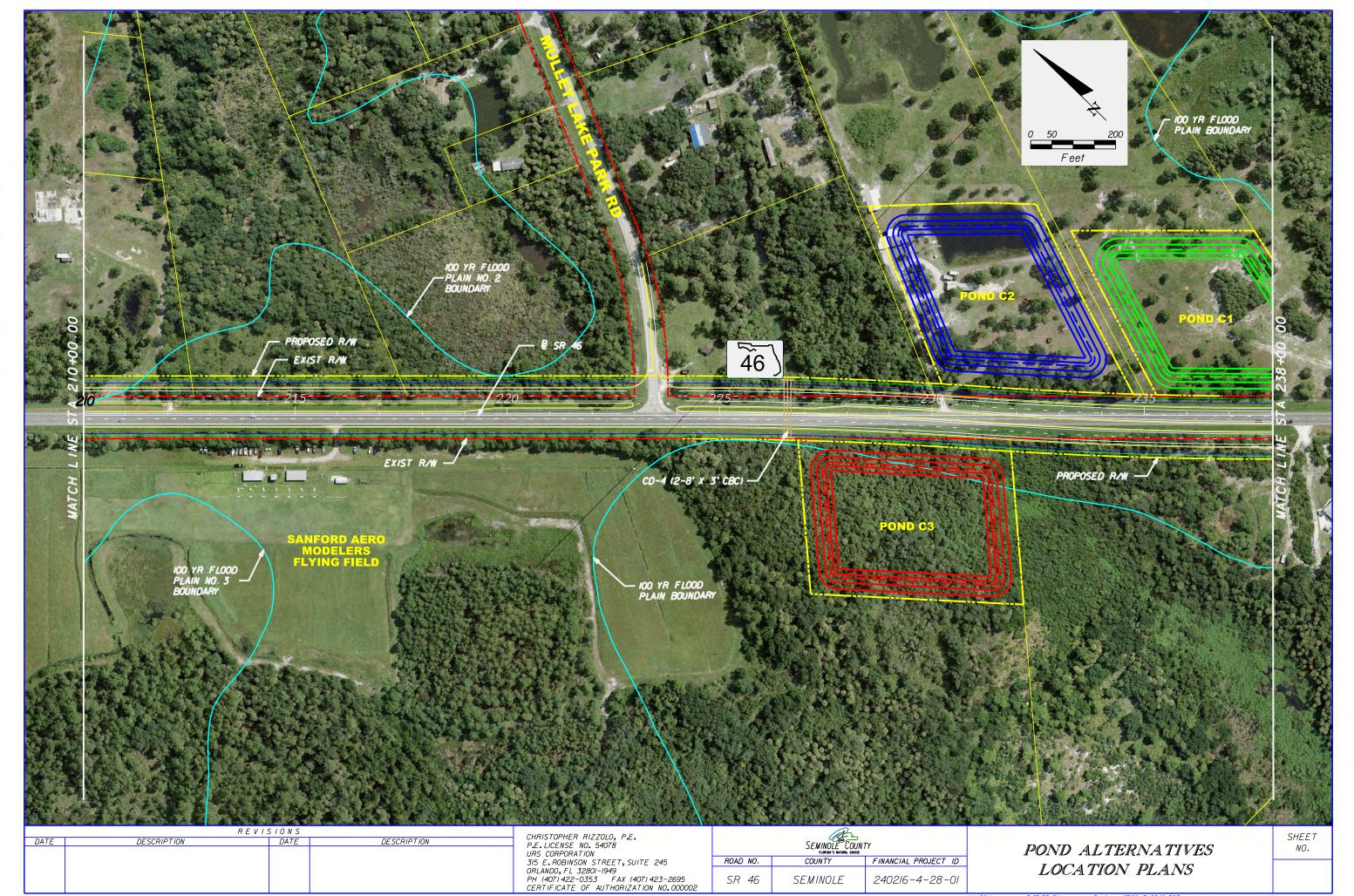


CHRISTOPHER RIZZOLO, P.E. P.E.LICENSE NO. 54078 URS CORPORATION 315 E.ROBINSON STREET, SUITE 245 ORLANDO, FL 32801-1949 PH (407) 422-0353 FAX (407) 423-2695 CERTIFICATE OF AUTHORIZATION NO.000002 ROAD NO. SR 46 SEMINOLE

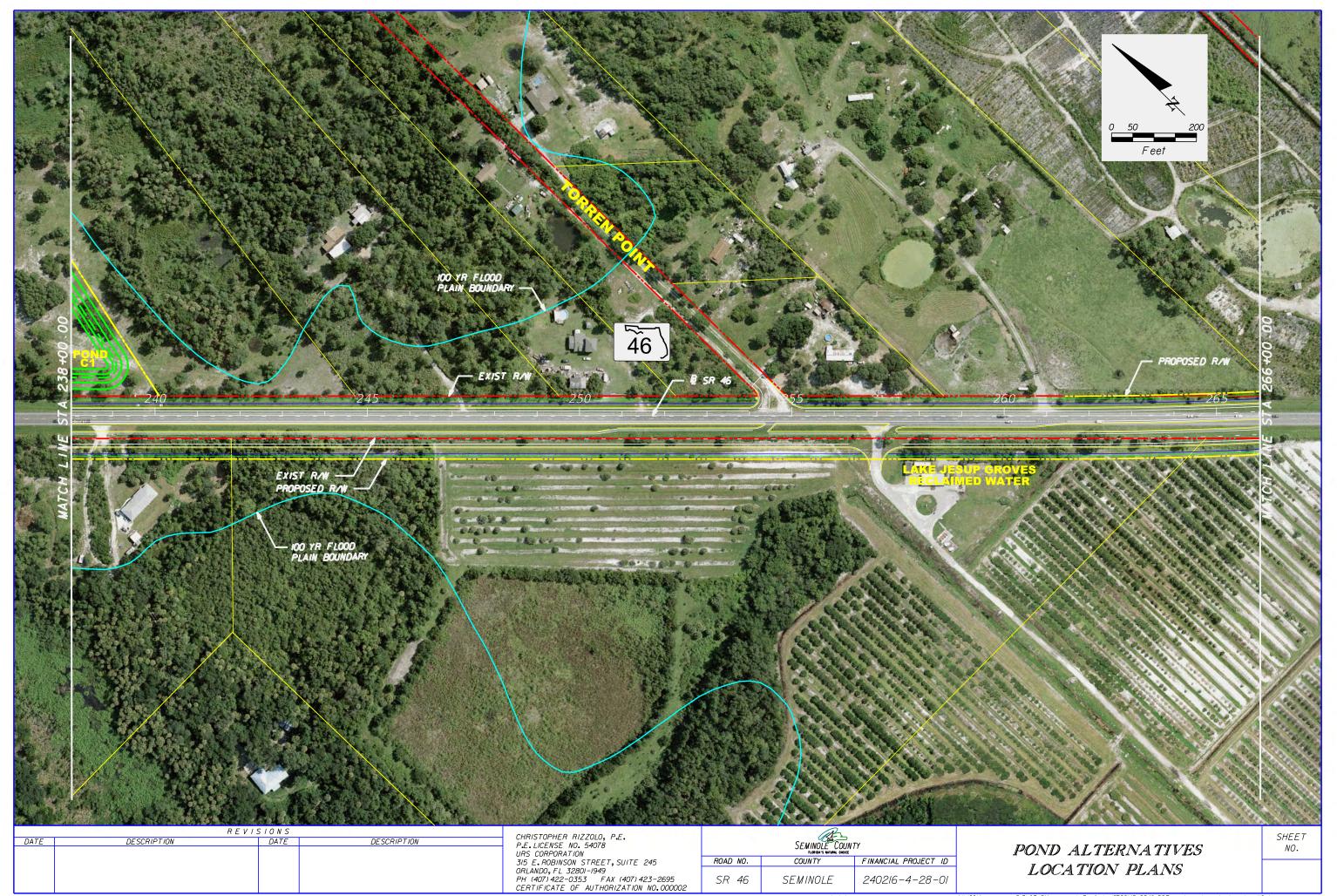
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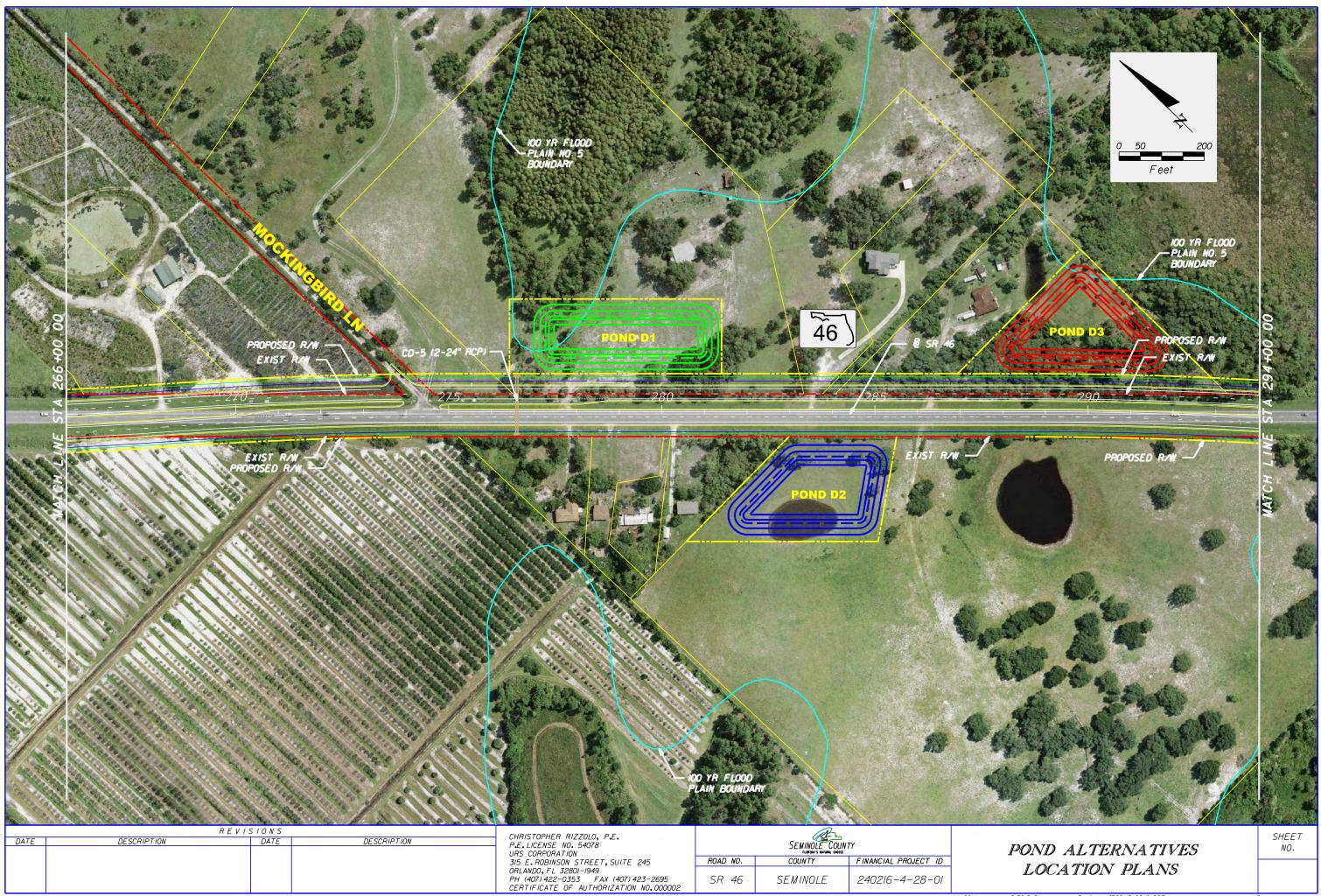
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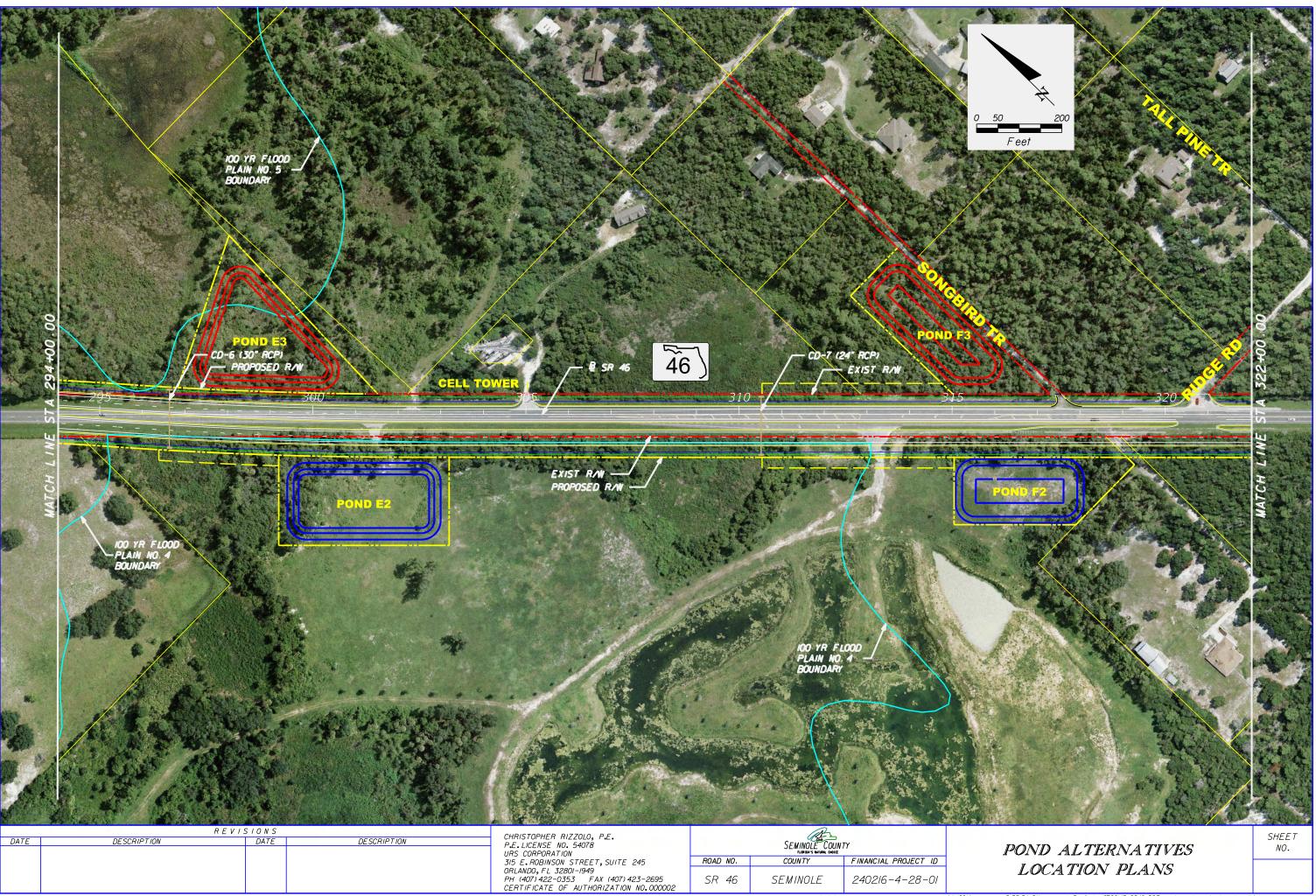
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POND ALTERNATIVES LOCATION PLANS



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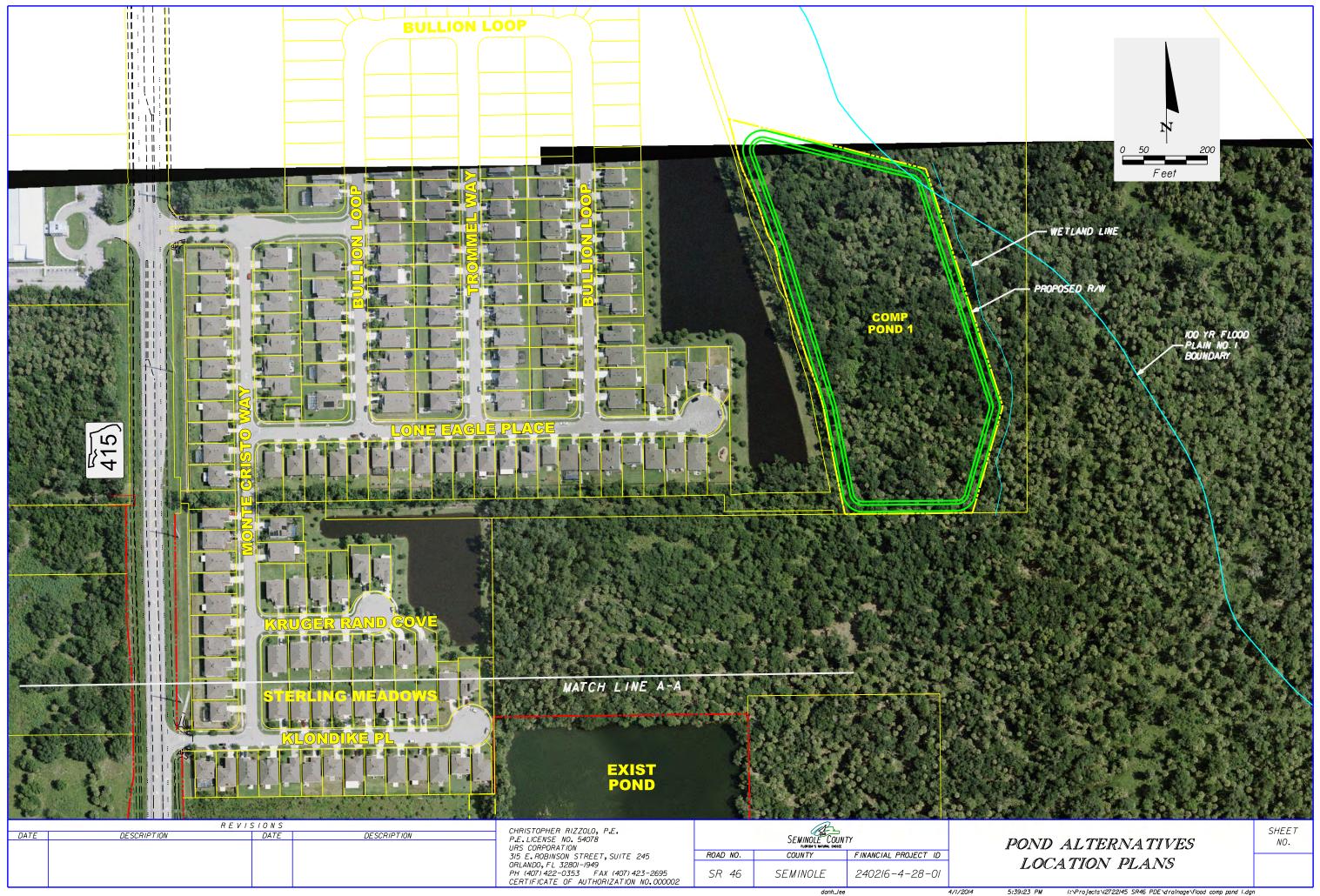
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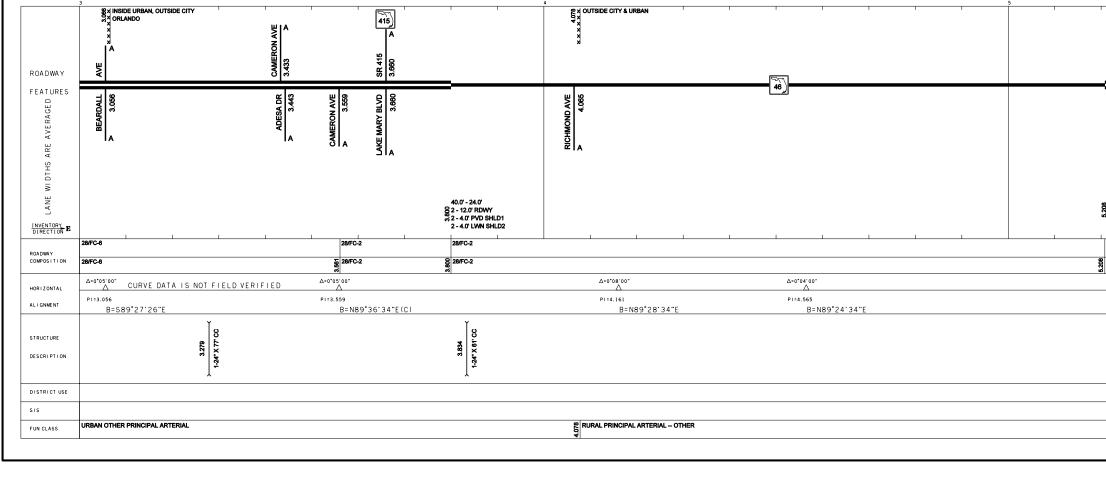
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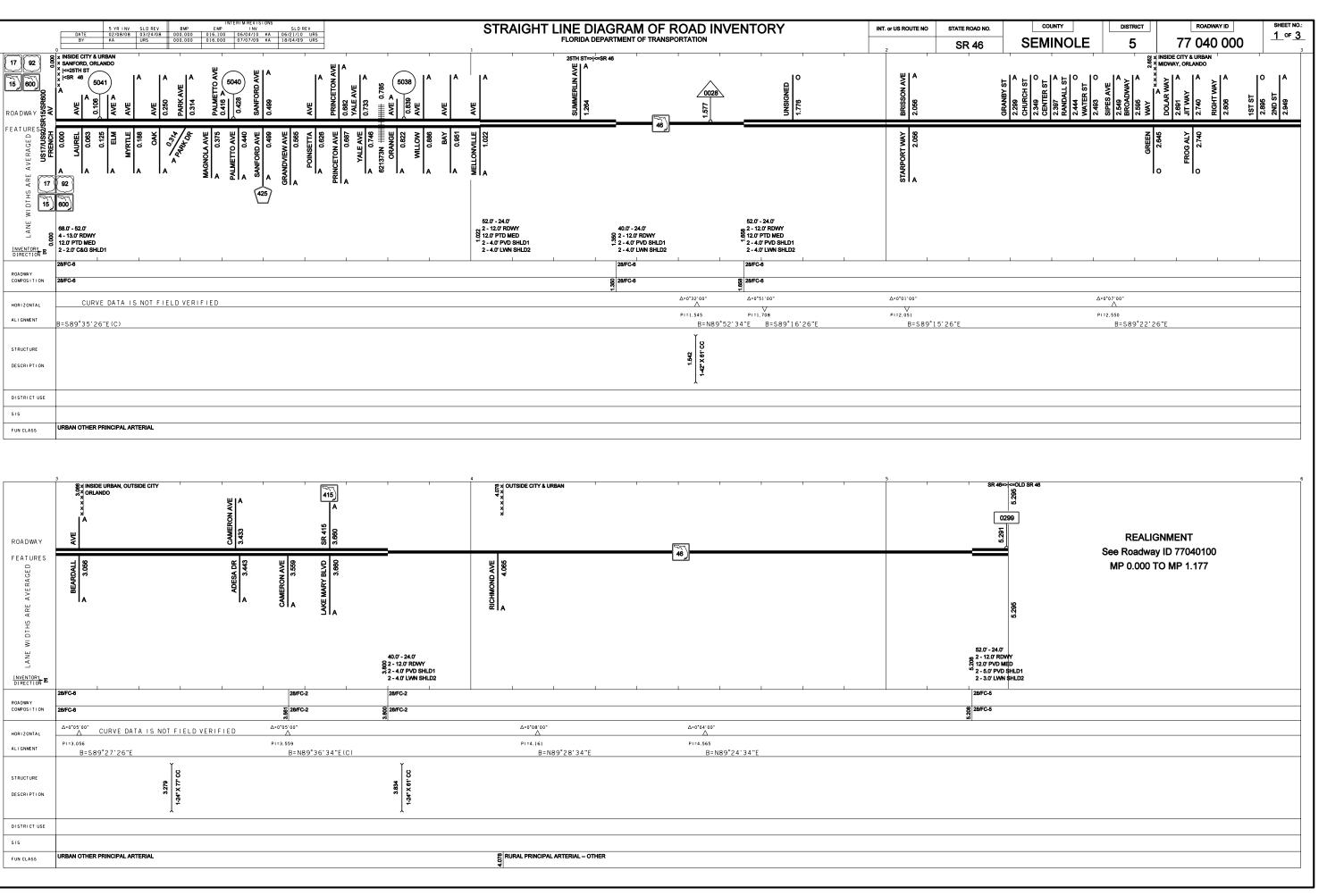
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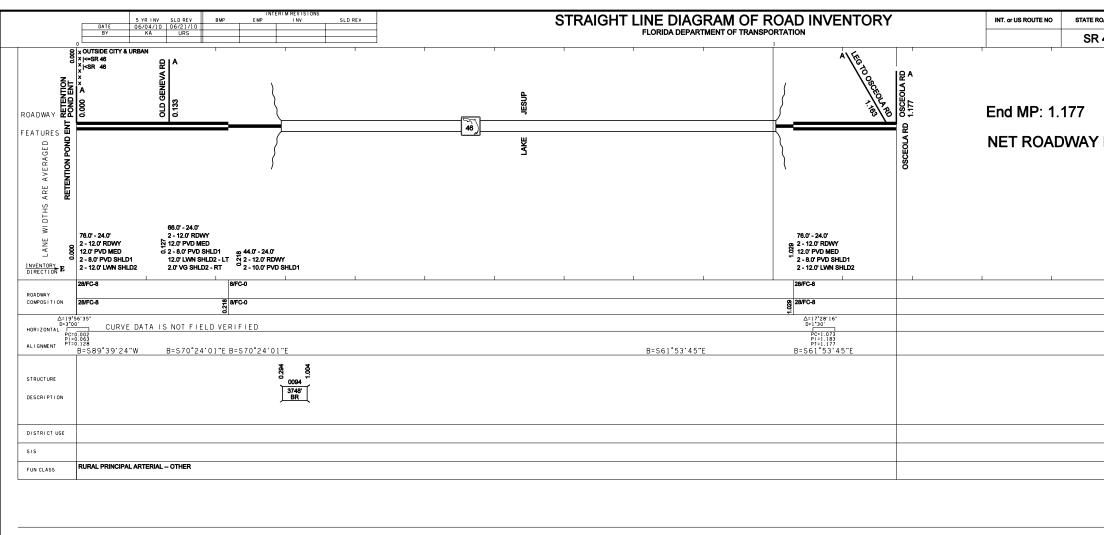
APPENDIX B FDOT Straight Line Diagram of Road Inventory

SR 46 PD&E LOCATION HYDRAULICS REPORT

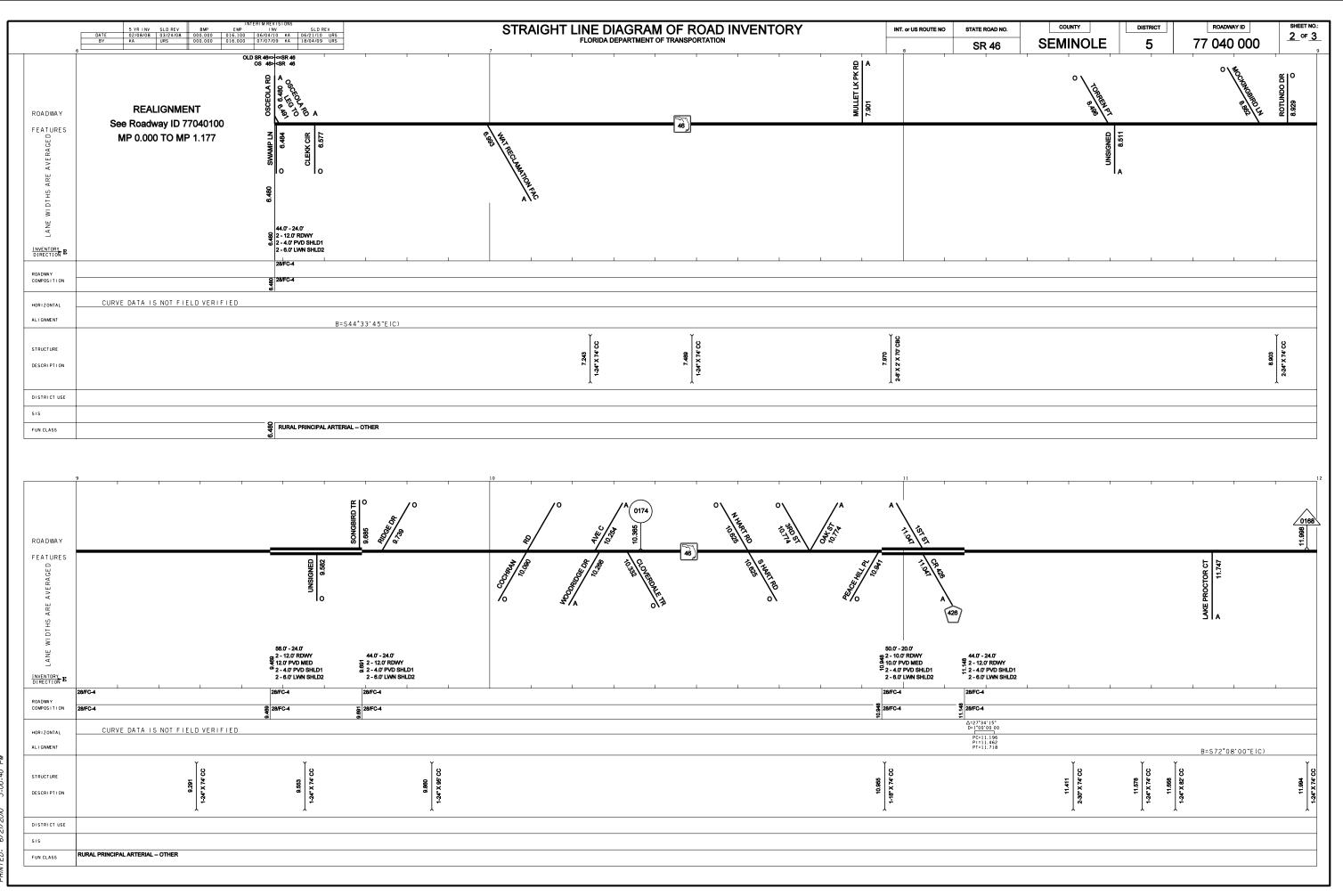




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APPENDIX C Cross Drain Photos

SR 46 PD&E LOCATION HYDRAULICS REPORT



<u>Cross Drain No. 1 – Looking North</u>



<u>Cross Drain No. 1 – Looking South</u>



<u>Cross Drain No. 2 – Looking North</u>



Cross Drain No. 2 – Looking South



Cross Drain No. 3 – Looking North



Cross Drain No. 3 – Looking South



<u>Cross Drain No. 4 – Looking North</u>



<u>Cross Drain No. 4 – Looking South</u>



<u>Cross Drain No. 5 – Looking North</u>



<u>Cross Drain No. 5 – Looking South</u>



<u>Cross Drain No. 6 – Looking North</u>



<u>Cross Drain No. 6 – Looking South</u>



<u>Cross Drain No. 7 – Looking North</u>



<u>Cross Drain No. 7 – Looking South</u>



Cross Drain No. 8 – Looking North



Cross Drain No. 8 – Looking South



<u>Cross Drain No. 9 – Looking North</u>



Cross Drain No. 9 – Looking South

APPENDIX D Cross Drain Analysis

SR 46 PD&E LOCATION HYDRAULICS REPORT

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| Project: | SR 46 PD&E Study (SR 415 to CR 426) | Design By: DEP | Date: | <u>9/25/2012</u> |
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| FIN No.: | 240216-4-28-01 | NT7 | . 1 | _ |
| | | Checked by: NTL | Date: 9 | 25/12 |
| Subject: | CD-1: 24" RCP (Sta 9+23.76) | | | |

Existing Culvert

Note: Based on the Record of Conversation document dated Feb. 7th, 2012 between URS and FDOT Maintenance Office (Jim Wood), there is no recorded history of problems associated with CD-1. Based on the URS site visit canducted on Feb. 12th, 2012 there are no apparent erosion problems. Existing plans were not consistent on the size or type of the pipe, for the purpose of the PD&E evaluatian the pipe was estimated to be a 24" RCP.

| Existing Information: Culvert Diameter: 2 ft No of culverts: 1 Material: RCP Exist culvert length: 62.5 ft | Method used: | Velocity (v) = | <u>6 ft/s</u> | (Since no | history of problems is known) | |
|--|-----------------------|---|--|-----------|-------------------------------|--|
| Avge flowline elev downstream: <u>10.72</u> (NAVD) Longitudinal slope: 0.029440 = <u>2.9440%</u> | Existing Information: | No of culverts: Exist culvert length: Avge flowline elev upstream: Avge flowline elev downstream: Longitudinal slope: | <u>1</u> <u>62.5 ft</u> <u>12.56</u> <u>10.72</u> 0.029440 | = | | |

Estimate discharge & Overtopping & HW for existing and proposed:

Area of culvert (A): <u>3.1 sq ft</u>

| Frequency | Factor | Q = A x v | HW Stage | HW Stage |
|-----------|--------|-----------|----------|----------|
| | | | Existing | Proposed |
| | | | (Note 2) | (Note 3) |
| (yr) | | cu ft/s | | |
| 25 | | 18.8 | | |
| 50 | | 22.50 | 15.89 | N/A |
| | | (Note 1) | | |
| 100 | 1.4 | 26.4 | 16.21 | N/A |
| 500 | 1.7 | 44.8 | 16.24 | N/A |
| | | | | |

| | Overtopping | I |
|-------------|-------------|----------|
| | Existing | Proposed |
| Elev (NAVD) | 16.2 | N/A |
| Q* (cfs) | 24.15 | N/A |
| Freq (yr) | 71 | N/A |

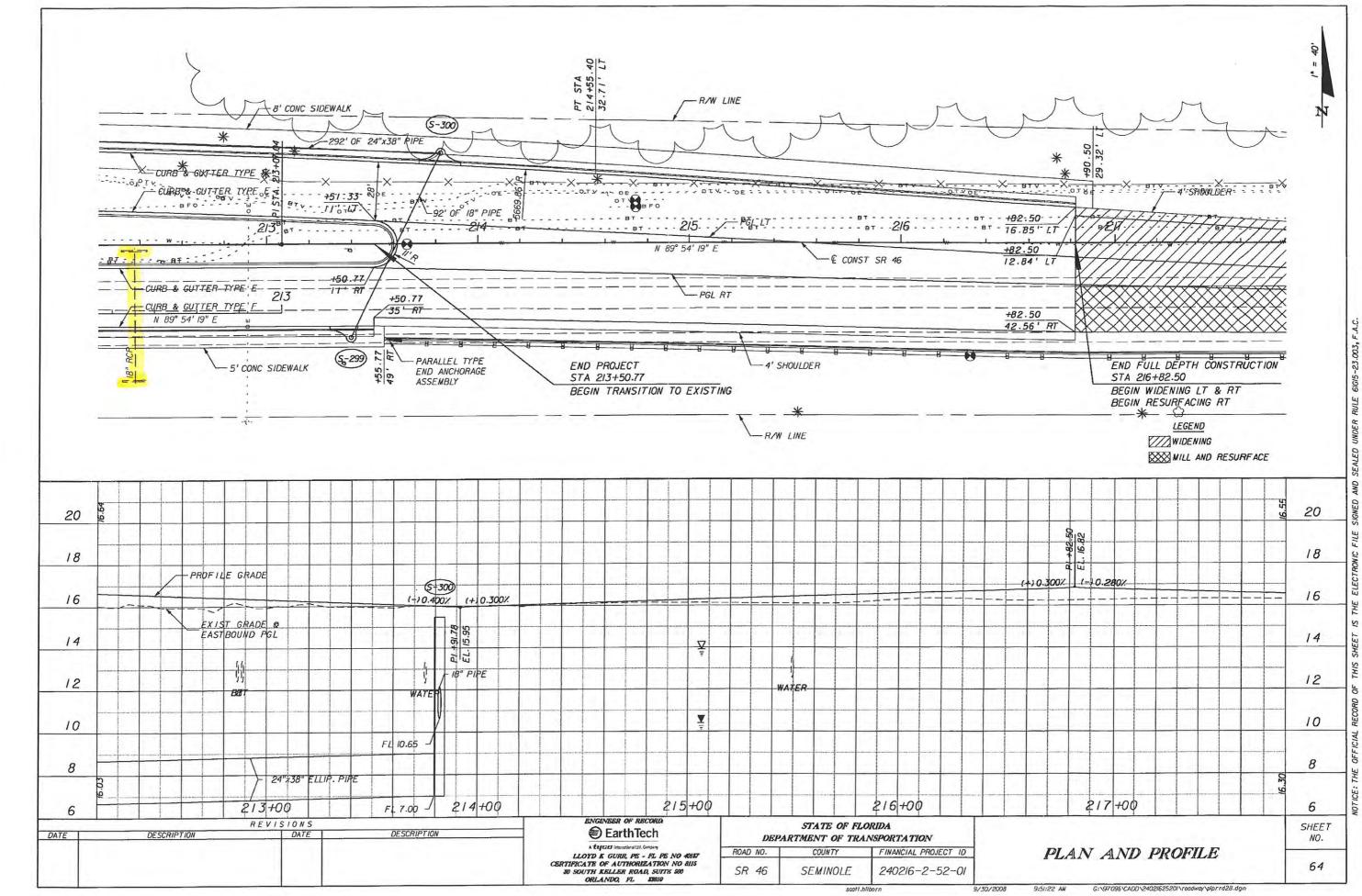
* From HY 8 culvert analysis

Note 1: Interpolated from Discharge vs Frequency graph (existing) Note 2: Values obtained from HY 8 model of existing Culvert

Note 3: Values obtained from HY 8 model of proposed extension Culvert

Proposed Culvert

No proposed Culvert, this culvert is scheduled for removal under FPID 240216-2-52-01 By Earthtech. No replacement Culvert has been shown in the proposed plans.



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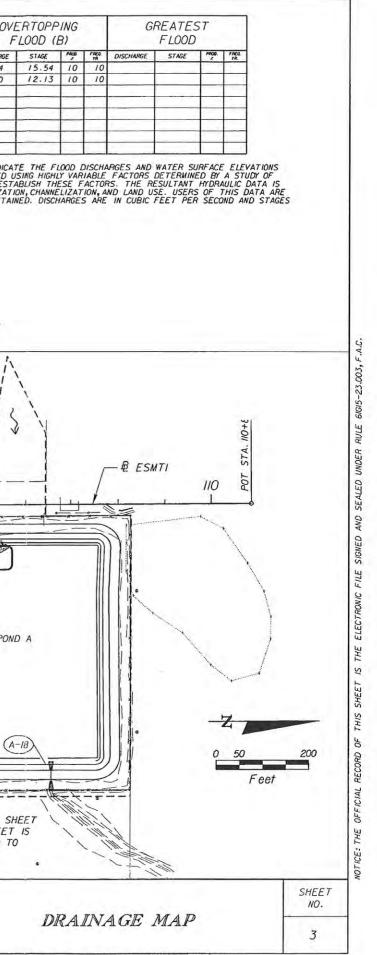
| | | | | | | | | DESIGN | FLOOD | BASE | FLOOD | OVE | ER |
|--------------------|---|--|---|---|------------|--|--------------------------|--------------------------------------|---|--|------------------------|---------------------------|---------|
| | EXISTING | DRAINAGE STRUCTURES | | | | STRUCTURE NO. | STATION | 2% PROB. | 50 YR.FREQ. | IZ PROB. | NO YR.FREQ. | F | LO |
| | | | | | | | 155.115 | DISCHARGE | STAGE | DISCHARGE | STAGE | DISCHARGE | S |
| | | | | | | CD-1 CD-2 | 466+15 | | | 100 | 15.77 | 104 | 1 |
| | METAL PIPE | (B) IB" RCP | (33) 24" RCP W INV 11.08 (HW | 1 | | 1 | | | 1 | 1.000 | | | |
| | IV 12.56 (HW) IV 10.72 (HW) | N INV 12.84 S INV 12.77 (MES) | E INV 10.85 (HV | | | - | | | | | | | - |
| (2) 36" | RCP | (19) 2 - 24" MES | | | | | | | - | | | | - |
| W II | W 11.19 (MES) W 10.27 (MES) | S INV 13.04 (W 15"RCP) S INV 13.01 (E 15"RCP) | (34) 18" RCP S INV 10.10 (ME. N INV 10.09 (ME | | | | | | | | | | |
| | RCP VV 11.11 (MES) VV 10.40 (MES) | 20 2 - 24" MES W INV 12.87 (N 15"RCP) | | | TH | HE HYDRAULIC HICH MAY BE HE WATERSHI INSITNE TO | ED. MANY J CHANGES, P | DGEMENTS | LY OF ANTE | ECEDENT CO | RE REQUIRE | ED TO ESTA URBANIZATIO | ABLIS |
| (4) 36" | | W INV 13.13 (S 15"RCP) | | | | NUTIONED AGA RE IN FEET, I <u>S:</u> | | ASSUMPTIO | N OF PREC | SISION WHICH | H CAN NOT | BE ATTAIN | VED. |
| | WV 10.38 (MES) | D STORM MH RIM 17.31 | | | DE | SIGN FLOOD: | | | | F.D.O.T. TANDARD L | | | |
| W II | RCP (ASSUMED AS 30" RCP) W 11.65 (MES) W 11.28 (MES) | N INV 13.12 (18"RCP) W INV 13.13 (N 24"RCP) W INV 13.17 (S 24"RCP) | | | | ASE FLOOD: ERTOPPING F | THE | FLOOD HA | ANY YEAR. II | CHANCE OF | QUENCY) | | |
| E // | 15" MES VV 11.43 (N 15"MES) | S INV 13.11 (W 24"RCP) S INV 13.11 (E 24"RCP) | | | | EATEST FLO | HIGH (C) T OD: THE | WAY (B) OVE HRU EMERO MOST SEV | ER A WATER GENCY RELIE VERE FLOOD | RSHED DIVI EF STRUCTO WHICH CA | DE OR URES. N BE | | |
| (7) DBI | W 11.53 (S 15"MES) | 22 18" MES N INV 13.62 | | | | | NORA | HALLY ONE | WITH A O.2 | OPPING IS 27. CHANCE 500 YR. FRE | OF BEING | ICABLE, | |
| GRA | TE 15.25 | | | | Ē | | 1 | 1 | | | | 1, | |
| W // E // | VV 11.53 (N 24"RCP) VV 11.51(S 24"RCP) VV 11.30 (N 15"RCP) VV 11.56 (S 15"RCP) | (23) 10'x3' CBC W INV 10.92 (HW) E INV 10.94 (HW) | | | | | <u>ـــــ</u> ــ | -' 2 | | | | /`` | 1 |
| N /A | IV 11.79 (15"RCP) | (24) 24" RCP | | | | MATCHL | NE STA. | 209+00 | | | | 12 | |
| (8) DBI | | W INV 12.08 (HW) E INV 11.59 (MES) | | | | | 40 | 15 | | | | 1 4 | 1 |
| | TE 15.95 IV 11.90 (15"RCP) | (25) 24" RCP | | | | D | | S-28 |) | 0 | \sim | 1 | |
| (9) 24" | MES | S INV 13.83 (MES) | | | | () T | | A-16 | <u>}</u> | (A-22) | A-17 | | |
| ~ N /N | IV 13.92 | N INV 13.40 (MES) | | | | 0 | | 12- | | -/ | 1 | ND D | _1_ |
| DBI GRA | TE 16.42 | 26 12" PVC | | | | | ille | Y | | | 2220 | 1=== | |
| | W 15.51 (24"RCP) | W INV 14.72 (MES) E INV 14.14 (MES) | | | | | FIII | A-23 |) (A | -21) | | - | |
| (1) 30" | | | | | | o | i- / / | 12 | | | 11 | Ű | |
| | W 11.86 (MES) W 12.10 (MES) | (27) 15" RCP S INV 14.07 (MES) | | | | | IM | | | 1 | 1/ | | |
| (12) 30" | RCP | N INV 14.04 (MES) | | | | | 124 | 1 | 1 | | / | | |
| W 11 | WV 11.68 (MES) WV 12.06 (MES) | 28 12" PVC | | | | į | 1 + 1 | 101 | Y, | | | | |
| (13) 30" | | W INV 14.75 (MES) E INV 13.91 (MES) | | | | | | 11 | 2 | 1 | | PONL | AC |
| W // | WV 11.76 (MES) | 0 | | | | | | Exi | 1 4 | | | | |
| E // | WV 12.12 (MES) | (29) DBI GRATE 16.47 | | | | | | 1.5 | Direk | | | | |
| E 11 | 24" MES VV 12.58 (N 24"RCP) VV 12.51 (S 24"RCP) | E INV 12.44 (12"PVC) 12"PVC OUTFALL, W INV 12.44 | | | | 1 | Ì | | * | 1 | | | |
| | | 30 8'x4' CBC | | | | | | | | | (A-19) | G | -18) |
| (15) 24" E | MES VV 14.11 (24"RCP) | W INV 7.41 (HW) E INV 6.96 (HW) | | | | | | İ. | (A- | 2011 | | C | |
| (16) DB1 | | (31) 18" RCP | | | | | 1 | | | | | | - |
| GRA | TE 16.49 W 15.46 (24"RCP) | S INV 13.40 (MES) N INV 12.54 (MES) | | | | | | NOTE: | | HE INFORM | ATION OF | I THIC CL | IFF |
| | | (32) 18" CMP | | | | | | FOR C | ONSTRUCT | ION PURP | OSES. TH | I THIS SH IS SHEET | IS |
| (17) 15" H N IN | RCP IV 12.66 (MES) | S INV 12.42 (MES) | | | | | j | ASSIST | CONSTR. | UCTION PL | | WITH | , |
| 5 /M | IV 12.63 (MES) | N INV 12.82 (MES) | | | | | | DRAIN | AGE CONCL | ERNS. | | | |
| BY | DESCRIPTION | REVISIONS DATE BY D | ESCRIPTION | IORIZON | | 0.00 | | TE OF FLO | | TION | | | |
| | | | | engineering group, inc. | - | ROAD NO. | ARTMEN | INTY | 1 | AL PROJECT | 10 | | |
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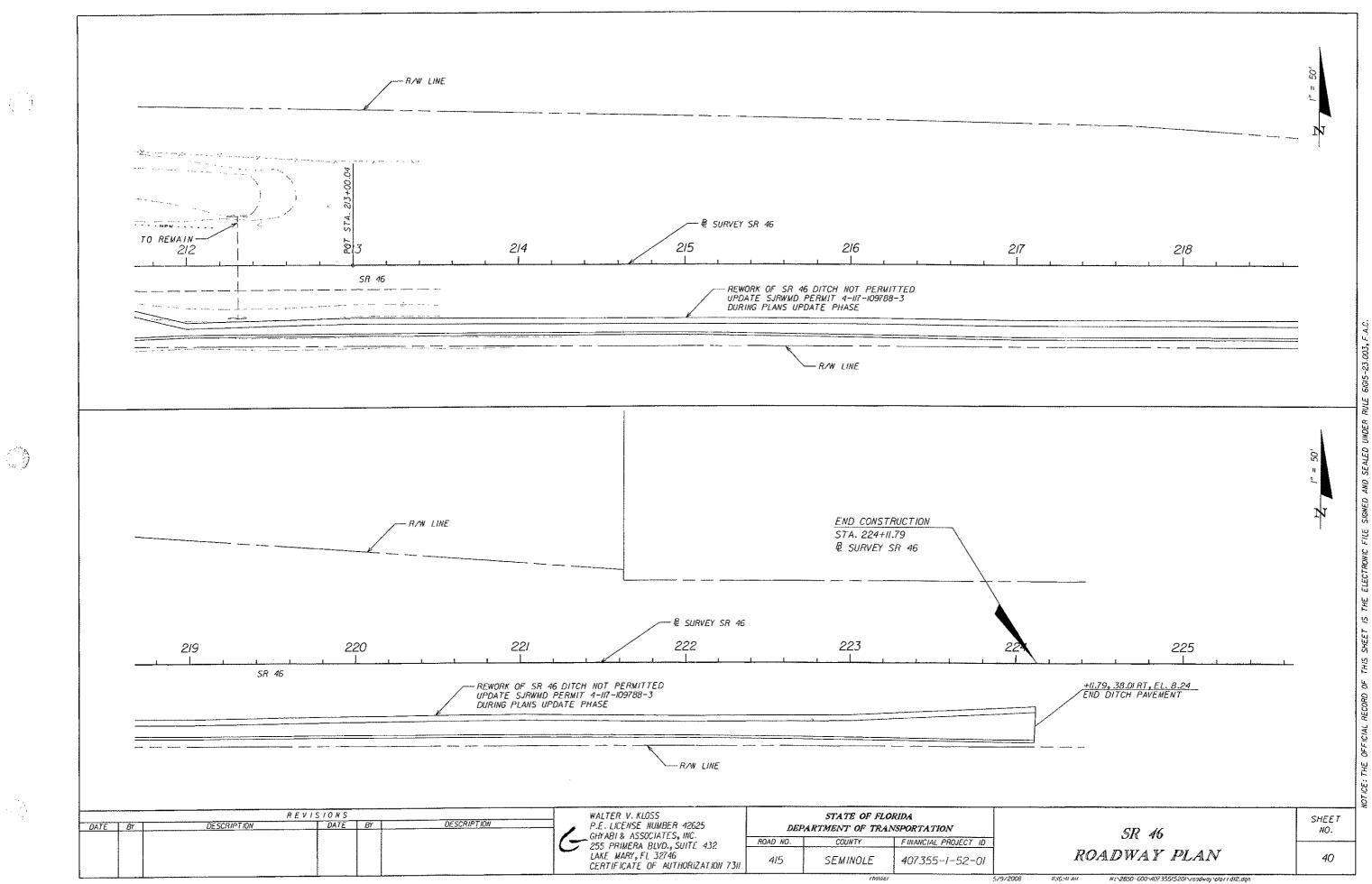
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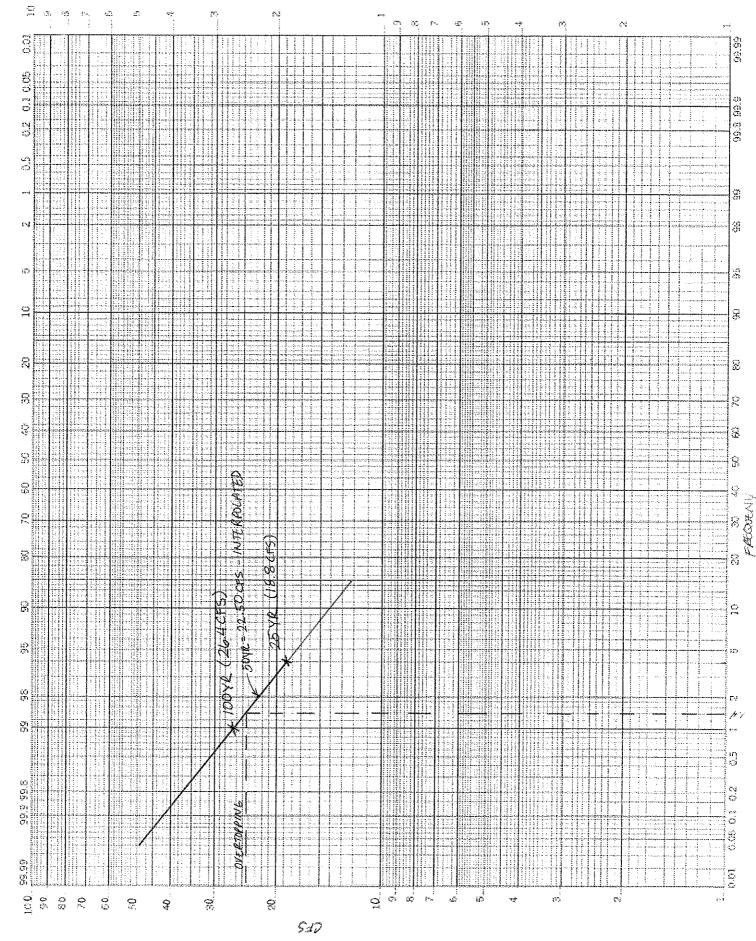
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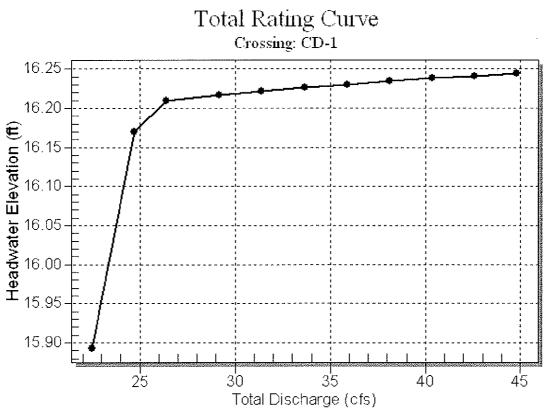
CD-1 2012-0453-02 194 (2016)

HY-8 Culvert Analysis Report CD-1 (Existing 24" RCP)

| Headwater Elevation (ft) | Total Discharge (cfs) | Culvert 1 Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------------------|-----------------------|------------------------------|----------------------------|------------|
| 15.89 | 22.50 | 22.50 | 0.00 | 1 |
| 16.17 | 24.73 | 23.99 | 0.00 | 50 |
| 16.21 | 26.40 | 24.20 | 1.96 | 12 |
| 16.22 | 29.19 | 24.24 | 4.71 | 4 |
| 16.22 | 31.42 | 24.26 | 7.05 | 4 |
| 16.23 | 33.65 | 24.28 | 9.15 | 3 |
| 16.23 | 35.88 | 24.30 | 11.39 | 3 |
| 16.23 | 38.11 | 24.32 | 13.65 | 3 |
| 16.24 | 40.34 | 24.34 | 15.90 | 3 |
| 16.24 | 42.57 | 24.36 | 18.14 | 3 |
| 16.24 | 44.80 | 24.38 | 20.04 | 2 |

Table 1 - Summary of Culvert Flows at Crossing: CD-1



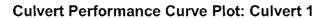


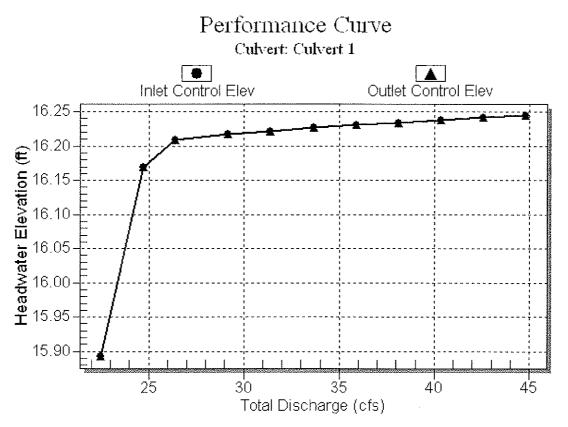
| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow ⊺ype | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (fVs) | Tailwater Velocity (ft/s) |
|-----------------------------|-------------------------------|--------------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|-----------------------------|---------------------------------|
| 22.50 | 22.50 | 15.89 | 3.333 | 3.333 | 5-S2n | 1.040 | 1.678 | 1,135 | 1.420 | 12,229 | 0.000 |
| 24.73 | 23.99 | 16.17 | 3.610 | 3.610 | 5-S2n | 1.081 | 1.722 | 1.181 | 1.420 | 12.423 | 0.000 |
| 26.40 | 24.20 | 16,21 | 3.649 | 3.649 | 5-S2n | 1.086 | 1.728 | 1.188 | 1.420 | 12.439 | 0.000 |
| 29.19 | 24.24 | 16.22 | 3.657 | 3.657 | 5-S2n | 1.088 | 1.730 | 1.190 | 1.420 | 12.444 | 0.000 |
| 31.42 | 24.26 | 16.22 | 3.662 | 3.662 | 5-S2n | 1.088 | 1.730 | 1.190 | 1.420 | 12.448 | 0.000 |
| 33.65 | 24.28 | 16.23 | 3.666 | 3.666 | 5-S2n | 1.089 | 1.731 | 1.191 | 1.420 | 12.451 | 0.000 |
| 35.88 | 24.30 | 16.23 | 3.670 | 3.670 | 5-S2n | 1,089 | 1.732 | 1.192 | 1.420 | 12.454 | 0.000 |
| 38.11 | 24.32 | 16.23 | 3.674 | 3.674 | 5-S2n | 1.090 | 1.732 | 1.192 | 1.420 | 12.457 | 0.000 |
| 40.34 | 24,34 | 16,24 | 3.678 | 3.678 | 5-S2n | 1.090 | 1.733 | 1.193 | 1.420 | 12.459 | 0.000 |
| 42.57 | 24.36 | 16.24 | 3.681 | 3.681 | 5-S2n | 1.091 | 1.733 | 1.193 | 1.420 | 12.462 | 0.000 |
| 44.80 | 24.38 | 16.24 | 3.684 | 3.684 | 5-S2n | 1.091 | 1.734 | 1.194 | 1.420 | 12.464 | 0.000 |

Table 2 - Culvert Summary Table: Culvert 1

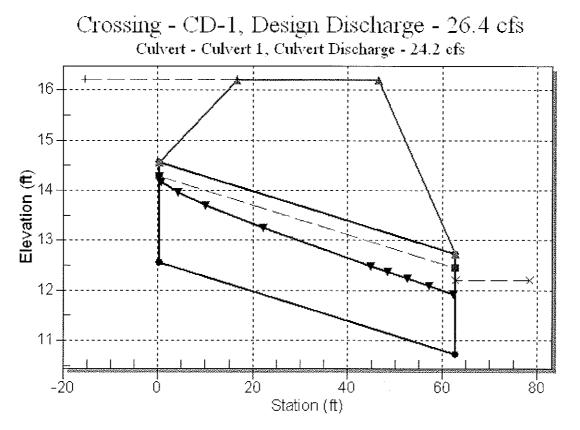
Inlet Elevation (invert): 12.56 ft, Outlet Elevation (invert): 10.72 ft

Culvert Length: 62.53 ft, Culvert Slope: 0.0294









Site Data - Culvert 1

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 12.56 ft Outlet Station: 62.50 ft Outlet Elevation: 10.72 ft Number of Barrels: 1

Culvert Data Summary - Culvert 1

Barrel Shape: Circular Barrel Diameter: 2.00 ft Barrel Material: Concrete Barrel Manning's n: 0.0120 Inlet Type: Conventional Inlet Edge Condition: Square Edge with Headwall Inlet Depression: None

Water Surface Elev (ft) Flow (cfs) Depth (ft) 22.50 12.20 1.42 12.20 24.73 1.42 26.40 12.20 1.42 29.19 12.20 1.42 31.42 12.20 1.42 33.65 12.20 1.42 35.88 12.20 1.42 38.11 12.20 1.42 12.20 40.34 1.42 42.57 12.20 1.42 44.80 12.20 1.42

Table 3 - Downstream Channel Rating Curve (Crossing: CD-1)

Tailwater Channel Data - CD-1

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 12.20 ft

Roadway Data for Crossing: CD-1

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 740.00 ft Crest Elevation: 16.20 ft Roadway Surface: Paved Roadway Top Width: 30.00 ft

| Project: | SR 46 PD&E Study (SR 415 to CR 426) | Design By: <u>DEP</u> | Date: | <u>8/7/2012</u> |
|----------|-------------------------------------|-----------------------|---------|-----------------|
| FIN No.: | 240216-4-28-01 | Checked by: ML | Date: 9 | 25/12 |
| Subject: | CD-2: 24" RCP (Sta 188+61.8) | | Dalo. (| - Ma |

Existing Culvert

Note: Based on the Record of Conversation document dated Feb. 7th, 2012 between URS and FDOT Maintenance Office (Jim Wood), there is no recorded history of flooding problems associated with CD-2. Based on the URS site visit conducted on Feb 12th, 2012 there are no apporent erosion problems. The existing concrete culvert has been lined with a plastic pipe insert to protect the roadway base due to leaks in the existing RCP joints. For the purpose of the PD&E Study, the existing culvert onalysis shall ignore the plastic pipe insert as our understanding is this was a temporary solution. Approximate historical drainage area is 33.79 acres per existing SR 46 Plans. Due ta no record of flooding, Velocity Method shall be used for the analysis.

| Method used: | Velocity (v) = | <u>6_ft/s</u> | (Since no | history of pro | blems is known) |
|-----------------------|---|------------------------------------|-----------|-------------------|--------------------------|
| Existing Information: | Culvert Diameter: No of culverts: Exist culvert length: | <u>2 ft</u> <u>1</u> 73.7 ft | | Material | : <u>RCP</u> |
| | Avge flowline elev upstream: | 13.70 | (NAVD) | (14.7 NGVD) | Per Existing SR 46 Plans |
| | Avge flowline elev downstream: | <u>13.00</u> - | (NAVD) | [14.0 NGVD] | Per Existing SR 46 Plans |
| | Longitudinal slope: | 0.009498 | = | <u>0.9498%</u> | |
| | Tailwater: | <u>15.00</u> | (NAVD) | <u>High Water</u> | Mark Stain on D/S End |
| | | | | (Approxime | <u>ately @ Crown)</u> |

Estimate discharge & Overtopping & HW for existing and proposed:

Area of culvert (A): <u>3.1 sq ft</u>

| Frequency | Factor | Q = A x v | HW Stage | HW Stage |
|-----------|--------|------------|----------|----------|
| | | | Existing | Proposed |
| | | | (Note 2) | (Note 3) |
| (yr) | | cu ft/s | | |
| 25 | | 18.8 | | |
| 50 | | 22.5 (Note | 17.05 | 15.92 |
| | | 1) | | |
| 100 | 1.4 | 26.4 | 17.21 | 16.27 |
| 500 | 1.7 | 44.8 | 17.24 | 17.22 |

Note 1: Interpolated from Discharge vs Frequency graph (existing) Note 2: Values obtained from HY 8 model of existing Culvert

Note 3: Values obtained from HY 8 model of proposed extension Culvert

Proposed Culvert

Note: Culvert Replacement to be 30" RCP

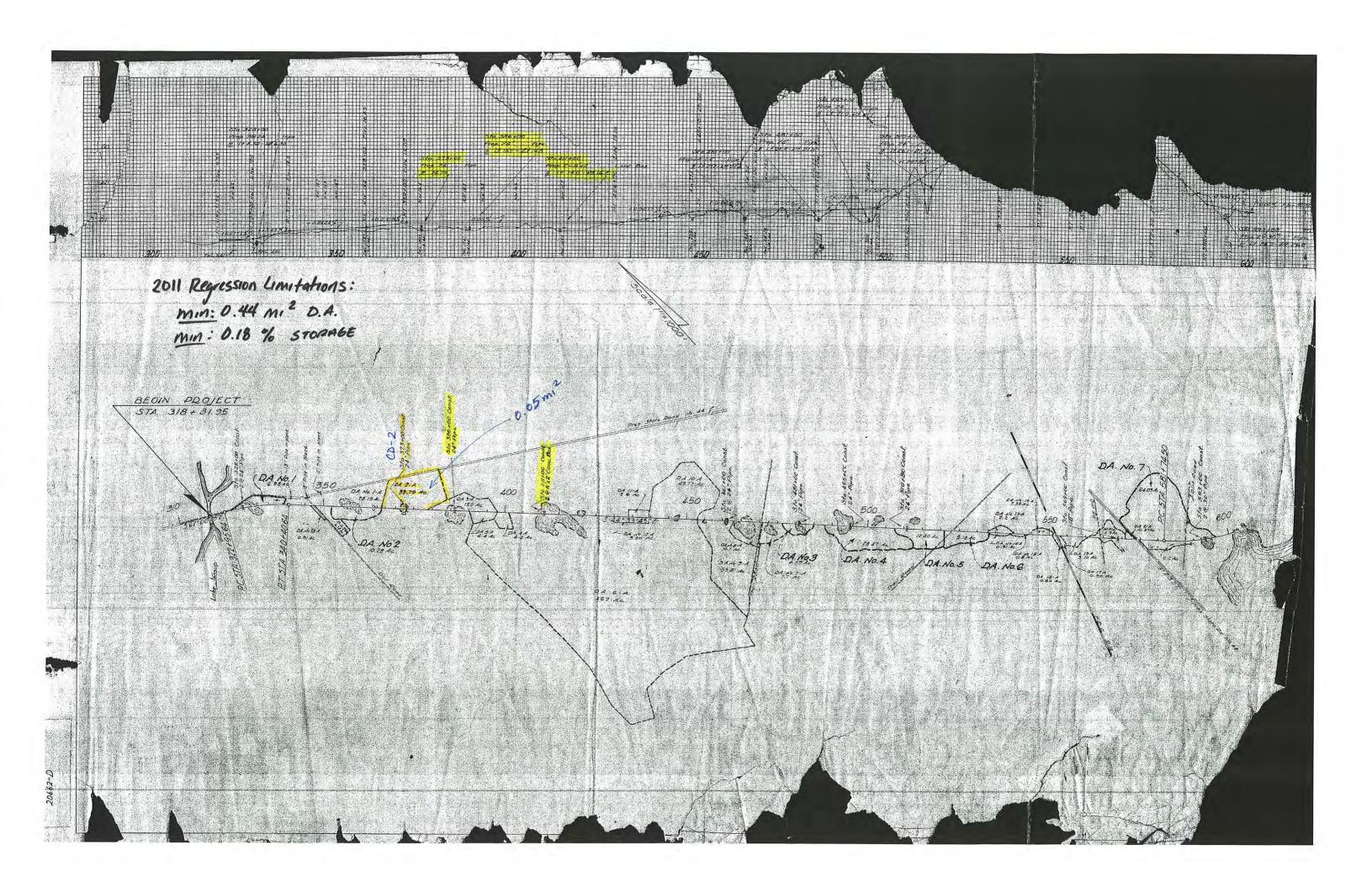
Assume allowable headwater (EOT) to be 6" below CL of Existing SR 46 = 16.70

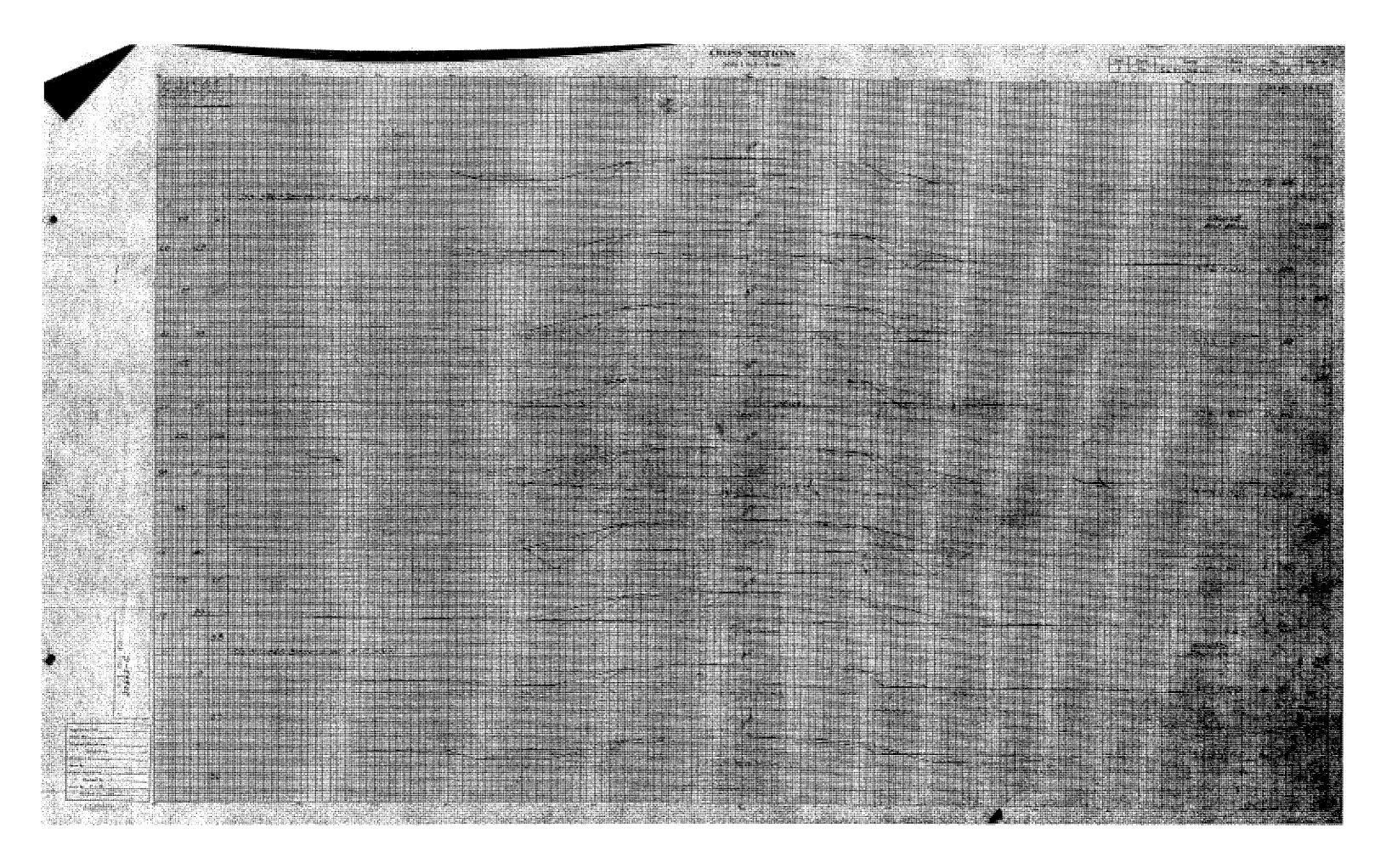
Proposed Information

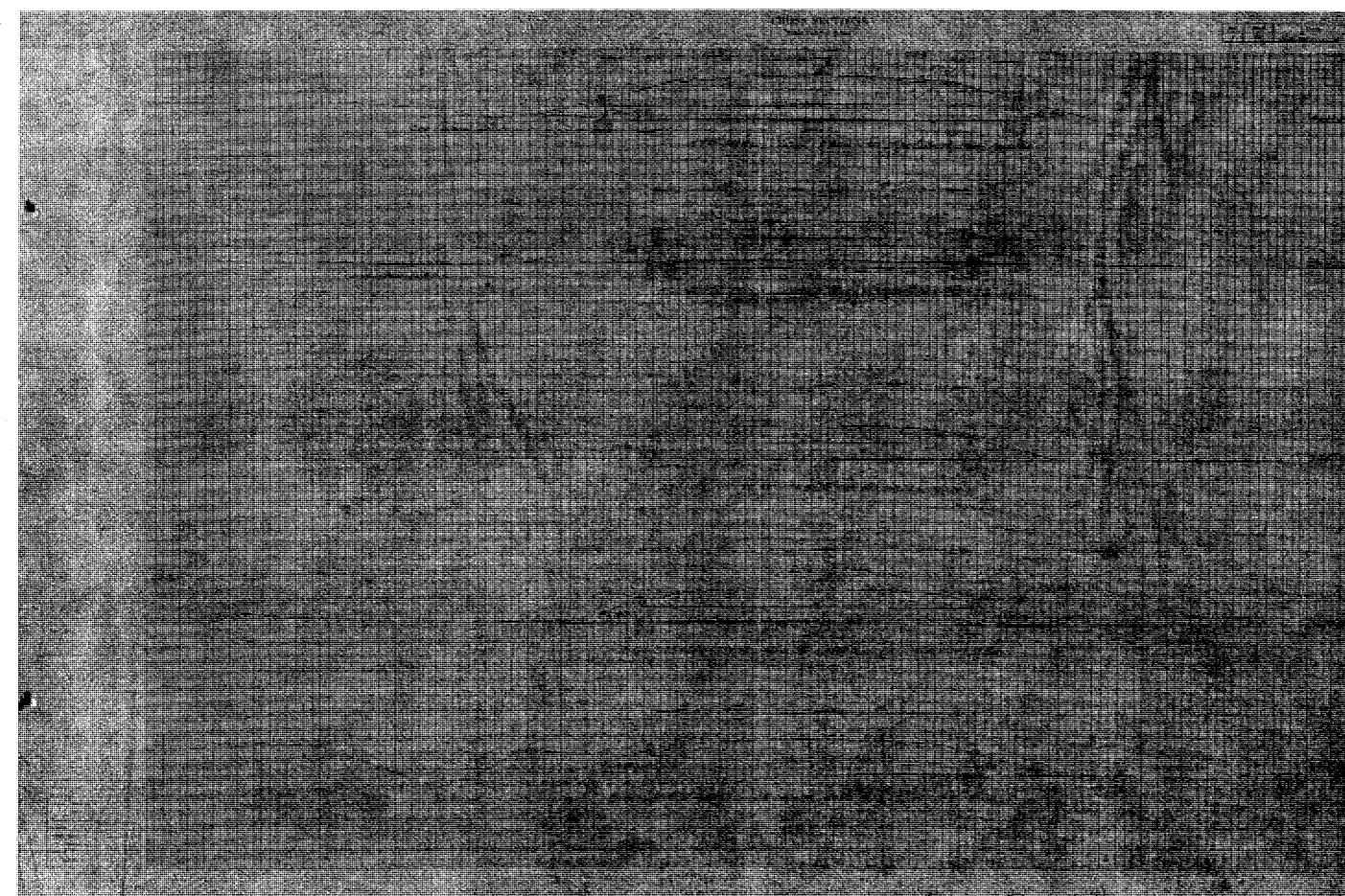
| | Extension | Invert |
|-----------------------------------|-----------|--------|
| | Length | (NAVD) |
| Upstream: | 49.9 ft | 13.20 |
| Downstream: | 46.4 ft | 12.50 |
| Total length of proposed culvert: | 170.0 ft | |

| | Overtopping | |
|-------------|-------------|----------|
| | | |
| | Existing | Proposed |
| Elev (NAVD) | 17.2 | 17.20 |
| Q* (cfs) | 23.3 | 34.74 |
| Freq (yr) | 59 | 364 |

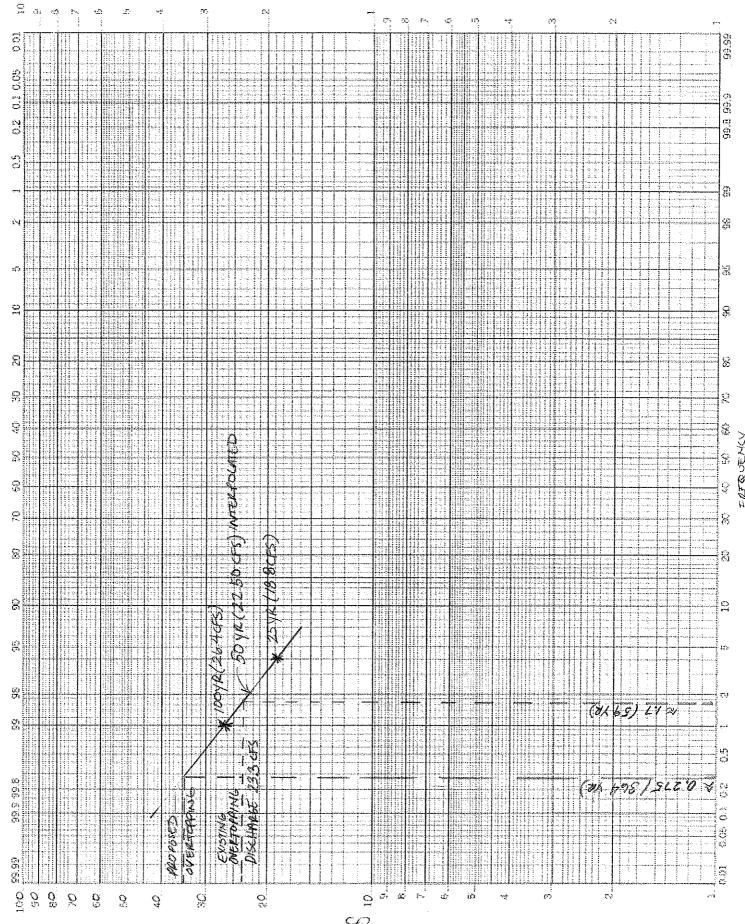
* From HY 8 culvert analysis









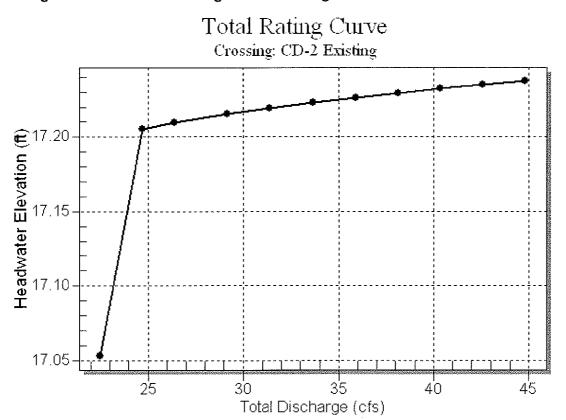


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HY-8 Culvert Analysis Report CD-2 (Existing 24" RCP)

| Headwater Elevation (ft) | Total Discharge (cfs) | CD-2 Existing Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------------------|-----------------------|----------------------------------|----------------------------|------------|
| 17.05 | 22.50 | 22.50 | 0.00 | 1 |
| 17.21 | 24.73 | 23.33 | 1.20 | 37 |
| 17.21 | 26.40 | 23.36 | 2.79 | 4 |
| 17.22 | 29.19 | 23.39 | 5.61 | 4 |
| 17.22 | 31.42 | 23.41 | 7.73 | 3 |
| 17.22 | 33.65 | 23.43 | 9.99 | 3 |
| 17.23 | 35.88 | 23.45 | 12.26 | 3 |
| 17.23 | 38.11 | 23.46 | 14.53 | 3 |
| 17.23 | 40.34 | 23.48 | 16.77 | 3 |
| 17.23 | 42.57 | 23.49 | 19.01 | 3 |
| 17.24 | 44.80 | 23.50 | 20.94 | 2 |

Table 1 - Summary of Culvert Flows at Crossing: CD-2 Existing



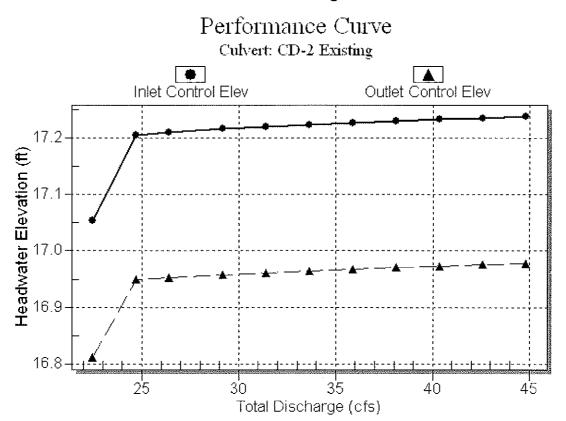
Rating Curve Plot for Crossing: CD-2 Existing

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (fl) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (fl) | Outlet Velocity (fl/s) | Tailwater Velocity (ft/s) |
|-----------------------------|-------------------------------|--------------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|------------------------------|---------------------------------|
| 22.50 | 22.50 | 17.05 | 3.353 | 3.112 | 4-FFf | 1.547 | 1.678 | 1.547 | 2.000 | 8.646 | 0,000 |
| 24.73 | 23.33 | 17.21 | 3.505 | 3.249 | 4-FFf | 1.597 | 1.703 | 1.597 | 2.000 | 8.680 | 0.000 |
| 26,40 | 23.36 | 17.21 | 3.510 | 3.253 | 4-FFf | 1.598 | 1.704 | 1.598 | 2.000 | 8.681 | 0.000 |
| 29.19 | 23.39 | 17.22 | 3.515 | 3.258 | 4-FFf | 1.600 | 1.705 | 1.600 | 2.000 | 8.682 | 0.000 |
| 31.42 | 23.41 | 17.22 | 3.519 | 3.262 | 4-FFf | 1.601 | 1.705 | 1.601 | 2.000 | 8.680 | 0.000 |
| 33.65 | 23.43 | 17,22 | 3.523 | 3.265 | 4-FFf | 1.603 | 1.706 | 1.603 | 2.000 | 8.677 | 0.000 |
| 35.88 | 23.45 | 17.23 | 3.526 | 3.268 | 4-FFf | 1.605 | 1.706 | 1.605 | 2.000 | 8.675 | 0.000 |
| 38.11 | 23.46 | 17.23 | 3.529 | 3.271 | 4-FFf | 1.606 | 1.707 | 1.606 | 2.000 | 8.672 | 0.000 |
| 40.34 | 23.48 | 17.23 | 3.532 | 3.273 | 4-FFf | 1.608 | 1.707 | 1.608 | 2.000 | 8.670 | 0.000 |
| 42.57 | 23.49 | 17.23 | 3,535 | 3.276 | 4-FFf | 1.609 | 1.708 | 1.609 | 2.000 | 8.667 | 0.000 |
| 44.80 | 23.50 | 17.24 | 3.537 | 3.278 | 4-FFf | 1.611 | 1.708 | 1.611 | 2.000 | 8.665 | 0,000 |

Table 2 - Culvert Summary Table: CD-2 Existing

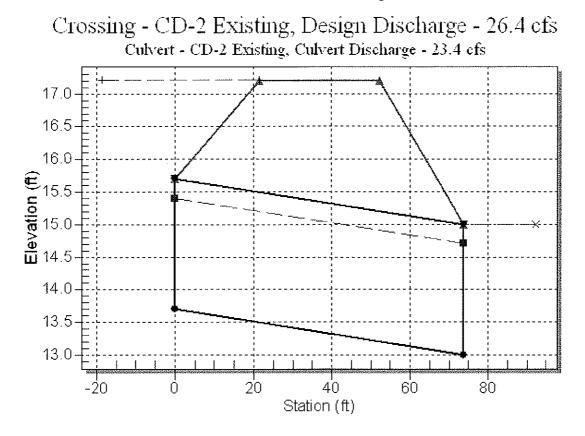
Inlet Elevation (invert): 13.70 ft, Outlet Elevation (invert): 13.00 ft

Culvert Length: 73.70 ft, Culvert Slope: 0.0095



Culvert Performance Curve Plot: CD-2 Existing

Water Surface Profile Plot for Culvert: CD-2 Existing



Site Data - CD-2 Existing

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 13.70 ft Outlet Station: 73.70 ft Outlet Elevation: 13.00 ft Number of Barrels: 1

Culvert Data Summary - CD-2 Existing

Barrel Shape: Circular Barrel Diameter: 2.00 ft Barrel Material: Concrete Barrel Manning's n: 0.0120 Inlet Type: Conventional Inlet Edge Condition: Square Edge with Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-2 Existing)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
|------------|-------------------------|------------|
| 22.50 | 15.00 | 2.00 |
| 24.73 | 15.00 | 2.00 |
| 26.40 | 15.00 | 2.00 |
| 29.19 | 15.00 | 2.00 |
| 31.42 | 15.00 | 2.00 |
| 33.65 | 15.00 | 2.00 |
| 35.88 | 15.00 | 2.00 |
| 38.11 | 15.00 | 2.00 |
| 40.34 | 15.00 | 2.00 |
| 42.57 | 15.00 | 2.00 |
| 44.80 | 15.00 | 2.00 |

Tailwater Channel Data - CD-2 Existing

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 15.00 ft

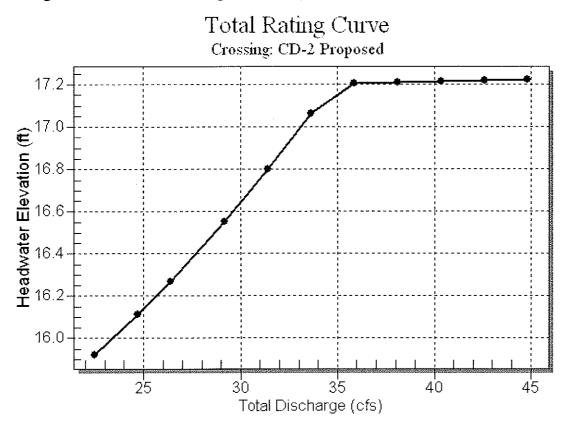
Roadway Data for Crossing: CD-2 Existing

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 1000.00 ft Crest Elevation: 17.20 ft Roadway Surface: Paved Roadway Top Width: 31.00 ft HY-8 Culvert Analysis Report CD-2 (Proposed 30" RCP)

| Headwater Elevation (ft) | Total Discharge (cfs) | CD-2 Proposed Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------------------|-----------------------|----------------------------------|----------------------------|------------|
| 15.92 | 22.50 | 22.50 | 0.00 | 1 |
| 16,11 | 24.73 | 24.73 | 0.00 | 1 |
| 16.27 | 26.40 | 26.40 | 0.00 | 1 |
| 16.55 | 29.19 | 29.19 | 0.00 | 1 |
| 16.80 | 31.42 | 31.42 | 0.00 | 1 |
| 17.06 | 33.65 | 33.65 | 0.00 | 1 |
| 17.20 | 35.88 | 34.78 | 0.85 | 39 |
| 17.21 | 38.11 | 34.82 | 2.95 | 4 |
| 17.21 | 40.34 | 34.86 | 5.30 | 4 |
| 17.22 | 42.57 | 34.89 | 7.39 | 3 |
| 17.22 | 44.80 | 34.92 | 9.64 | 3 |

Table 1 - Summary of Culvert Flows at Crossing: CD-2 Proposed



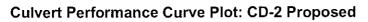


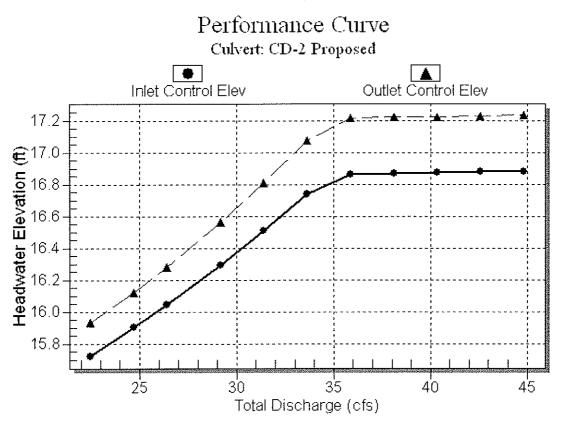
| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | iniet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (fl) | Critical Depth (fl) | Outlet Depth (fl) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
|-----------------------------|-------------------------------|--------------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|------------------------------|---------------------------------|
| 22.50 | 22.50 | 15.92 | 2,515 | 2.723 | 4-FFf | 1.675 | 1.608 | 2.500 | 2.500 | 4.584 | 0.000 |
| 24.73 | 24.73 | 16.11 | 2.694 | 2.915 | 4-FFf | 1.800 | 1,690 | 2,500 | 2.500 | 5.038 | 0.000 |
| 26.40 | 26.40 | 16.27 | 2.835 | 3.070 | 4-FFf | 1.905 | 1.751 | 2.500 | 2.500 | 5.378 | 0.000 |
| 29.19 | 29.19 | 16.55 | 3.085 | 3.353 | 4-FFf | 2.125 | 1.835 | 2.500 | 2.500 | 5.947 | 0.000 |
| 31.42 | 31.42 | 16.80 | 3.301 | 3.599 | 4-FFf | 2.500 | 1.902 | 2.500 | 2.500 | 6.401 | 0.000 |
| 33.65 | 33.65 | 17.06 | 3.533 | 3.864 | 4-FFf | 2.500 | 1.970 | 2.500 | 2.500 | 6.855 | 0.000 |
| 35.88 | 34.78 | 17.20 | 3.656 | 4.004 | 4-FFf | 2.500 | 2.002 | 2.500 | 2.500 | 7.084 | 0.000 |
| 38.11 | 34.82 | 17.21 | 3.661 | 4.010 | 4-FFf | 2.500 | 2.003 | 2.500 | 2.500 | 7.094 | 0.000 |
| 40.34 | 34.86 | 17.21 | 3.665 | 4.015 | 4-FFf | 2,500 | 2.004 | 2.500 | 2.500 | 7.101 | 0.000 |
| 42.57 | 34.89 | 17.22 | 3.669 | 4.019 | 4-FFf | 2.500 | 2.005 | 2.500 | 2,500 | 7,107 | 0.000 |
| 44.80 | 34,92 | 17.22 | 3,672 | 4.022 | 4-FFf | 2.500 | 2.005 | 2.500 | 2.500 | 7.113 | 0.000 |

Table 2 - Culvert Summary Table: CD-2 Proposed

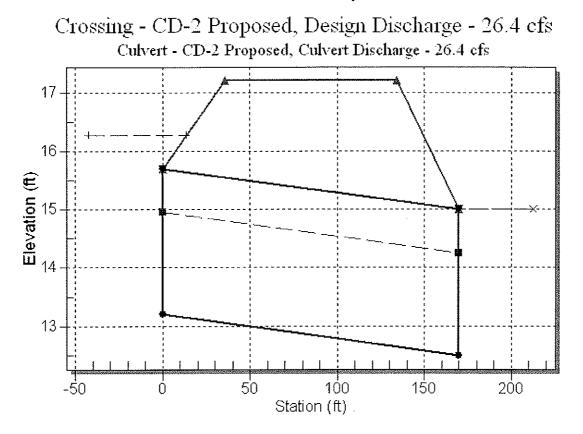
Inlet Elevation (invert): 13.20 ft, Outlet Elevation (invert): 12.50 ft

Culvert Length: 170.00 ft, Culvert Slope: 0.0041





Water Surface Profile Plot for Culvert: CD-2 Proposed



Site Data - CD-2 Proposed

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 13.20 ft Outlet Station: 170.00 ft Outlet Elevation: 12.50 ft Number of Barrels: 1

Culvert Data Summary - CD-2 Proposed

Barrel Shape: Circular Barrel Diameter: 2.50 ft Barrel Material: Concrete Barrel Manning's n: 0.0120 Inlet Type: Conventional Inlet Edge Condition: Square Edge with Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-2 Proposed)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
|------------|-------------------------|------------|
| 22.50 | 15.00 | 2.50 |
| 24.73 | 15.00 | 2.50 |
| 26.40 | 15.00 | 2,50 |
| 29.19 | 15.00 | 2.50 |
| 31.42 | 15.00 | 2.50 |
| 33.65 | 15.00 | 2.50 |
| 35.88 | 15.00 | 2.50 |
| 38.11 | 15.00 | 2.50 |
| 40.34 | 15.00 | 2.50 |
| 42.57 | 15.00 | 2.50 |
| 44.80 | 15.00 | 2.50 |

Tailwater Channel Data - CD-2 Proposed

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 15.00 ft

Roadway Data for Crossing: CD-2 Proposed

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 1000.00 ft Crest Elevation: 17.20 ft Roadway Surface: Paved Roadway Top Width: 98.00 ft

| Project: | SR 46 PD&E Study (SR 415 to CR 426) | Design By: DEP | Date: | 8/6/2012 |
|----------|-------------------------------------|-----------------|---------|----------|
| FIN No.: | 240216-4-28-01 | Checked by: NTL | Date: 9 | 2515 |
| Subject: | CD-3: 24" RCP (Sta 201+60.80) | | Dalo. | 112 |

Existing Culvert

Note: Based on the Record of Conversation document dated Feb. 7th, 2012 between URS and FDOT Maintenance Office (Jim Wood), there is no recorded history of flooding problems associated with CD-3. Based on the URS site visit conducted on Feb. 12th, 2012 there are no apparent erosion problems. The pipe was halfway submerged and was heavily vegetated with aquatic vegetation and maintenance clipping waste. The existing concrete culvert has been lined with a plastic pipe insert to protect the roadway base due to leaks in the existing RCP joints. For the purpose of the PD&E Study, the existing culvert analysis shall ignore the plastic pipe insert as our understanding is this was a temporary solution. Approximate historical drainage area is 13 acres per existing SR 46 Plans. Due to no record of flooding, Velocity Method shall be used for the analysis.

| Method used: | Velocity (v) = | <u>6 ft/s</u> ` | (Since no | history of problems is known) |
|-----------------------|---|---|------------------|--|
| Existing Information: | Culvert Diameter: No of culverts: Exist culvert length: Avge flowline elev upstream: Avge flowline elev downstream: | <u>2 ft</u> <u>1</u> <u>74.0 ft</u> <u>14.00</u> <u>13.80</u> | (NAVD) (NAVD) | Material: <u>RCP</u> (15.0 NGVD) Per Existing SR 46 Plans (14.8 NGVD) Per Existing SR 46 Plans |
| | Longitudinal slope: Tailwater: | 0.002703 <u>16.13</u> | = (NAVD) | <u>0.2703%</u> <u>High Water Mark Stain on D/S End</u> (Approximately 4" above Crown) |

3.1 sq ft

Estimate discharge & Overtopping & HW for existing and proposed:

Area of culvert (A):

| Frequency | Factor | Q = A x v | HW Stage | HW Stage |
|-----------|--------|------------|----------|----------|
| | | | Existing | Proposed |
| | | | (Note 2) | (Note 3) |
| (yr) | | cu ft/s | | |
| 25 | | 18.8 | | |
| 50 | | 22.5 (Note | 17.94 | 17.05 |
| | | 1) | | |
| 100 | 1.4 | 26.4 | 18.01 | 17.40 |
| 500 | 1.7 | 44.8 | 18.04 | 18.03 |

Note 1: Interpolated from Discharge vs Frequency graph (existing) Note 2: Values obtained from HY 8 model of existing CBC

Note 3: Values obtained from HY 8 model of proposed extension CBC

Proposed Culvert

Note: Culvert Replacement to be 30" RCP

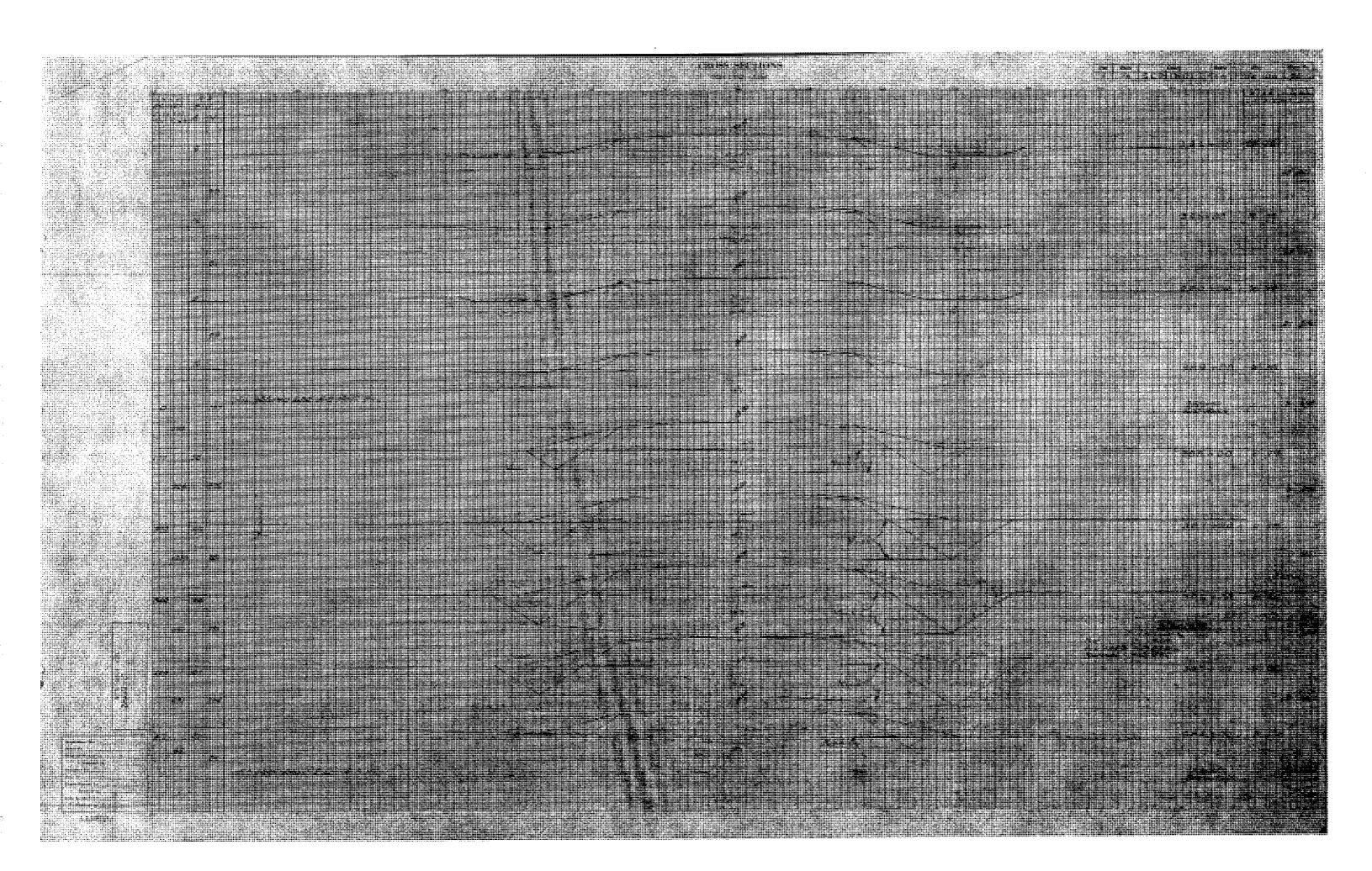
Assume allowable headwater (EOT) to be 6" below CL of Existing SR 46 = 17.5

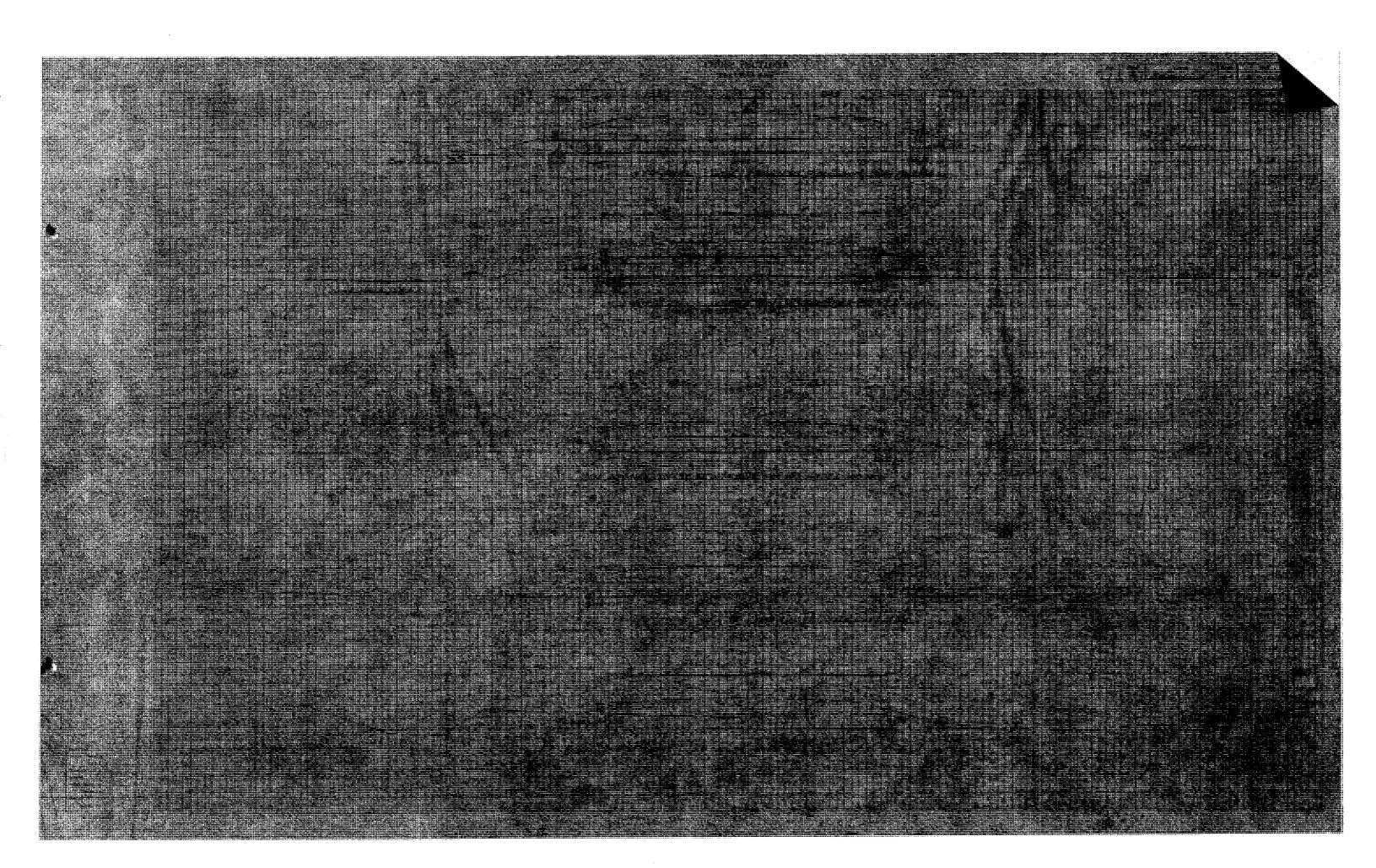
Proposed Information

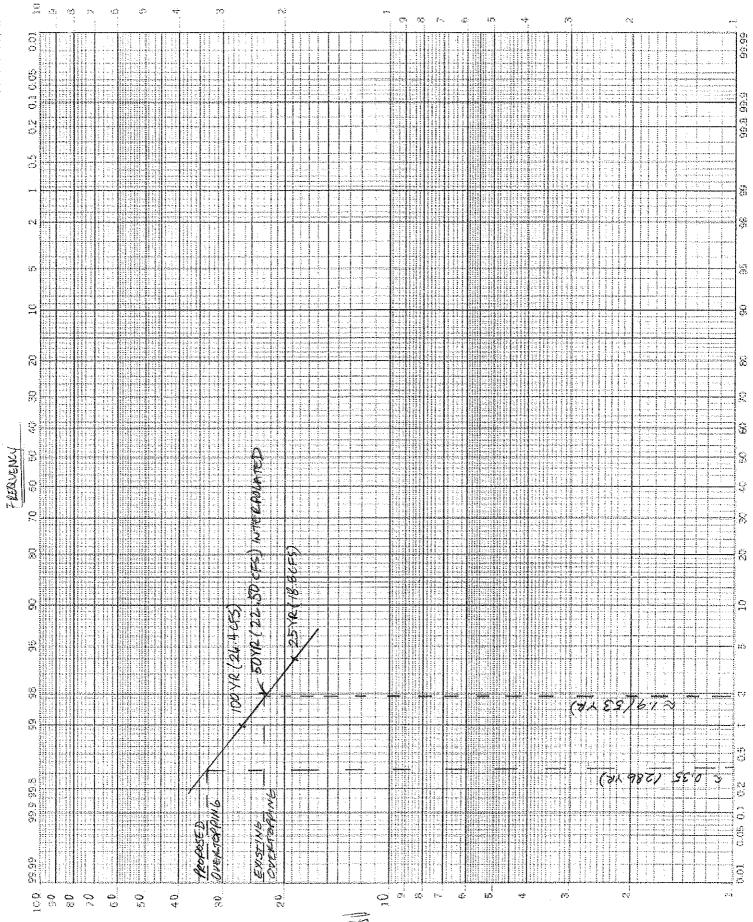
| | Extension | Invert |
|-----------------------------------|-----------|--------|
| | Length | (NAVD) |
| Upstream: | 80.0 ft | 13.50 |
| Downstream: | 16.0 ft | 13.30 |
| Total length of proposed culvert: | | |

| Overtopping | | | | | |
|-------------|----------|----------|--|--|--|
| | Existing | Proposed | | | |
| Elev (NAVD) | 18.00 | 18.00 | | | |
| Q* (cfs) | 22.84 | 32.03 | | | |
| Freq (yr) | 53 | 286 | | | |

* From HY 8 culvert analysis







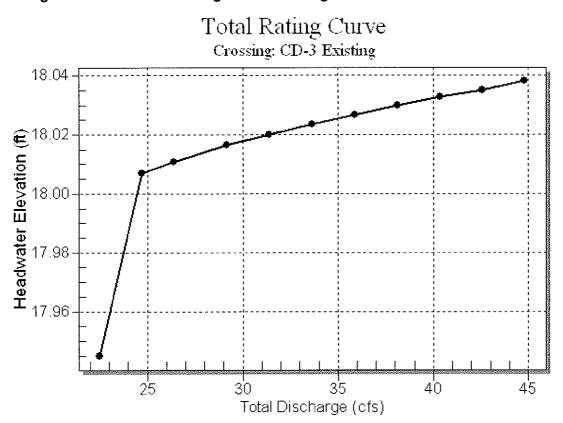
5.40

20-3 20-3

HY-8 Culvert Analysis Report CD-3 (Existing 24" RCP)

| Headwater Elevation (ft) | Total Discharge (cfs) | CD-3 Existing Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------------------|-----------------------|----------------------------------|----------------------------|------------|
| 17.94 | 22.50 | 22.50 | 0.00 | 1 |
| 18.01 | 24.73 | 22.88 | 1.71 | 20 |
| 18.01 | 26.40 | 22.90 | 3.30 | 4 |
| 18.02 | 29.19 | 22.94 | 6.09 | 4 |
| 18.02 | 31.42 | 22.96 | 8.20 | 3 |
| 18.02 | 33.65 | 22.98 | 10.45 | 3 |
| 18.03 | 35.88 | 23.00 | 12.72 | 3 |
| 18.03 | 38.11 | 23.02 | 14.98 | 3 |
| 18.03 | 40.34 | 23.04 | 17.22 | 3 |
| 18.04 | 42.57 | 23.05 | 19.11 | 2 |
| 18.04 | 44.80 | 23.07 | 21.65 | 3 |

Table 1 - Summary of Culvert Flows at Crossing: CD-3 Existing



Rating Curve Plot for Crossing: CD-3 Existing

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Iniet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ff) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
|-----------------------------|-------------------------------|--------------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|------------------------------|---------------------------------|
| 22.50 | 22.50 | 17.94 | 3.360 | 3.945 | 4-FFf | 2.000 | 1.678 | 2.000 | 2.330 | 7.162 | 0.000 |
| 24.73 | 22.88 | 18.01 | 3.429 | 4.007 | 4-FFf | 2,000 | 1.690 | 2,000 | 2.330 | 7.283 | 0.000 |
| 26.40 | 22.90 | 18.01 | 3.433 | 4.011 | 4-FFf | 2.000 | 1.690 | 2.000 | 2.330 | 7.291 | 0,000 |
| 29.19 | 22.94 | 18.02 | 3.439 | 4.016 | 4-FFf | 2.000 | 1.691 | 2.000 | 2.330 | 7.301 | 0.000 |
| 31.42 | 22.96 | 18.02 | 3.443 | 4.020 | 4-FFf | 2.000 | 1.692 | 2.000 | 2.330 | 7.308 | 0.000 |
| 33.65 | 22,98 | 18.02 | 3.447 | 4.023 | 4-FFf | 2.000 | 1.693 | 2,000 | 2.330 | 7.315 | 0.000 |
| 35.88 | 23.00 | 18.03 | 3.451 | 4.027 | 4-FFf | 2.000 | 1.693 | 2.000 | 2.330 | 7.322 | 0.000 |
| 38.11 | 23.02 | 18.03 | 3.454 | 4.030 | 4-FFf | 2.000 | 1.694 | 2.000 | 2.330 | 7.327 | 0.000 |
| 40.34 | 23.04 | 18.03 | 3.457 | 4.033 | 4-FFf | 2.000 | 1.694 | 2.000 | 2.330 | 7.333 | 0.000 |
| 42.57 | 23.05 | 18.04 | 3.460 | 4.035 | 4-FFf | 2.000 | 1.695 | 2.000 | 2.330 | 7.338 | 0.000 |
| 44.80 | 23.07 | 18.04 | 3.463 | 4.038 | 4-FFf | 2.000 | 1.695 | 2.000 | 2.330 | 7.343 | 0.000 |

Table 2 - Culvert Summary Table: CD-3 Existing

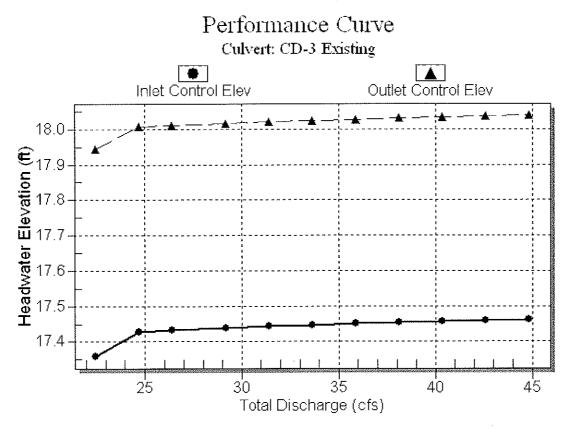
4

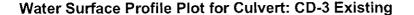
Inlet Elevation (invert): 14.00 ft, Outlet Elevation (invert): 13.80 ft

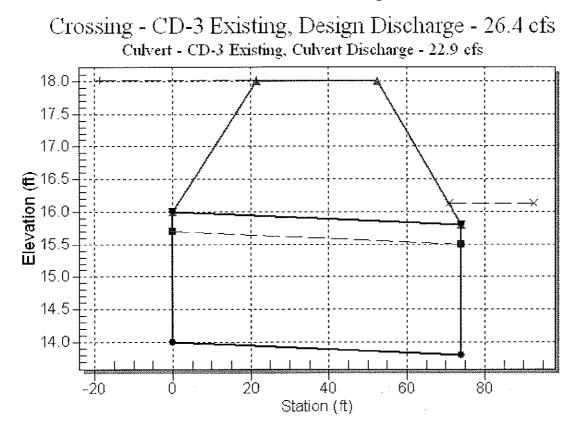
. .

Culvert Length: 74.00 ft, Culvert Slope: 0.0027









Site Data - CD-3 Existing

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 14.00 ft Outlet Station: 74.00 ft Outlet Elevation: 13.80 ft Number of Barrels: 1

Culvert Data Summary - CD-3 Existing

Barrel Shape: Circular Barrel Diameter: 2.00 ft Barrel Material: Concrete Barrel Manning's n: 0.0120 Inlet Type: Conventional Inlet Edge Condition: Square Edge with Headwall Inlet Depression: None

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
|------------|-------------------------|------------|
| 22.50 | 16.13 | 2.33 |
| 24.73 | 16.13 | 2.33 |
| 26.40 | 16.13 | 2.33 |
| 29.19 | 16.13 | 2.33 |
| 31.42 | 16.13 | 2.33 |
| 33.65 | 16.13 | 2.33 |
| 35.88 | 16.13 | 2.33 |
| 38.11 | 16.13 | 2.33 |
| 40.34 | 16.13 | 2.33 |
| 42.57 | 16.13 | 2.33 |
| 44.80 | 16.13 | 2.33 |

Table 3 - Downstream Channel Rating Curve (Crossing: CD-3 Existing)

Tailwater Channel Data - CD-3 Existing

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 16.13 ft

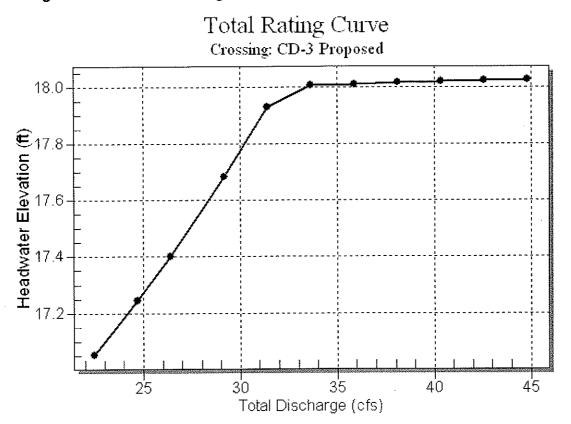
Roadway Data for Crossing: CD-3 Existing

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 1000.00 ft Crest Elevation: 18.00 ft Roadway Surface: Paved Roadway Top Width: 31.00 ft HY-8 Culvert Analysis Report CD-3 (Proposed 30" RCP)

| Headwater Elevation (ft) | Total Discharge (cfs) | CD-3 Proposed Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------------------|-----------------------|----------------------------------|----------------------------|------------|
| 17.05 | 22.50 | 22.50 | 0.00 | 1 |
| 17.24 | 24.73 | 24.73 | 0.00 | 1 |
| 17.40 | 26.40 | 26.40 | 0.00 | 1 |
| 17.68 | 29.19 | 29.19 | 0.00 | 1 |
| 17.93 | 31.42 | 31.42 | 0.00 | 1 |
| 18.01 | 33.65 | 32.08 | 1.28 | 23 |
| 18.01 | 35.88 | 32.13 | 3.46 | 4 |
| 18.02 | 38.11 | 32.17 | 5.79 | 4 |
| 18.02 | 40.34 | 32.20 | 7.88 | 3 |
| 18.02 | 42.57 | 32.23 | 10.12 | 3 |
| 18.03 | 44.80 | 32.25 | 12.38 | 3 |

Table 1 - Summary of Culvert Flows at Crossing: CD-3 Proposed



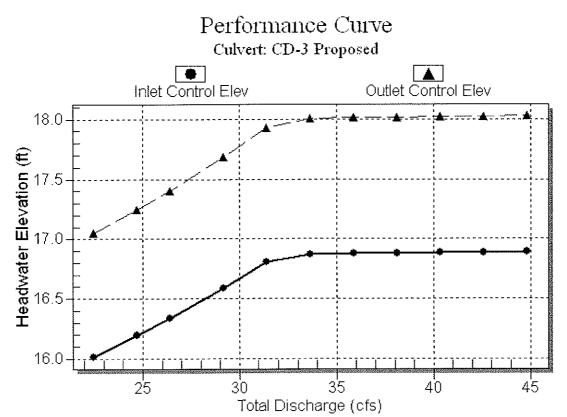


| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (fl/s) | Tailwater Velocity (ft/s) |
|-----------------------------|-------------------------------|--------------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|------------------------------|---------------------------------|
| 22.50 | 22.50 | 17.05 | 2.518 | 3.553 | 4-FFf | 2.500 | 1.608 | 2.500 | 2.330 | 4.584 | 0.000 |
| 24,73 | 24.73 | 17.24 | 2.698 | 3.745 | 4-FFf | 2.500 | 1.690 | 2.500 | 2.330 | 5.038 | 0.000 |
| 26.40 | 26.40 | 17.40 | 2.839 | 3.900 | 4-FFf | 2.500 | 1.751 | 2.500 | 2.330 | 5.378 | 0.000 |
| 29.19 | 29.19 | 17.68 | 3.089 | 4.183 | 4-FFf | 2.500 | 1.835 | 2.500 | 2.330 | 5.947 | 0.000 |
| 31.42 | 31.42 | 17.93 | 3,305 | 4.429 | 4-FFf | 2.500 | 1.902 | 2.500 | 2.330 | 6.401 | 0.000 |
| 33.65 | 32.08 | 18.01 | 3.372 | 4.506 | 4-FFf | 2.500 | 1.922 | 2.500 | 2.330 | 6.535 | 0.000 |
| 35.88 | 32.13 | 18.01 | 3.376 | 4.511 | 4-FFf | 2.500 | 1.924 | 2.500 | 2.330 | 6.545 | 0.000 |
| 38.11 | 32.17 | 18.02 | 3.381 | 4.516 | 4-FFf | 2.500 | 1.925 | 2.500 | 2.330 | 6,553 | 0.000 |
| 40.34 | 32.20 | 18.02 | 3.384 | 4.519 | 4-FFf | 2.500 | 1.926 | 2.500 | 2.330 | 6.559 | 0.000 |
| 42,57 | 32.23 | 18.02 | 3.387 | 4.523 | 4-FFf | 2.500 | 1.927 | 2.500 | 2.330 | 6.565 | 0.000 |
| 44.80 | 32.25 | 18.03 | 3.390 | 4.526 | 4-FFf | 2.500 | 1.928 | 2.500 | 2.330 | 6,571 | 0.000 |

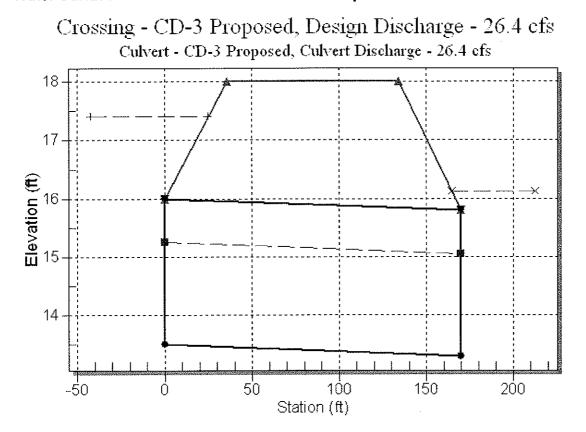
Table 2 - Culvert Summary Table: CD-3 Proposed

Inlet Elevation (invert): 13.50 ft, Outlet Elevation (invert): 13.30 ft

Culvert Length: 170.00 ft, Culvert Slope: 0.0012



Culvert Performance Curve Plot: CD-3 Proposed



Water Surface Profile Plot for Culvert: CD-3 Proposed

Site Data - CD-3 Proposed

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 13.50 ft Outlet Station: 170.00 ft Outlet Elevation: 13.30 ft Number of Barrels: 1

Culvert Data Summary - CD-3 Proposed

Barrel Shape: Circular Barrel Diameter: 2.50 ft Barrel Material: Concrete Barrel Manning's n: 0.0120 Inlet Type: Conventional Inlet Edge Condition: Square Edge with Headwall Inlet Depression: None

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
|------------|-------------------------|------------|
| 22.50 | 16.13 | 2.33 |
| 24.73 | 16.13 | 2.33 |
| 26.40 | 16.13 | 2.33 |
| 29.19 | 16.13 | 2.33 |
| 31.42 | 16.13 | 2.33 |
| 33.65 | 16.13 | 2.33 |
| 35.88 | 16.13 | 2.33 |
| 38.11 | 16.13 | 2.33 |
| 40.34 | 16.13 | 2.33 |
| 42.57 | 16.13 | 2.33 |
| 44.80 | 16.13 | 2.33 |

Table 3 - Downstream Channel Rating Curve (Crossing: CD-3 Proposed)

Tailwater Channel Data - CD-3 Proposed

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 16.13 ft

Roadway Data for Crossing: CD-3 Proposed

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 1000.00 ft Crest Elevation: 18.00 ft Roadway Surface: Paved Roadway Top Width: 98.00 ft

| Project: | SR 46 PD&E Study (SR 415 to CR 426) | Design By: <u>DEP</u> | Date: | 12/20/2013 |
|----------|--------------------------------------|-----------------------|-------|------------|
| FIN No.: | <u>240216-4-28-01</u> | Checked by: DTL | Date: | 12/20/13 |
| Subject: | CD-4: Double 8' X 3' (Sta 226+59.46) | | Dule. | 14/20/13 |

Existing Culvert

Note: Based on the Record of Conversation document dated Feb. 7th, 2012 between URS and FDOT Maintenance Office (Jim Wood), there is no recorded history of flooding problems associated with CD-4. Based on the URS site visit conducted on Feb. 12th, 2012 both the upstream and downstream vertical faces of the toewalls have been exposed due to long term flow conditions of the culvert. Erosion protection may be considered in the proposed design based on velocities in the culvert extension. Approximate historical drainage area is 567 acres per existing SR 46 Plans. Due to no record of flooding, Velocity Method shall be used for the analysis.

| Method used: | Velocity (v) = | <u>6 ft/s</u> | (Since no | history of problems is known) |
|-----------------------|--|----------------------------|---------------------|---|
| Existing Information: | Box Culvert Rise: Box Culvert Span: | <u>3 ft</u> <u>8 ft</u> | <u>Note:</u> Culver | t size field verified. |
| | No of culverts: | 2 | | Material: <u>Concrete</u> |
| | Exist culvert length: | <u>72.0 ft</u> | | |
| | Avge flowline elev upstream: | <u>13.20</u> | (NAVD) | (14.2 NGVD) Per Existing SR 46 Plans |
| | Avge flowline elev downstream: | <u>13.00</u> | (NAVD) | (14.0 NGVD) Per Existing SR 46 Plans |
| | Longitudinal slope: | 0.002778 | = | <u>0.2778%</u> |
| | Tailwater: | <u>14.50</u> | (NAVD) | <u>High Water Mark Stain on D/S Ena</u> |

Estimate discharge & Overtopping & HW for existing and proposed:

Area of culvert (A): <u>48.0 sq ft</u>

| Frequency | Factor | Q = A x v | HW Stage Existing (Note 2) | HW Stage Proposed (Note 3) |
|-----------|--------|--------------|----------------------------------|----------------------------------|
| (yr) | | cu ft/s | | |
| 25 | | 288.0 | | |
| 50 | | 340 (Note 1) | 17.55 | 17.60 |
| 100 | 1.4 | 403.2 | 18.04 | 18.04 |
| 500 | 1.7 | 685.4 | 18.21 | 18.22 |

Note 1: Interpolated from Discharge vs Frequency graph (existing) Note 2: Values obtained from HY 8 model of existing C8C

Note 3: Values obtained from HY 8 model of proposed extension CBC

Proposed Cuivert

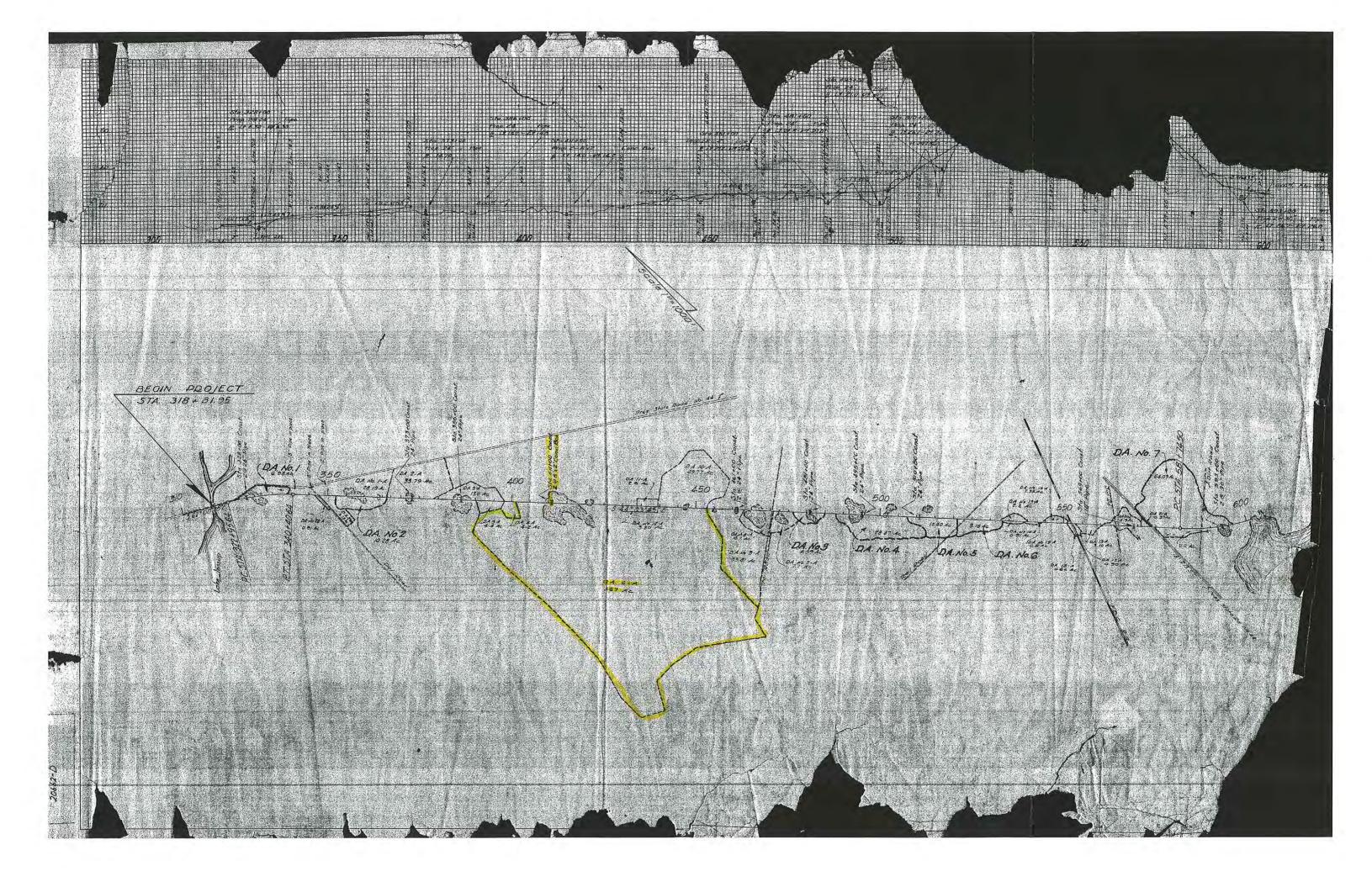
Note: Culvert extension span and rise to match existing Culvert U/S Invert Proposed at existing elevation

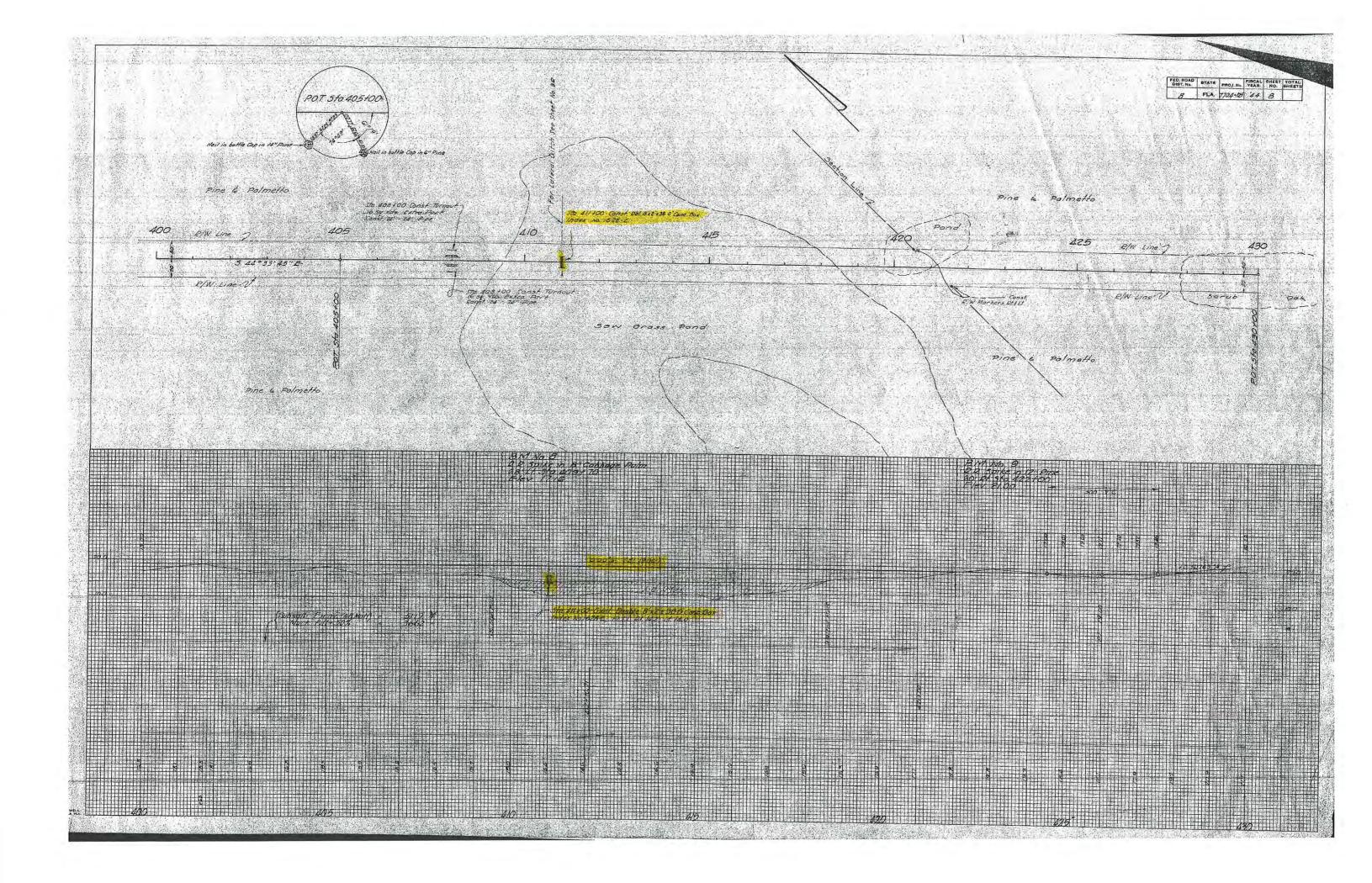
Proposed Information

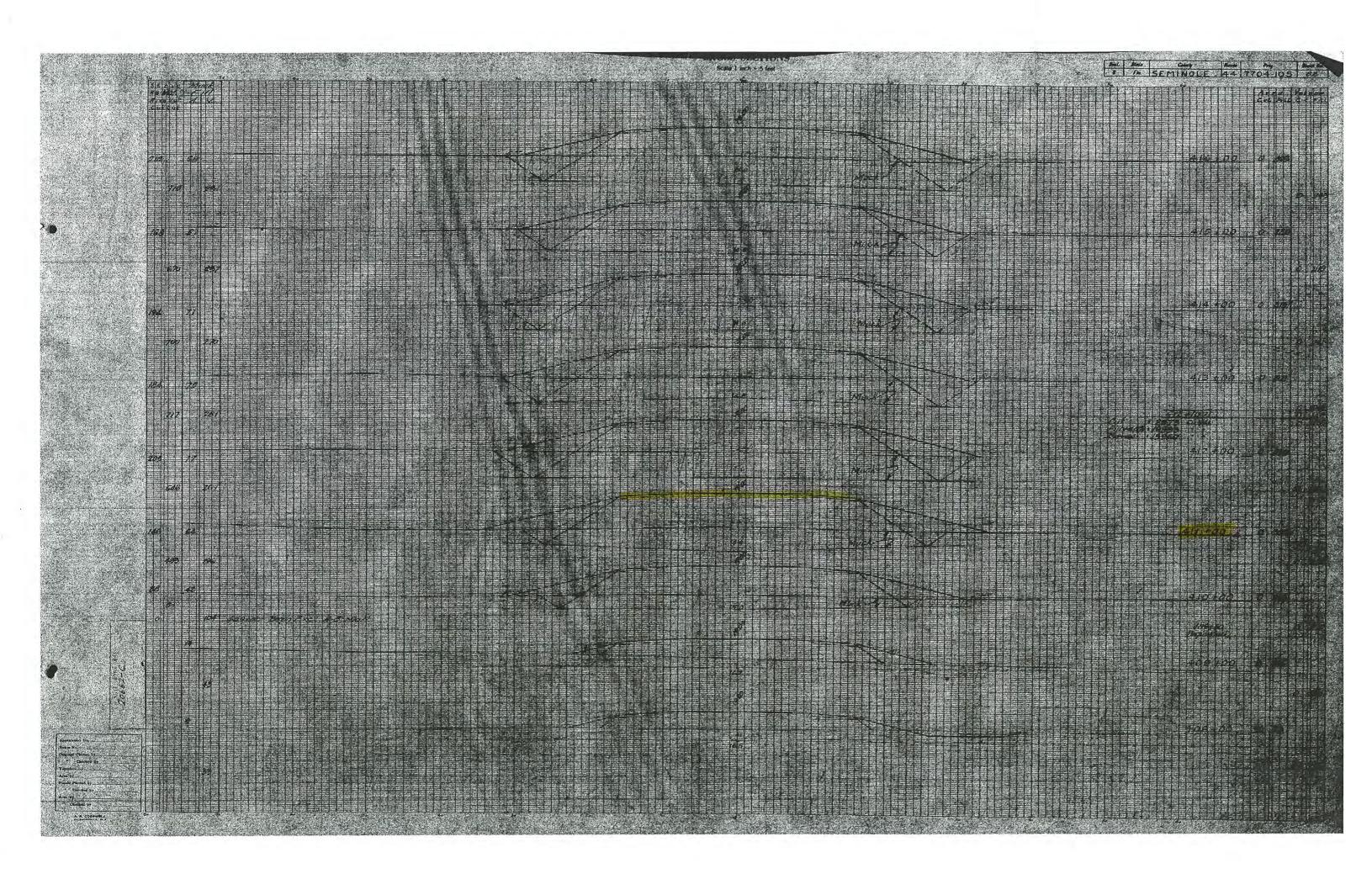
| | Extension | Invert |
|-----------------------------------|-----------|--------|
| | Length | (NAVD) |
| Upstream: | 17.0 ft | 13.25 |
| Downstream: | 81.0 ft | 12.78 |
| Total length of proposed culvert: | 170.0 ft | |

| | Overtopping | |
|-------------|-------------|----------|
| | | |
| | Existing | Proposed |
| Elev (NAVD) | 18 | 18 |
| Q* (cfs) | 375.57 | 371.79 |
| Freq (yr) | 72 | 72 |

* From HY 8 culvert analysis









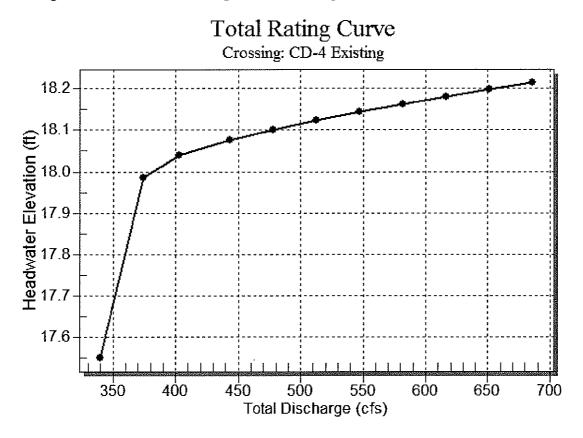
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HY-8 Culvert Analysis Report CD-4 (Existing Double 8'x3' CBC)

| Headwater Elevation (ft) | Total Discharge (cfs) | CD-4 Existing Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------------------|-----------------------|----------------------------------|----------------------------|------------|
| 17.55 | 340.00 | 340.00 | 0.00 | 1 |
| 17.99 | 374.54 | 374.54 | 0.00 | 1 |
| 18.04 | 403.20 | 378.64 | 23.25 | 8 |
| 18.08 | 443.62 | 381.32 | 60.74 | 5 |
| 18.10 | 478.16 | 383.17 | 93.25 | 4 |
| 18.12 | 512.70 | 384.85 | 126.78 | 4 |
| 18.14 | 547.24 | 386.37 | 160.23 | 4 |
| 18.16 | 581.78 | 387.72 | 192.16 | 3 |
| 18.18 | 616.32 | 389.05 | 225.55 | 3 |
| 18.20 | 650.86 | 390.32 | 259.22 | 3 |
| 18.21 | 685.40 | 391.53 | 292.90 | 3 |

Table 1 - Summary of Culvert Flows at Crossing: CD-4 Existing

Rating Curve Plot for Crossing: CD-4 Existing



| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (ft) | Critical Depth (ft) | Outiet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (fl/s) | Tailwater Velocity (fl/s) |
|-----------------------------|-------------------------------|--------------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|------------------------------|---------------------------------|
| 340.00 | 340.00 | 17.55 | 4.351 | 4.199 | 2-M2c | 2.455 | 2.417 | 2.417 | 1.500 | 8.793 | 0.000 |
| 374.54 | 374.54 | 17.99 | 4.786 | 4.474 | 2-M2c | 2.630 | 2.578 | 2,578 | 1.500 | 9.081 | 0.000 |
| 403.20 | 378.64 | 18.04 | 4.840 | 4.506 | 2-M2c | 2.651 | 2.596 | 2.596 | 1.500 | 9.114 | 0.000 |
| 443.62 | 381.32 | 18.08 | 4.876 | 4.527 | 2-M2c | 2.664 | 2.609 | 2.609 | 1.500 | 9.136 | 0.000 |
| 478.16 | 383.17 | 18.10 | 4.900 | 4.541 | 2-M2c | 2.674 | 2.617 | 2.617 | 1.500 | 9.151 | 0.000 |
| 512.70 | 384.85 | 18.12 | 4.923 | 4.554 | 2-M2c | 2.682 | 2.625 | 2.625 | 1.500 | 9.164 | 0.000 |
| 547.24 | 386.37 | 18.14 | 4.943 | 4.566 | 2-M2c | 2.690 | 2.632 | 2.632 | 1.500 | 9.176 | 0.000 |
| 581.78 | 387.72 | 18.16 | 4.962 | 4.577 | 2-M2c | 2.697 | 2.638 | 2.638 | 1.500 | 9.187 | 0.000 |
| 616.32 | 389.05 | 18.18 | 4.980 | 4.587 | 2-M2c | 3.000 | 2.644 | 2.644 | 1.500 | 9.197 | 0.000 |
| 650.86 | 390.32 | 18.20 | 4.997 | 4.597 | 2-M2c | 3.000 | 2.650 | 2.650 | 1.500 | 9.207 | 0.000 |
| 685.40 | 391.53 | 18.21 | 5.014 | 4.606 | 2-M2c | 3.000 | 2.655 | 2.655 | 1.500 | 9.217 | 0.000 |

Table 2 - Culvert Summary Table: CD-4 Existing

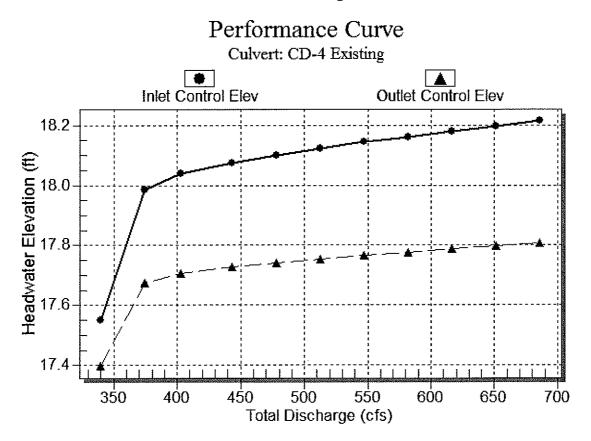
Inlet Elevation (invert): 13.20 ft, Outlet Elevation (invert): 13.00 ft

N

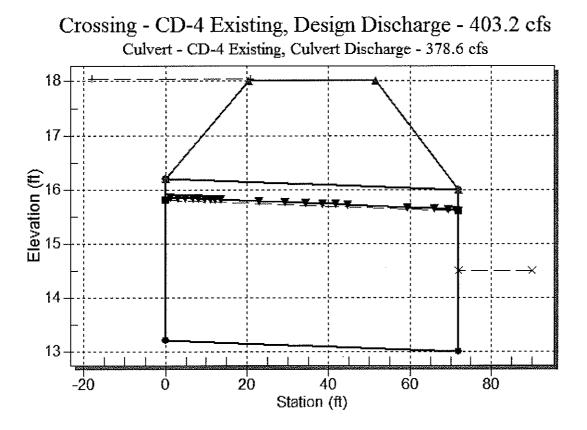
Culvert Length: 72.00 ft, Culvert Slope: 0.0028

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Culvert Performance Curve Plot: CD-4 Existing



Water Surface Profile Plot for Culvert: CD-4 Existing



Site Data - CD-4 Existing

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 13.20 ft Outlet Station: 72.00 ft Outlet Elevation: 13.00 ft Number of Barrels: 2

Culvert Data Summary - CD-4 Existing

Barrel Shape: Concrete Box Barrel Span: 8.00 ft Barrel Rise: 3.00 ft Barrel Material: Concrete Barrel Manning's n: 0.0120 Inlet Type: Conventional Inlet Edge Condition: Square Edge (90°) Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-4 Existing)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
|------------|-------------------------|------------|
| 340.00 | 14.50 | 1.50 |
| 374.54 | 14.50 | 1.50 |
| 403.20 | 14.50 | 1.50 |
| 443.62 | 14.50 | 1.50 |
| 478.16 | 14.50 | 1.50 |
| 512.70 | 14.50 | 1.50 |
| 547.24 | 14.50 | 1.50 |
| 581.78 | 14.50 | 1.50 |
| 616.32 | 14.50 | 1.50 |
| 650.86 | 14.50 | 1.50 |
| 685.40 | 14.50 | 1.50 |

Tailwater Channel Data - CD-4 Existing

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 14.50 ft

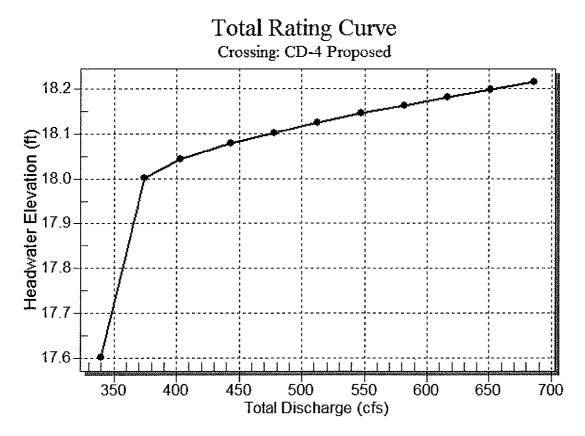
Roadway Data for Crossing: CD-4 Existing

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 1000.00 ft Crest Elevation: 18.00 ft Roadway Surface: Paved Roadway Top Width: 31.00 ft HY-8 Culvert Analysis Report CD-4 (Proposed Double 8'x'3 CBC)

| Headwater Elevation (ft) | Total Discharge (cfs) | CD-4 Proposed Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------------------|-----------------------|----------------------------------|----------------------------|------------|
| 17.60 | 340.00 | 340.00 | 0.00 | 1 |
| 18.00 | 374.54 | 371.89 | 0.13 | 50 |
| 18.04 | 403.20 | 375.13 | 26.74 | 7 |
| 18.08 | 443.62 | 377.78 | 64.43 | 5 |
| 18.10 | 478.16 | 379.62 | 96.93 | 4 |
| 18.13 | 512.70 | 381.29 | 130.41 | 4 |
| 18.15 | 547.24 | 382.81 | 163.83 | 4 |
| 18.16 | 581.78 | 384.16 | 195.77 | 3 |
| 18.18 | 616.32 | 385.50 | 229.16 | 3 |
| 18.20 | 650.86 | 386.77 | 262.82 | 3 |
| 18.22 | 685.40 | 387.98 | 296.48 | 3 |

Table 1 - Summary of Culvert Flows at Crossing: CD-4 Proposed





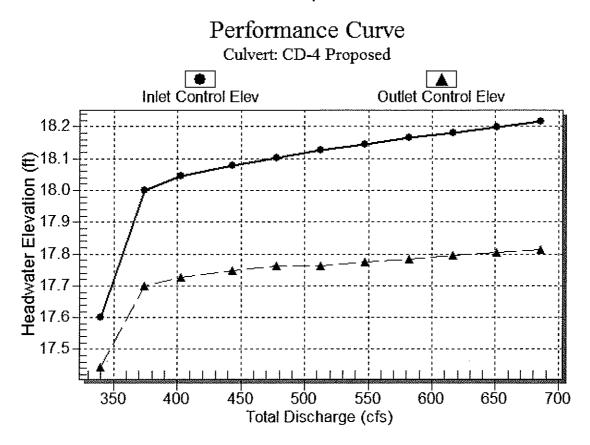
| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (fl) | Inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normał Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
|-----------------------------|-------------------------------|-----------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|------------------------------|---------------------------------|
| 340.00 | 340.00 | 17.60 | 4.351 | 4.195 | 2-M2c | 2.459 | 2.417 | 2.417 | 1.720 | 8.793 | 0.000 |
| 374.54 | 371.89 | 18.00 | 4.751 | 4.451 | 2-M2c | 2.621 | 2.565 | 2.565 | 1,720 | 9.060 | 0.000 |
| 403.20 | 375.13 | 18.04 | 4,794 | 4.477 | 2-M2c | 2.637 | 2.580 | 2.580 | 1.720 | 9.086 | 0.000 |
| 443.62 | 377.78 | 18.08 | 4.829 | 4.497 | 2-M2c | 2.651 | 2.593 | 2.593 | 1.720 | 9.107 | 0.000 |
| 478.16 | 379.62 | 18.10 | 4.853 | 4.512 | 2-M2c | 2.660 | 2.601 | 2.601 | 1.720 | 9.122 | 0.000 |
| 512.70 | 381.29 | 18.13 | 4.875 | 4.512 | 2-M2c | 2.669 | 2.609 | 2.609 | 1.720 | 9.136 | 0.000 |
| 547.24 | 382.81 | 18.15 | 4.896 | 4.524 | 2-M2c | 2.676 | 2.615 | 2.615 | 1.720 | 9.148 | 0.000 |
| 581.78 | 384.16 | 18.16 | 4.914 | 4.534 | 2-M2c | 2.683 | 2.622 | 2.622 | 1.720 | 9.158 | 0.000 |
| 616.32 | 385.50 | 18.18 | 4.932 | 4.545 | 2-M2c | 2.690 | 2.628 | 2.628 | 1.720 | 9.169 | 0.000 |
| 650.86 | 386.77 | 18.20 | 4.949 | 4.555 | 2-M2c | 2.696 | 2.633 | 2.633 | 1.720 | 9.179 | 0.000 |
| 685.40 | 387.98 | 18.22 | 4.965 | 4.565 | 2-M2c | 3.000 | 2.639 | 2.639 | 1.720 | 9.189 | 0.000 |

Table 2 - Culvert Summary Table: CD-4 Proposed

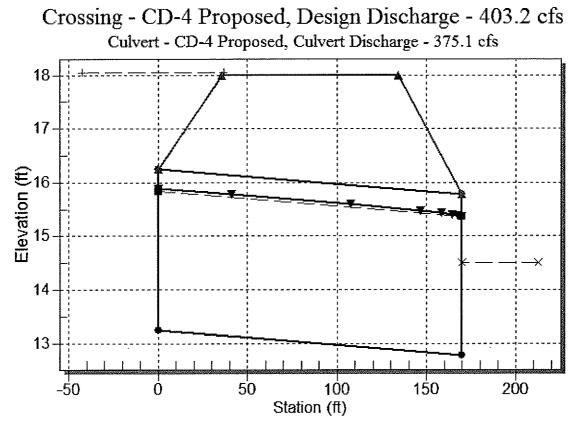
Inlet Elevation (invert): 13.25 ft, Outlet Elevation (invert): 12.78 ft

Culvert Length: 170.00 ft, Culvert Slope: 0.0028

Culvert Performance Curve Plot: CD-4 Proposed



Water Surface Profile Plot for Culvert: CD-4 Proposed



Site Data - CD-4 Proposed

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 13.25 ft Outlet Station: 170.00 ft Outlet Elevation: 12.78 ft Number of Barrels: 2

Culvert Data Summary - CD-4 Proposed

Barrel Shape: Concrete Box Barrel Span: 8.00 ft Barrel Rise: 3.00 ft Barrel Material: Concrete Barrel Manning's n: 0.0120 Inlet Type: Conventional Inlet Edge Condition: Square Edge (90°) Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-4 Proposed)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
|------------|-------------------------|------------|
| 340.00 | 14.50 | 1.72 |
| 374.54 | 14.50 | 1.72 |
| 403.20 | 14.50 | 1.72 |
| 443.62 | 14.50 | 1.72 |
| 478.16 | 14.50 | 1.72 |
| 512.70 | 14.50 | 1.72 |
| 547.24 | 14.50 | 1.72 |
| 581.78 | 14.50 | 1.72 |
| 616.32 | 14.50 | 1.72 |
| 650.86 | 14.50 | 1.72 |
| 685.40 | 14.50 | 1.72 |

Tailwater Channel Data - CD-4 Proposed

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 14.50 ft

Roadway Data for Crossing: CD-4 Proposed

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 1000.00 ft Crest Elevation: 18.00 ft Roadway Surface: Paved Roadway Top Width: 98.00 ft

| Project: | SR 46 PD&E Study (SR 415 to CR 426) | Design By: <u>DEP</u> | Date: | <u>8/7/2012</u> |
|----------|---|-----------------------|--------|-----------------|
| FIN No.: | 240216-4-28-01 | Charles the NT | Derter | aladu |
| Subject: | CD-5: Double 24" RCP (Sta 276+59.84) | Checked by: DTL_ | Date: | 9 25/12 |

Existing Culvert

Note: Based on the Record of Conversation document dated Feb. 7th, 2012 between URS and FDOT Maintenance Office (Jim Wood), there is no recorded history of flooding problems associated with CD-5. Jim Wood did indicate residents in the area have expressed a concern about positive grading in the ditches outside the FDOT *R/W*. Based on the URS site visit conducted on Feb. 12th, 2012 there are no apparent erosion problems. The existing concrete culverts have been lined with a plastic pipe insert to protect the roadway base due to leaks in the existing RCP joints. For the purpose of the PD&E Study, the existing culvert analysis shall ignore the plastic pipe insert as our understanding is this was a temporary solution. Approximate historical drainage area is 53.81 acres per existing SR 46 Plans. Due to no record of flooding at CD-5, Velocity Method shall be used for the analysis.

| Method used: | Velocity (v) = | <u>6 ft/s</u> | (Since no history of problems is known) | | |
|-----------------------|---|------------------------------------|---|--|--|
| Existing Information: | Culvert Diameter: No of culverts: Exist culvert length; | <u>2 ft</u> <u>2</u> 74.0 ft | | Material: <u>RCP</u> | |
| | Avge flawline elev upstream: | <u>20.40</u> * | (NAVD) | (21.4 NGVD) Per Existing SR. 46 Plans | |
| | Avge flawline elev downstream: | <u>20.20</u> (0.002703 | (NAVD) | (21.2 NGVD) <u>Per Existing SR 46 Plans</u> | |
| | Longitudinal slope: Tailwater: | 21.95 | = (NAVD) | <u>0.2703%</u> High Water Mark Stain on D/S End | |
| | | 21.79 | (10,170) | [Approximately 3" below Crown] | |

<u>6.3 sa ft</u>

Estimate discharge & Overtopping & HW for existing and proposed:

Area of culvert (A):

| Frequency | Factor | Q=Axv | HW Stage | HW Stage |
|-----------|--------|------------|----------|----------|
| | | | Existing | Proposed |
| | | | (Note 2) | (Note 3) |
| (yr) | | cu ft/s | | |
| 25 | | 37.7 | | |
| 50 | | 45.5 (Note | 23.93 | 24.76 |
| | | 1) | | |
| 100 | 1.4 | 52.8 | 24.62 | 25.73 |
| 500 | 1.7 | 89.7 | 25.84 | 25.85 |

 Existing
 Proposed

 Elev (NAVD)
 25.8
 25.80

 Q* (cfs)
 63.45
 53.33

 Freq (yr)
 308
 105

* From HY 8 culvert analysis

Note 1: Interpolated from Discharge vs Frequency graph (existing) Note 2: Values obtained from HY 8 model of existing Culvert

Note 3: Values obtained from HY 8 model of proposed replacement Culvert

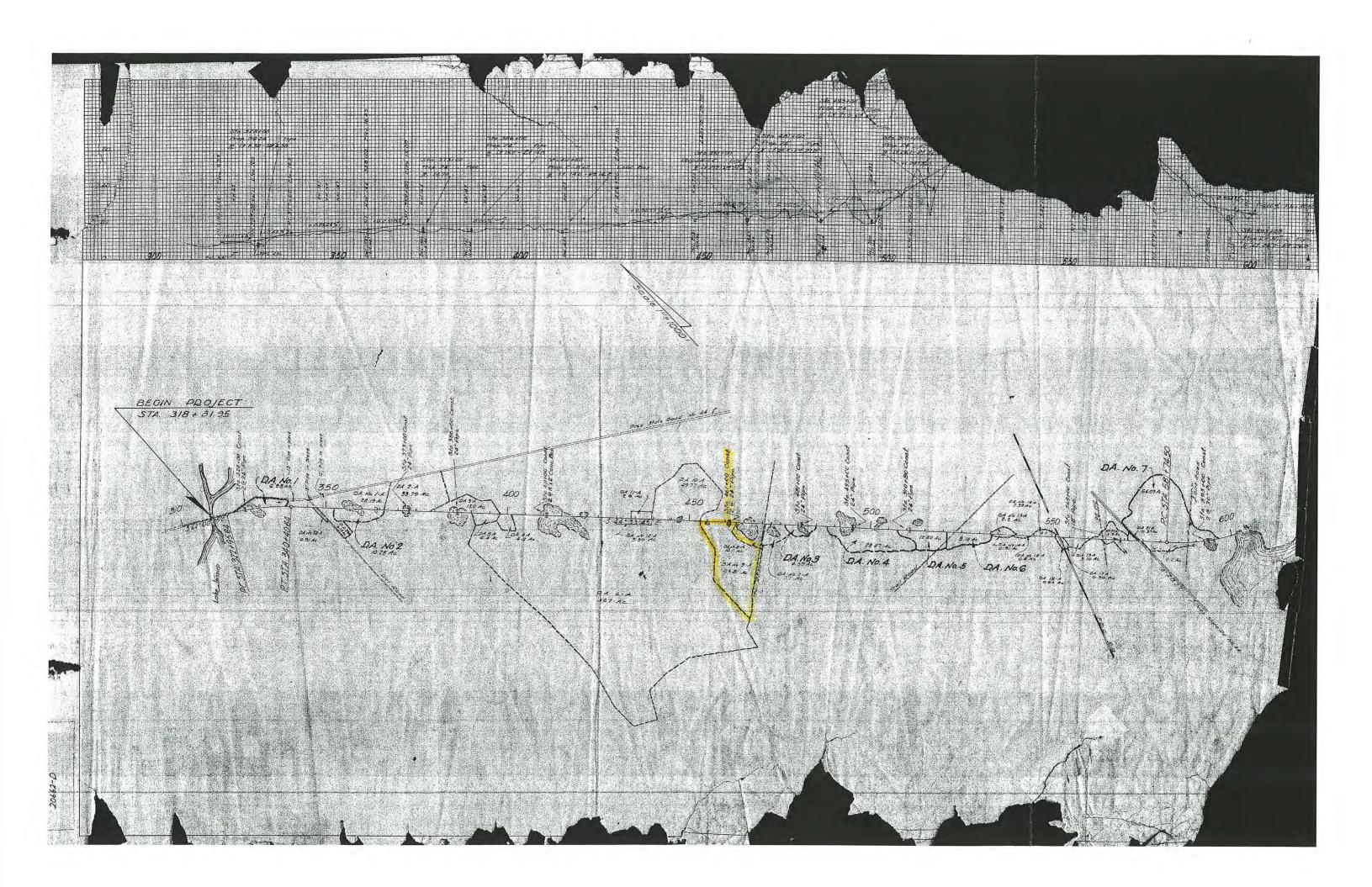
Proposed Culvert

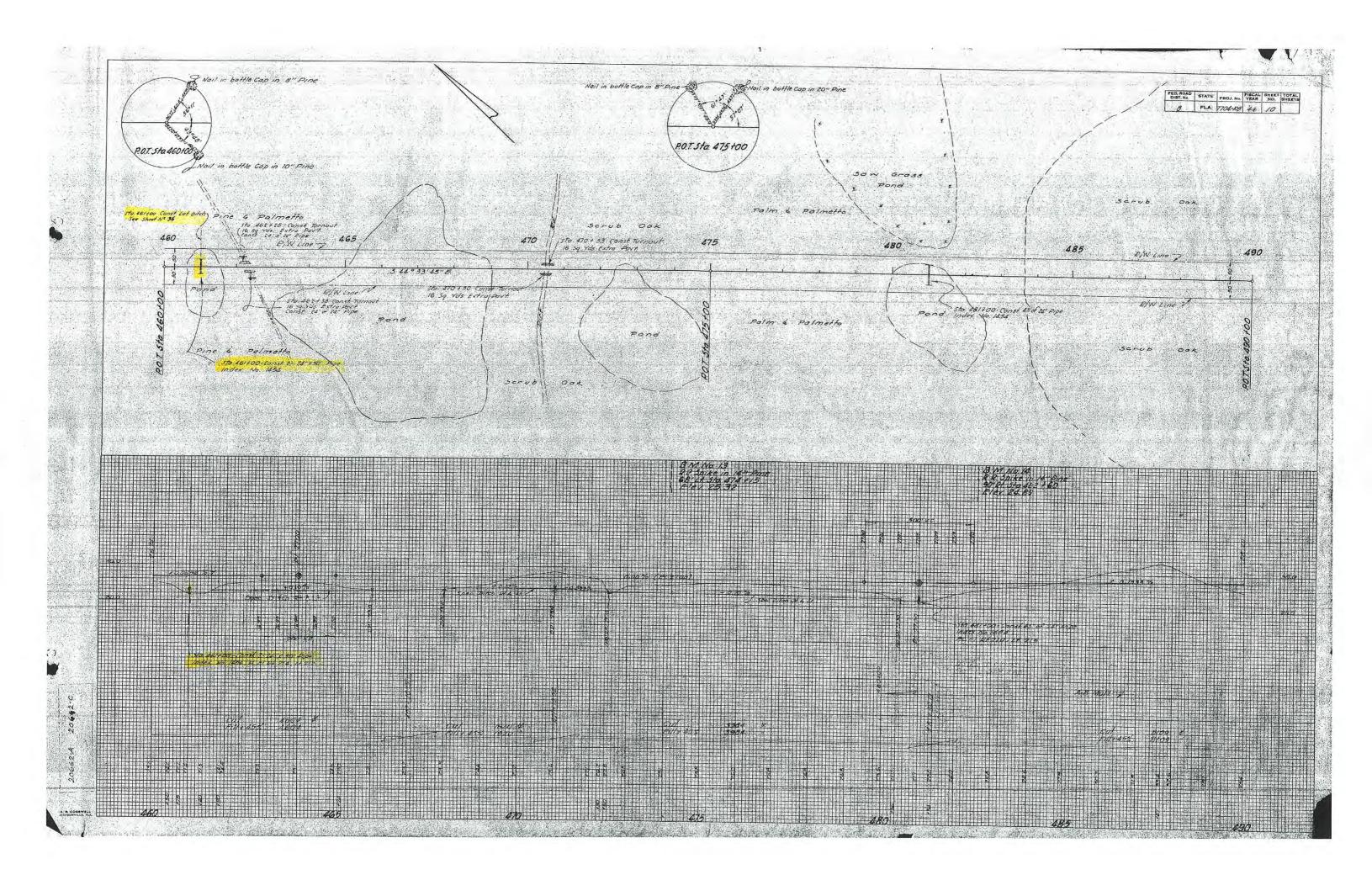
Note: Culvert Replacement to be double 24" RCP

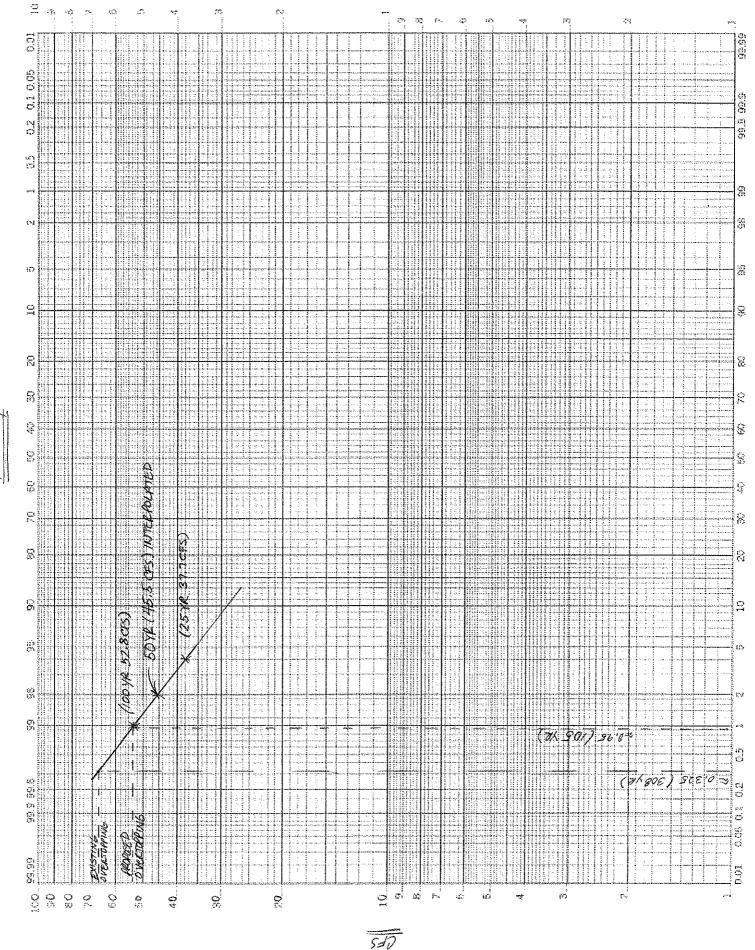
Assume allowable headwater (EOT) to be 6" below CL of Existing SR 46 = 25.3

Proposed Information

| | Extension | Invert |
|-----------------------------------|-----------|--------|
| | Length | (NAVD) |
| Upstream: | 14.0 ft | 20.40 |
| Downstream: | 82.0 ft | 20.20 |
| Total length of proposed culvert: | 170.0 ft | |







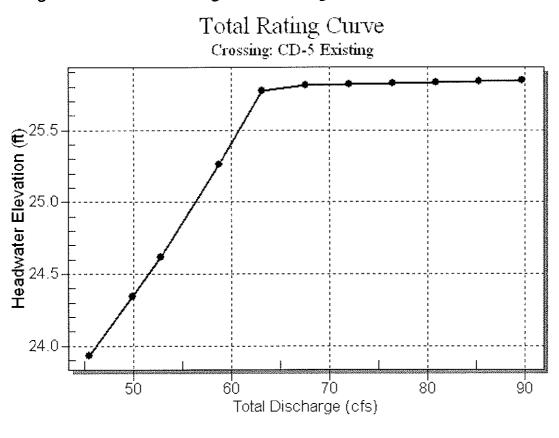
CD-5 months, chargeday

FREQUENCY

HY-8 Culvert Analysis Report CD-5 (Existing Double 24" RCP)

| Headwater Elevation (ft) | Total Discharge (cfs) | CD-5 Existing Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------------------|-----------------------|----------------------------------|----------------------------|------------|
| 23.93 | 45.50 | 45.50 | 0.00 | 1 |
| 24.34 | 49.92 | 49.92 | 0.00 | 1 |
| 24.62 | 52.80 | 52.80 | 0.00 | 1 |
| 25.26 | 58.76 | 58.76 | 0.00 | 1 |
| 25.77 | 63.18 | 63.18 | 0.00 | 1 |
| 25.81 | 67.60 | 63.54 | 3.53 | 11 |
| 25.82 | 72.02 | 63.61 | 7.92 | 4 |
| 25.83 | 76.44 | 63.67 | 12.51 | 4 |
| 25.83 | 80.86 | 63.72 | 16.65 | 3 |
| 25.84 | 85.28 | 63.76 | 21.09 | 3 |
| 25.84 | 89.70 | 63.81 | 25.58 | 3 |

Table 1 - Summary of Culvert Flows at Crossing: CD-5 Existing



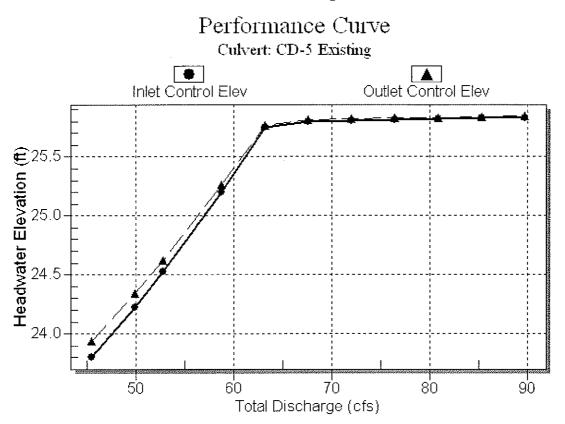
Rating Curve Plot for Crossing: CD-5 Existing

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (fl) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
|-----------------------------|-------------------------------|--------------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|------------------------------|---------------------------------|
| 45.50 | 45.50 | 23.93 | 3,405 | 3.534 | 7-M2t | 2.000 | 1.686 | 1.750 | 1.750 | 7.826 | 0.000 |
| 49.92 | 49.92 | 24.34 | 3.827 | 3.941 | 7-M2c | 2,000 | 1.751 | 1,751 | 1.750 | 8.582 | 0.000 |
| 52.80 | 52,80 | 24.62 | 4.126 | 4.217 | 7-M2c | 2.000 | 1.793 | 1.793 | 1.750 | 8,893 | 0.000 |
| 58.76 | 58.76 | 25.26 | 4.801 | 4.862 | 7-M2c | 2.000 | 1.881 | 1.881 | 1.750 | 9.650 | 0.000 |
| 63.18 | 63.18 | 25.77 | 5.350 | 5.369 | 7-M2c | 2.000 | 1.946 | 1.946 | 1.750 | 10.197 | 0.000 |
| 67.60 | 63.54 | 25.81 | 5.397 | 5.411 | 7-M2c | 2.000 | 1.952 | 1,952 | 1.750 | 10,241 | 0.000 |
| 72.02 | 63.61 | 25.82 | 5.406 | 5.419 | 7-M2c | 2.000 | 1.953 | 1.953 | 1.750 | 10.250 | 0.000 |
| 76.44 | 63.67 | 25.83 | 5.413 | 5.426 | 7-M2c | 2.000 | 1.954 | 1.954 | 1.750 | 10.257 | 0.000 |
| 80.86 | 63.72 | 25.83 | 5.419 | 5.432 | 7-M2c | 2.000 | 1.954 | 1.954 | 1.750 | 10.263 | 0.000 |
| 85.28 | 63.76 | 25.84 | 5.425 | 5.437 | 7-M2c | 2.000 | 1.955 | 1.955 | 1.750 | 10.268 | 0.000 |
| 89.70 | 63.81 | 25.84 | 5.431 | 5.442 | 7-M2c | 2.000 | 1.956 | 1.956 | 1.750 | 10.273 | 0.000 |

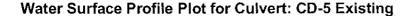
Table 2 - Culvert Summary Table: CD-5 Existing

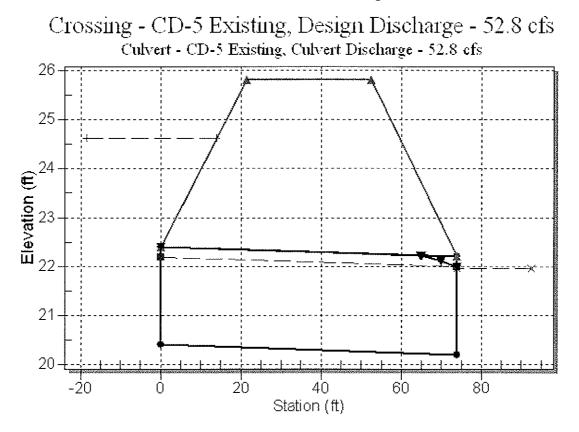
Inlet Elevation (invert): 20.40 ft, Outlet Elevation (invert): 20.20 ft

Culvert Length: 74.00 ft, Culvert Slope: 0.0027



Culvert Performance Curve Plot: CD-5 Existing





Site Data - CD-5 Existing

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 20.40 ft Outlet Station: 74.00 ft Outlet Elevation: 20.20 ft Number of Barrels: 2

Culvert Data Summary - CD-5 Existing

Barrel Shape: Circular Barrel Diameter: 2.00 ft Barrel Material: Concrete Barrel Manning's n: 0.0120 Inlet Type: Conventional Inlet Edge Condition: Square Edge with Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-5 Existing)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
|------------|-------------------------|------------|
| 45.50 | 21.95 | 1.75 |
| 49.92 | 21.95 | 1.75 |
| 52.80 | 21.95 | 1.75 |
| 58.76 | 21.95 | 1.75 |
| 63.18 | 21.95 | 1.75 |
| 67.60 | 21.95 | 1.75 |
| 72.02 | 21.95 | 1.75 |
| 76.44 | 21.95 | 1.75 |
| 80.86 | 21.95 | 1.75 |
| 85.28 | 21.95 | 1.75 |
| 89.70 | 21.95 | 1.75 |

Tailwater Channel Data - CD-5 Existing

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 21.95 ft

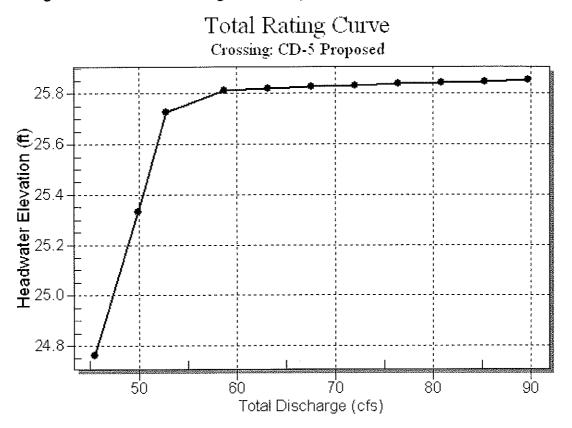
Roadway Data for Crossing: CD-5 Existing

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 1000.00 ft Crest Elevation: 25.80 ft Roadway Surface: Paved Roadway Top Width: 31.00 ft HY-8 Culvert Analysis Report CD-5 (Proposed Double 24" RCP)

| Headwater Elevation (ft) | Total Discharge (cfs) | CD-5 Proposed Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------------------|-----------------------|----------------------------------|----------------------------|------------|
| 24.76 | 45.50 | 45.50 | 0.00 | 1 |
| 25.33 | 49.92 | 49.92 | 0.00 | 1 |
| 25.73 | 52.80 | 52.80 | 0.00 | 1 |
| 25.81 | 58.76 | 53.43 | 4.84 | 14 |
| 25.82 | 63.18 | 53.48 | 9.30 | 4 |
| 25.83 | 67.60 | 53.52 | 13.41 | 3 |
| 25.83 | 72.02 | 53.57 | 17.89 | 3 |
| 25.84 | 76.44 | 53.60 | 22,42 | 3 |
| 25.84 | 80.86 | 53.64 | 26.93 | 3 |
| 25.85 | 85.28 | 53.67 | 31.40 | 3 |
| 25.85 | 89.70 | 53.71 | 35.84 | 3 |

Table 1 - Summary of Culvert Flows at Crossing: CD-5 Proposed





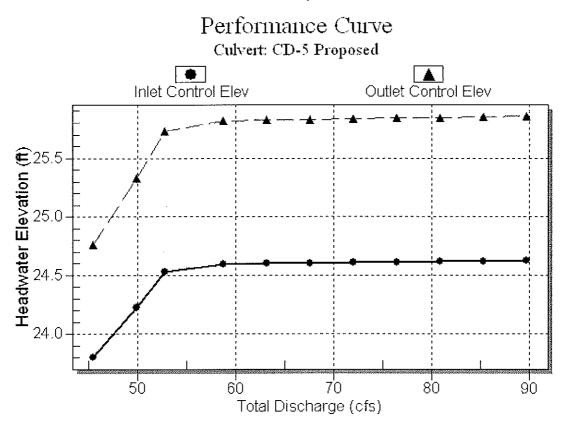
| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (fl) | Outlet Control Depth (ft) | Flow Type | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (fl) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
|-----------------------------|-------------------------------|--------------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|------------------------------|---------------------------------|
| 45.50 | 45.50 | 24.76 | 3.406 | 4.363 | 7-M2t | 2.000 | 1.686 | 1.750 | 1.750 | 7.826 | 0.000 |
| 49.92 | 49.92 | 25.33 | 3.828 | 4.933 | 7-M2c | 2.000 | 1.751 | 1.751 | 1.750 | 8.582 | 0.000 |
| 52.80 | 52.80 | 25.73 | 4.127 | 5.326 | 7-M2c | 2,000 | 1.793 | 1,793 | 1.750 | 8,893 | 0.000 |
| 58.76 | 53.43 | 25.81 | 4.195 | 5.413 | 7-M2c | 2.000 | 1.803 | 1.803 | 1.750 | 8.958 | 0.000 |
| 63.18 | 53.48 | 25.82 | 4.200 | 5.421 | 7-M2c | 2.000 | 1.803 | 1.803 | 1.750 | 8.964 | 0.000 |
| 67.60 | 53.52 | 25.83 | 4.205 | 5.427 | 7-M2c | 2.000 | 1.804 | 1.804 | 1.750 | 8,969 | 0.000 |
| 72.02 | 53.57 | 25.83 | 4.210 | 5.433 | 7-M2c | 2.000 | 1.805 | 1.805 | 1.750 | 8.973 | 0.000 |
| 76.44 | 53.60 | 25.84 | 4.214 | 5.438 | 7-M2c | 2.000 | 1.805 | 1.805 | 1.750 | 8.977 | 0.000 |
| 80.86 | 53.64 | 25.84 | 4.218 | 5.443 | 7-M2c | 2,000 | 1.806 | 1,806 | 1.750 | 8,981 | 0,000 |
| 85.28 | 53.67 | 25.85 | 4,221 | 5.448 | 7-M2c | 2.000 | 1.806 | 1.806 | 1.750 | 8.984 | 0.000 |
| 89.70 | 53.71 | 25.85 | 4.226 | 5.453 | 7-M2c | 2.000 | 1.807 | 1.807 | 1.750 | 8.988 | 0.000 |

Table 2 - Culvert Summary Table: CD-5 Proposed

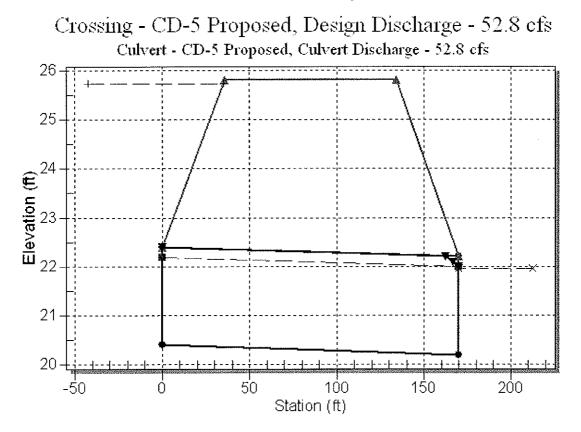
Inlet Elevation (invert): 20.40 ft, Outlet Elevation (invert): 20.20 ft

Culvert Length: 170.00 ft, Culvert Stope: 0.0012

Culvert Performance Curve Plot: CD-5 Proposed







Site Data - CD-5 Proposed

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 20.40 ft Outlet Station: 170.00 ft Outlet Elevation: 20.20 ft Number of Barrels: 2

Culvert Data Summary - CD-5 Proposed

Barrel Shape: Circular Barrel Diameter: 2.00 ft Barrel Material: Concrete Barrel Manning's n: 0.0120 Inlet Type: Conventional Inlet Edge Condition: Square Edge with Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-5 Proposed)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
|------------|-------------------------|------------|
| 45.50 | 21.95 | 1.75 |
| 49.92 | 21.95 | 1.75 |
| 52.80 | 21.95 | 1.75 |
| 58.76 | 21.95 | 1.75 |
| 63.18 | 21.95 | 1.75 |
| 67.60 | 21.95 | 1.75 |
| 72.02 | 21.95 | 1.75 |
| 76.44 | 21.95 | 1.75 |
| 80.86 | 21.95 | 1.75 |
| 85.28 | 21.95 | 1.75 |
| 89.70 | 21.95 | 1.75 |

Tailwater Channel Data - CD-5 Proposed

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 21.95 ft

Roadway Data for Crossing: CD-5 Proposed

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 1000.00 ft Crest Elevation: 25.80 ft Roadway Surface: Paved Roadway Top Width: 98.00 ft

| Project: | SR 46 PD&E Study (SR 415 to CR 426) | Design By: <u>DEP</u> | Date: | <u>8/7/2012</u> |
|----------|---------------------------------------|-----------------------|-------|-----------------|
| FIN No.: | 240216-4-28-01 | Chapterd hun ND | Date: | 9/25/12 |
| Subject: | CD-6 : 24" RCP (Sta 296+63.64) | Checked by: DTL | Date: | 9125/12 |

Existing Culvert

Note: Based on the Record of Conversation document dated Feb. 7th, 2012 between URS and FDOT Maintenance Office (Jim Wood), there is no recorded history of flooding problems associated with CD-6. Based on the URS site visit conducted on Feb. 12th, 2012 there are no apparent erosion problems. The existing concrete culverts have been lined with a plastic pipe insert to protect the roadway base due to leaks in the existing RCP joints. For the purpose of the PD&E Study, the existing culvert analysis shall ignore the plastic pipe insert as our understanding is this was a temporary solution. Approximate historical drainage area is 4.59 acres per existing SR 46 Plans. Due to no record of flooding at CD-6, Velocity Method shall be used for the analysis.

| Method used: | Velocity (v) = | <u>6 ft/s</u> | (Since no history of problems is known) | | |
|-----------------------|---|------------------------------------|---|------------------------|--------------------------|
| Existing Information: | Culvert Diameter: No of culverts: Exist culvert length: | <u>2 ft</u> <u>1</u> 76.0 ft | | Material | : <u>RCP</u> |
| | Avge flowline elev upstream: | 20.50 | (NAVD) | (21.5 NGVD) | Per Existing SR 46 Plans |
| | Avge flowline elev downstream: | <u>20.00</u> 0.006579 | (NAVD) = | (21.0 NGVD) 0.6579% | Per Existing SR 46 Plans |
| | Longitudinal slope: Tailwater: | 23,00 | - (NAVD) | - | Mark Stain on D/S End |
| | | 20100 | (Approximately 12" above Crown) | | |

Estimate discharge & Overtopping & HW for existing and proposed:

Area of culvert (A): <u>3.1 sq ft</u>

| Factor | Q = A x v | HW Stage | HW Stage |
|--------|------------|---|---|
| | | Existing | Proposed |
| | | (Note 2) | (Note 3) |
| | cu ft/s | | |
| | 18.8 | | |
| | 22.5 (Note | 24.83 | 23.92 |
| | 1) | | |
| 1.4 | 26.4 | 25.52 | 24.27 |
| 1.7 | 44.8 | 26.03 | 26.01 |
| | | cu ft/s 18.8 22.5 - (Note 1) 1.4 26.4 | Cu ft/s Existing (Note 2) 18.8 22.5 (Note 24.83 1) 1.4 26.4 25.52 |

| Overtopping | | | | | | |
|-------------|----------|----------|--|--|--|--|
| | Existing | Proposed | | | | |
| Elev (NAVD) | 26.00 | 26.00 | | | | |
| Q* (cfs) | 28.79 | 40.56 | | | | |
| Freq (yr) | 143 | >500 | | | | |

* From HY 8 culvert analysis

Note 1: Interpolated from Discharge vs Frequency graph (existing) Note 2: Values obtained from HY 8 model of existing Culvert

Note 2. Values obtained from HT 8 moder of existing Colven

Note 3: Values obtained from HY 8 model of proposed replacement Culvert

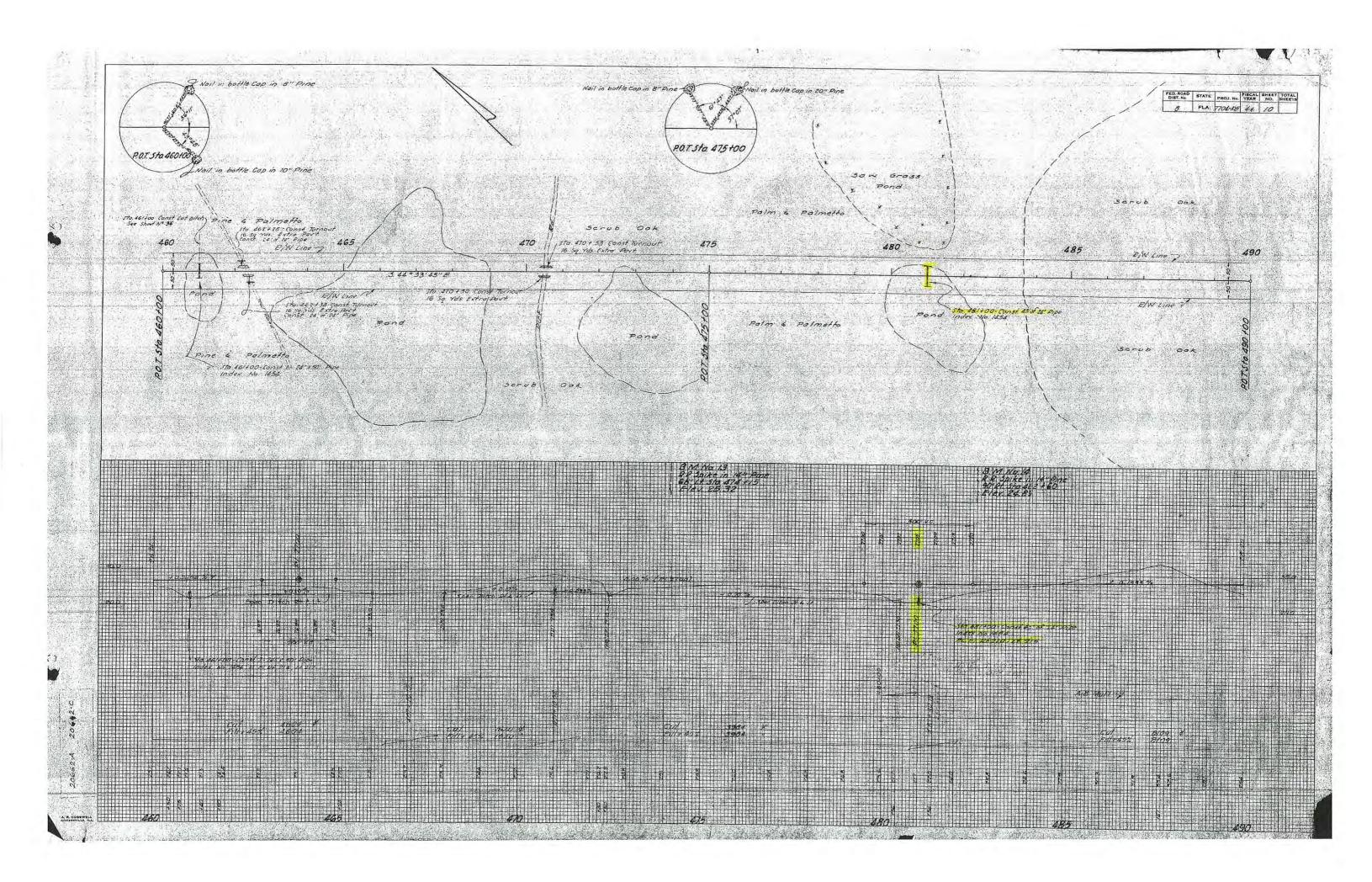
Proposed Culvert

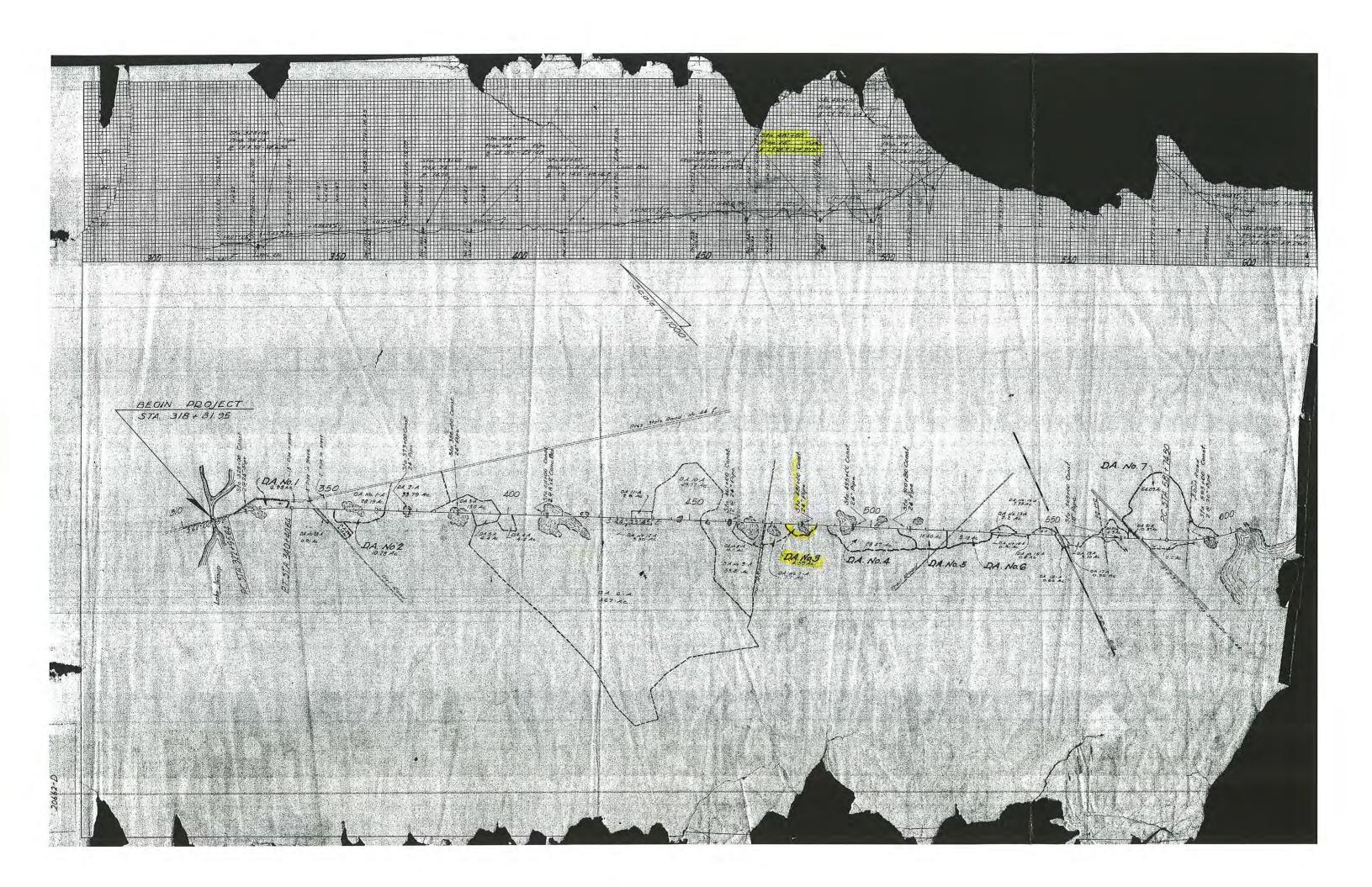
Note: Culvert Replacement to be 30" RCP

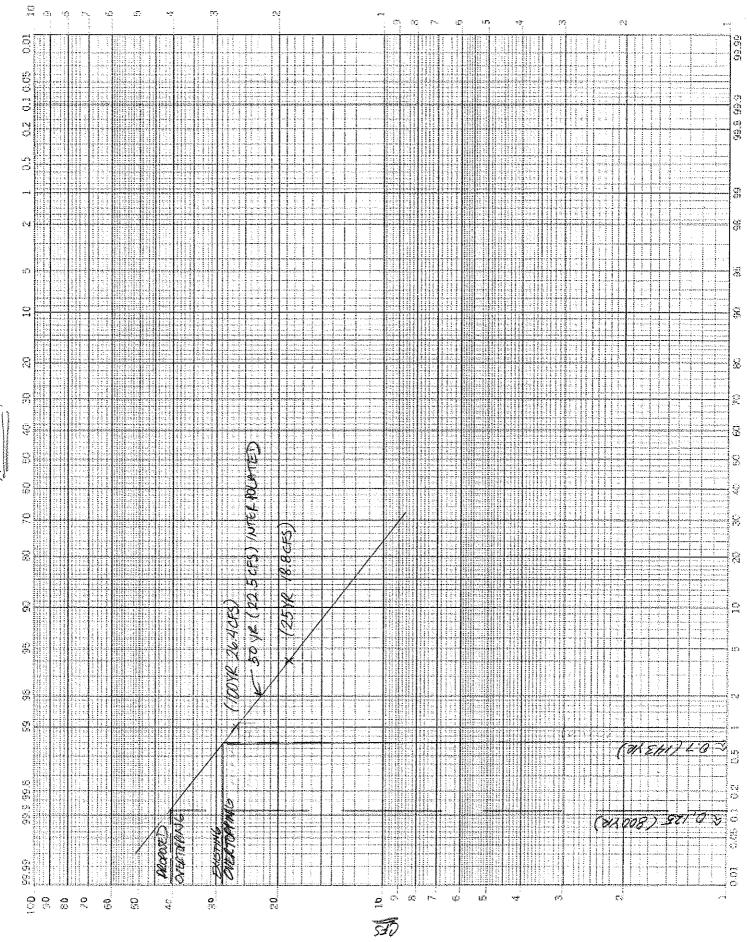
Assume allowable headwater (EOT) to be 6" below CL of Existing SR 46 = 25.5 -

Proposed Information

| | Extension | Invert |
|-----------------------------------|-----------|--------|
| | Length | (NAVD) |
| Upstream: | 64.5 ft | 20.00 |
| Downstream: | 29.5 ft | 19.50 |
| Total length of proposed culvert: | 170.0 ft | |







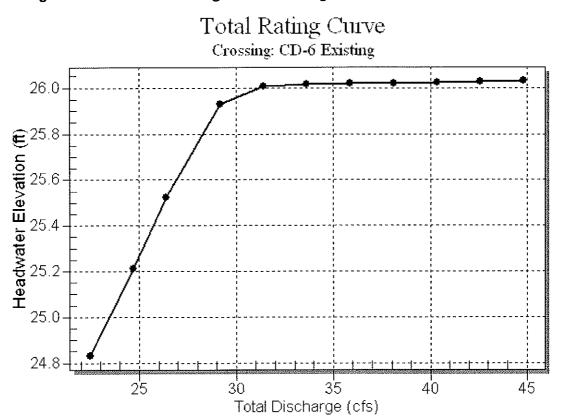
CD-6 protection of equivalent

FEQUENCY

HY-8 Culvert Analysis Report CD-6 (Existing 24" RCP)

| Headwater Elevation (ft) | Total Discharge (cfs) | CD-6 Existing Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------------------|-----------------------|----------------------------------|----------------------------|------------|
| 24.83 | 22.50 | 22.50 | 0.00 | 1 |
| 25.21 | 24.73 | 24.73 | 0.00 | 1 |
| 25.52 | 26.40 | 26.40 | 0.00 | 1 |
| 25.93 | 29.19 | 28.46 | 0.00 | 50 |
| 26.01 | 31.42 | 28.84 | 2.42 | 18 |
| 26.01 | 33.65 | 28,86 | 4.61 | 4 |
| 26.02 | 35.88 | 28,88 | 6.68 | 3 |
| 26.02 | 38.11 | 28.90 | 8.93 | 3 |
| 26.02 | 40.34 | 28.91 | 11.22 | 3 |
| 26.03 | 42.57 | 28.93 | 13.50 | 3 |
| 26.03 | 44.80 | 28.94 | 15.76 | 3 |

Table 1 - Summary of Culvert Flows at Crossing: CD-6 Existing



Rating Curve Plot for Crossing: CD-6 Existing

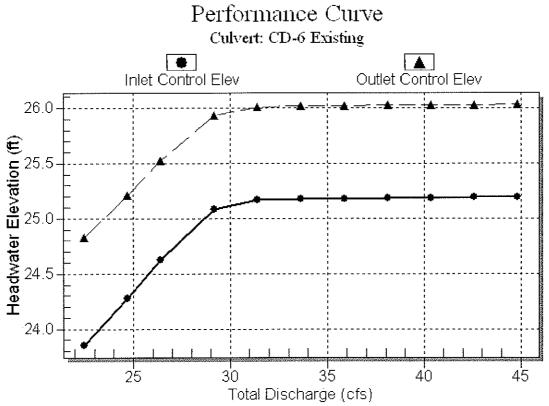
| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (fl) | Critical Depth (fl) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Taitwater Velocity (ft/s) |
|-----------------------------|-------------------------------|--------------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|------------------------------|---------------------------------|
| 22.50 | 22.50 | 24.83 | 3.356 | 4.332 | 4-FFf | 2.000 | 1.678 | 2.000 | 3.000 | 7.162 | 0.000 |
| 24.73 | 24.73 | 25.21 | 3.777 | 4.713 | 4-FFf | 2,000 | 1,744 | 2.000 | 3.000 | 7.872 | 0.000 |
| 26.40 | 26,40 | 25.52 | 4.122 | 5.022 | 4-FFf | 2.000 | 1.793 | 2.000 | 3.000 | 8.403 | 0.000 |
| 29.19 | 28.46 | 25.93 | 4,580 | 5.430 | 4-FFf | 2.000 | 1.854 | 2.000 | 3.000 | 9.059 | 0.000 |
| 31.42 | 28.84 | 26.01 | 4.669 | 5.509 | 4-FFf | 2.000 | 1.865 | 2.000 | 3.000 | 9.179 | 0.000 |
| 33.65 | 28.86 | 26.01 | 4.674 | 5.514 | 4-FFf | 2.000 | 1.866 | 2.000 | 3.000 | 9.186 | 0.000 |
| 35.88 | 28.88 | 26.02 | 4.678 | 5.517 | 4-FFf | 2.000 | 1.867 | 2.000 | 3.000 | 9.192 | 0.000 |
| 38.11 | 28.90 | 26.02 | 4.683 | 5.521 | 4-FFf | 2.000 | 1.867 | 2.000 | 3.000 | 9.198 | 0.000 |
| 40.34 | 28.91 | 26.02 | 4.687 | 5.525 | 4-FFf | 2.000 | 1.868 | 2.000 | 3.000 | 9.203 | 0.000 |
| 42.57 | 28.93 | 26.03 | 4.690 | 5.528 | 4-FFf | 2.000 | 1.868 | 2.000 | 3.000 | 9.208 | 0.000 |
| 44.80 | 28.94 | 26.03 | 4.694 | 5.531 | 4-FFf | 2.000 | 1.868 | 2.000 | 3.000 | 9.213 | 0.000 |

Table 2 - Culvert Summary Table: CD-6 Existing

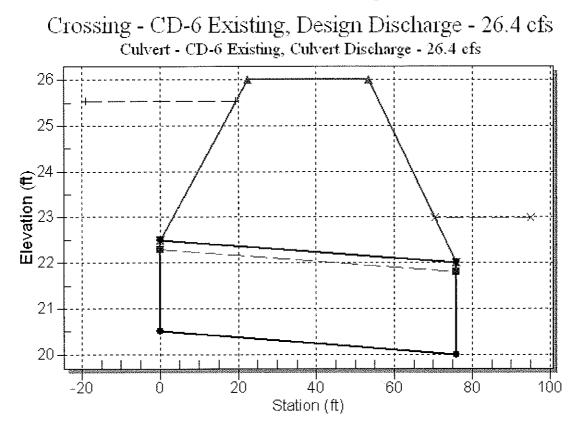
Inlet Elevation (invert): 20.50 ft, Outlet Elevation (invert): 20.00 ft

Culvert Length: 76.00 ft, Culvert Siope: 0.0066





Water Surface Profile Plot for Culvert: CD-6 Existing



Site Data - CD-6 Existing

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 20.50 ft Outlet Station: 76.00 ft Outlet Elevation: 20.00 ft Number of Barrels: 1

Culvert Data Summary - CD-6 Existing

Barrel Shape: Circular Barrel Diameter: 2.00 ft Barrel Material: Concrete Barrel Manning's n: 0.0120 Inlet Type: Conventional Inlet Edge Condition: Square Edge with Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-6 Existing)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
|------------|-------------------------|------------|
| 22.50 | 23.00 | 3.00 |
| 24.73 | 23.00 | 3.00 |
| 26.40 | 23.00 | 3.00 |
| 29.19 | 23.00 | 3.00 |
| 31.42 | 23.00 | 3.00 |
| 33.65 | 23.00 | 3.00 |
| 35.88 | 23.00 | 3.00 |
| 38.11 | 23.00 | 3.00 |
| 40.34 | 23.00 | 3.00 |
| 42.57 | 23.00 | 3.00 |
| 44.80 | 23.00 | 3.00 |

Tailwater Channel Data - CD-6 Existing

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 23.00 ft

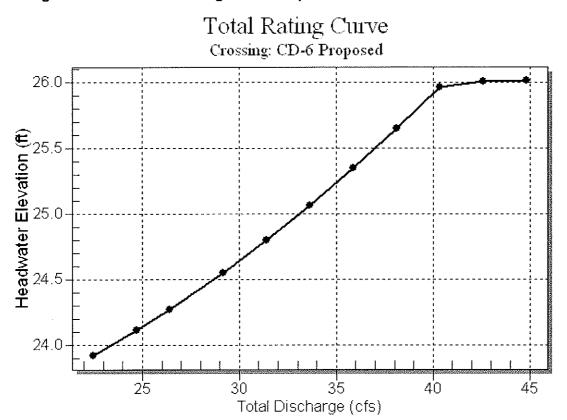
Roadway Data for Crossing: CD-6 Existing

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 1000.00 ft Crest Elevation: 26.00 ft Roadway Surface: Paved Roadway Top Width: 31.00 ft

HY-8 Culvert Analysis Report CD-6 (Proposed 30" RCP)

| Headwater Elevation (ft) | Total Discharge (cfs) | CD-6 Proposed Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------------------|-----------------------|----------------------------------|----------------------------|------------|
| 23.92 | 22.50 | 22.50 | 0.00 | 1 |
| 24.11 | 24.73 | 24.73 | 0.00 | 1 |
| 24.27 | 26.40 | 26.40 | 0.00 | 1 |
| 24.55 | 29.19 | 29.19 | 0.00 | 1 |
| 24.80 | 31.42 | 31.42 | 0.00 | 1 |
| 25.06 | 33.65 | 33.65 | 0.00 | 1 |
| 25.35 | 35.88 | 35.88 | 0.00 | 1 |
| 25.65 | 38.11 | 38.11 | · 0.00 | 1 |
| 25.97 | 40.34 | 40.34 | 0.00 | 1 |
| 26.01 | 42.57 | 40.61 | 1.64 | 14 |
| 26.01 | 44.80 | 40.65 | 3.89 | 4 |

Table 1 - Summary of Culvert Flows at Crossing: CD-6 Proposed



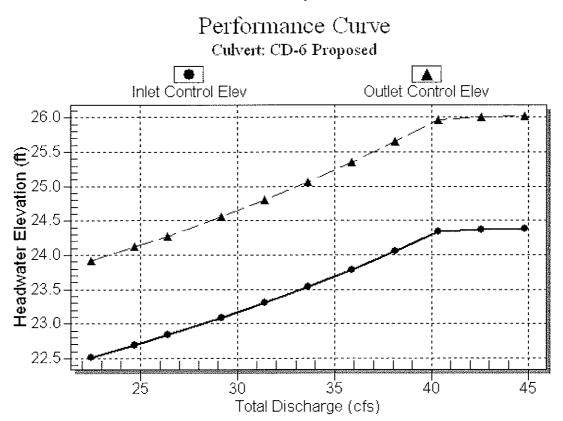
Rating Curve Plot for Crossing: CD-6 Proposed

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (fi) | Flow Type | Normal Depth (ft) | Critical Depth (fl) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
|-----------------------------|-------------------------------|--------------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|------------------------------|---------------------------------|
| 22.50 | 22.50 | 23.92 | 2.516 | 3.923 | 4-FFf | 1.919 | 1.608 | 2.500 | 3.000 | 4,584 | 0.000 |
| 24.73 | 24.73 | 24.11 | 2.696 | 4.115 | 4-FFf | 2.132 | 1.690 | 2.500 | 3.000 | 5.038 | 0.000 |
| 26.40 | 26.40 | 24.27 | 2.837 | 4.270 | 4-FFf | 2.500 | 1.751 | 2.500 | 3.000 | 5.378 | 0.000 |
| 29,19 | 29.19 | 24.55 | 3.087 | 4.553 | 4-FFf | 2.500 | 1.835 | 2.500 | 3.000 | 5.947 | 0.000 |
| 31.42 | 31.42 | 24.80 | 3.303 | 4.799 | 4-FFf | 2.500 | 1.902 | 2,500 | 3.000 | 6.401 | 0.000 |
| 33.65 | 33.65 | 25.06 | 3.534 | 5.064 | 4-FFf | 2,500 | 1.970 | 2.500 | 3.000 | 6.855 | 0.000 |
| 35.88 | 35.88 | 25.35 | 3.783 | 5.347 | 4-FFf | 2.500 | 2.026 | 2.500 | 3.000 | 7.309 | 0.000 |
| 38.11 | 38.11 | 25.65 | 4.049 | 5.647 | 4-FFf | 2.500 | 2.073 | 2.500 | 3.000 | 7.764 | 0,000 |
| 40.34 | 40.34 | 25.97 | 4.334 | 5.966 | 4-FFf | 2.500 | 2.120 | 2.500 | 3.000 | 8.218 | 0.000 |
| 42.57 | 40.61 | 26.01 | 4,369 | 6.006 | 4-FFf | 2.500 | 2.126 | 2.500 | 3.000 | 8.273 | 0.000 |
| 44.80 | 40.65 | 26.01 | 4.375 | 6.012 | 4-FFf | 2.500 | 2.126 | 2.500 | 3.000 | 8.281 | 0.000 |

Table 2 - Culvert Summary Table: CD-6 Proposed

Inlet Elevation (invert): 20.00 ft, Outlet Elevation (invert): 19.50 ft

Culvert Length: 170.00 ft, Culvert Slope: 0.0029



Cuivert Performance Curve Plot: CD-6 Proposed

Crossing - CD-6 Proposed, Design Discharge - 26.4 cfs Culvert - CD-6 Proposed, Culvert Discharge - 26.4 cfs

50

1<u>0</u>0

Station (ft)

150

200

Water Surface Profile Plot for Culvert: CD-6 Proposed

Site Data - CD-6 Proposed

21

20

-50

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 20.00 ft Outlet Station: 170.00 ft Outlet Elevation: 19.50 ft Number of Barrels: 1

Ó

Culvert Data Summary - CD-6 Proposed

Barrel Shape: Circular Barrel Diameter: 2.50 ft Barrel Material: Concrete Barrel Manning's n: 0.0120 Inlet Type: Conventional Inlet Edge Condition: Square Edge with Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-6 Proposed)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
|------------|-------------------------|------------|
| 22.50 | 23.00 | 3.00 |
| 24.73 | 23.00 | 3.00 |
| 26.40 | 23.00 | 3.00 |
| 29.19 | 23.00 | 3.00 |
| 31.42 | 23.00 | 3.00 |
| 33.65 | 23.00 | 3.00 |
| 35.88 | 23.00 | 3.00 |
| 38.11 | 23.00 | 3.00 |
| 40.34 | 23.00 | 3.00 |
| 42.57 | 23.00 | 3.00 |
| 44.80 | 23.00 | 3.00 |

Tailwater Channel Data - CD-6 Proposed

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 23.00 ft

Roadway Data for Crossing: CD-6 Proposed

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 1000.00 ft Crest Elevation: 26.00 ft Roadway Surface: Paved Roadway Top Width: 98.00 ft

| Project: | SR 46 PD&E Study (SR 415 to CR 426) | Design By: DEP | Date: | 8/7/2012 |
|----------|-------------------------------------|------------------|---------|----------|
| FIN No.: | 240216-4-28-01 | Checked by: DTL | Date: 9 | elis |
| Subject: | CD-7: 24" RCP (Sta 310+51.92) | Checked by. Dite | | 5/102 |

Existing Culvert

Note: Based on the Record of Conversation document dated Feb. 7th, 2012 between URS and FDOT Maintenance Office (Jim Wood), there is no recorded history of flooding problems associated with CD-7. Based on the URS site visit conducted on Feb. 12th, 2012 the headwall of the culvert was buried. It appears a turn lane had been added and the culvert was not extended. The pipe was nearly halfway filled with sediment at the Endwall. The existing concrete culvert has been lined with a plastic pipe insert to protect the roadway base due to leaks in the existing RCP joints. For the purpose of the PD&E Study, the existing culvert analysis shall ignore the plastic pipe insert as our understanding is this was a temporary solution. We will also ignore the existing turn lane addition and buried culvert as we understand this was a temporary condition to access an adjacent borrow pit. Approximate historical drainage area is 28.47 acres per existing SR 46 Plans. Due to no record of flooding at CD-7, Velocity Method shall be used for the analysis.

| Method used: | Velocity (v) = | <u>6 ft/s</u> | (Since no | history of pro | blems is known) |
|-----------------------|---|--|-----------|----------------|---|
| Existing Information: | Culvert Diameter: No of culverts: Exist culvert length: | <u>2 ft</u> ' <u>1</u> - 79.0 ft | | Material | : <u>RCP</u> |
| | Avge flowline elev upstream: | 20.10 | (NAVD) | (21.1 NGVD) | Per Existing SR 46 Plans |
| | Avge flowline elev downstream: | <u>20.00</u> 1 | (NAVD) | (21.0 NGVD) | Per Existing SR 46 Plans |
| | Longitudinal slope: | 0.001266 | = | <u>0.1266%</u> | 2 |
| | Tailwater: | <u>22.83</u> | (NAVD) | | Mark Stain on D/S End ately 10" above Crown1 |

Estimate discharge & Overtopping & HW for existing and proposed:

Area of culvert (A): <u>3.1 sq ft</u>

| Frequency | Factor | Q=Axv | HW Stage | HW Stage |
|-----------|--------|------------|----------|----------|
| | | | Existing | Proposed |
| | | | (Note 2) | (Note 3) |
| (yr) | | cu ft/s | | |
| 25 | | 18.8 | | |
| 50 | | 22.5 (Note | 24.69 | 25.45 |
| | | 1) | | |
| 100 | 1.4 | 26.4 | 25.39 | 26.44 |
| 500 | 1.7 | 44.8 | 27.02 | 27.03 |

| Overtopping | | | | | | | |
|-------------------|-------|-------|--|--|--|--|--|
| Existing Proposed | | | | | | | |
| Elev (NAVD) | 27.00 | 27.00 | | | | | |
| Q* (cfs) | 33.72 | 28.39 | | | | | |
| Freq (yr) | 308 | 143 | | | | | |

* From HY 8 culvert analysis

Note 1: Interpolated from Discharge vs Frequency graph (existing)

Note 2: Values obtained from HY 8 model of existing Culvert

Note 3: Values obtained from HY 8 model of proposed extension Culvert

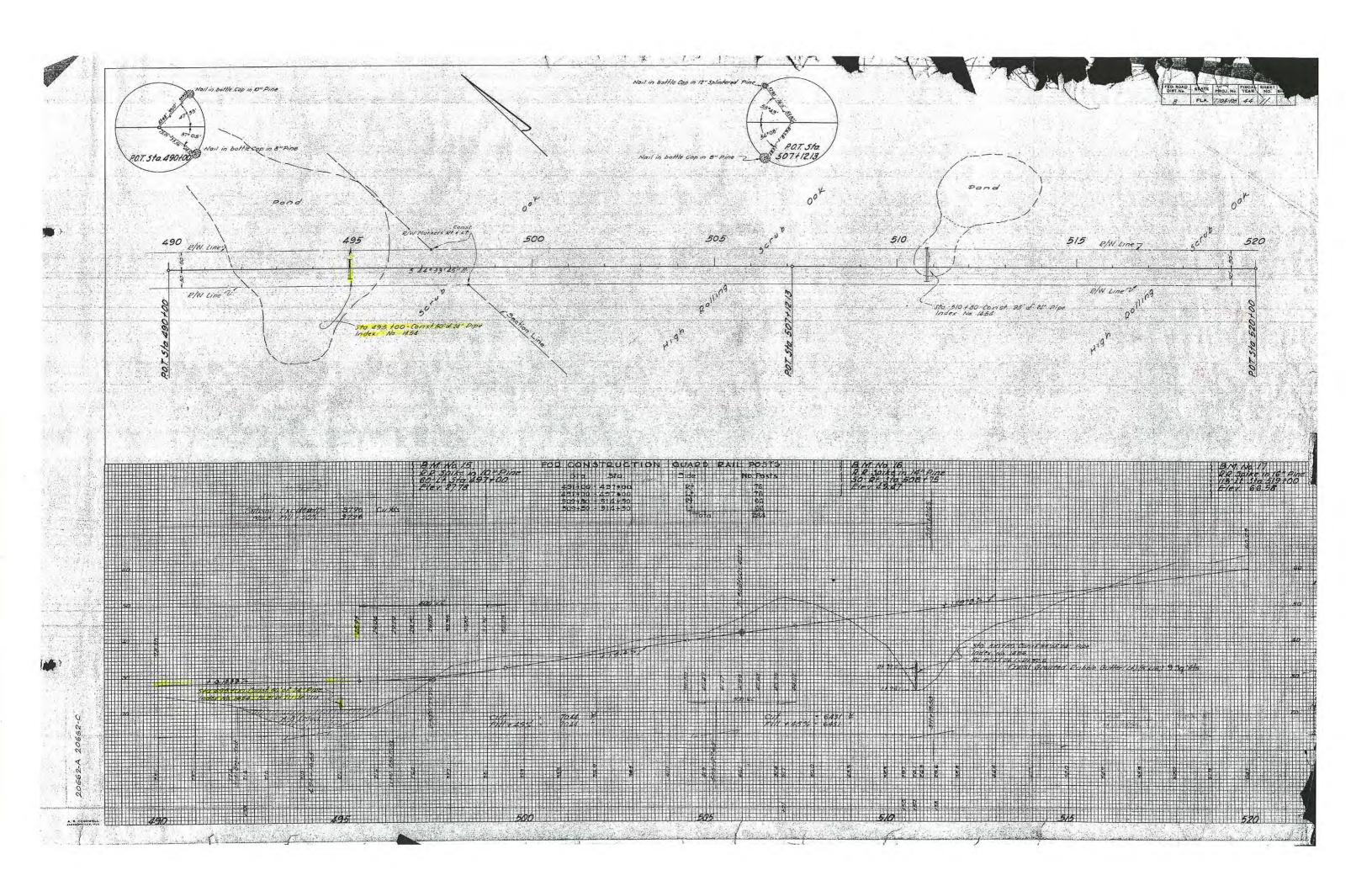
Proposed Culvert

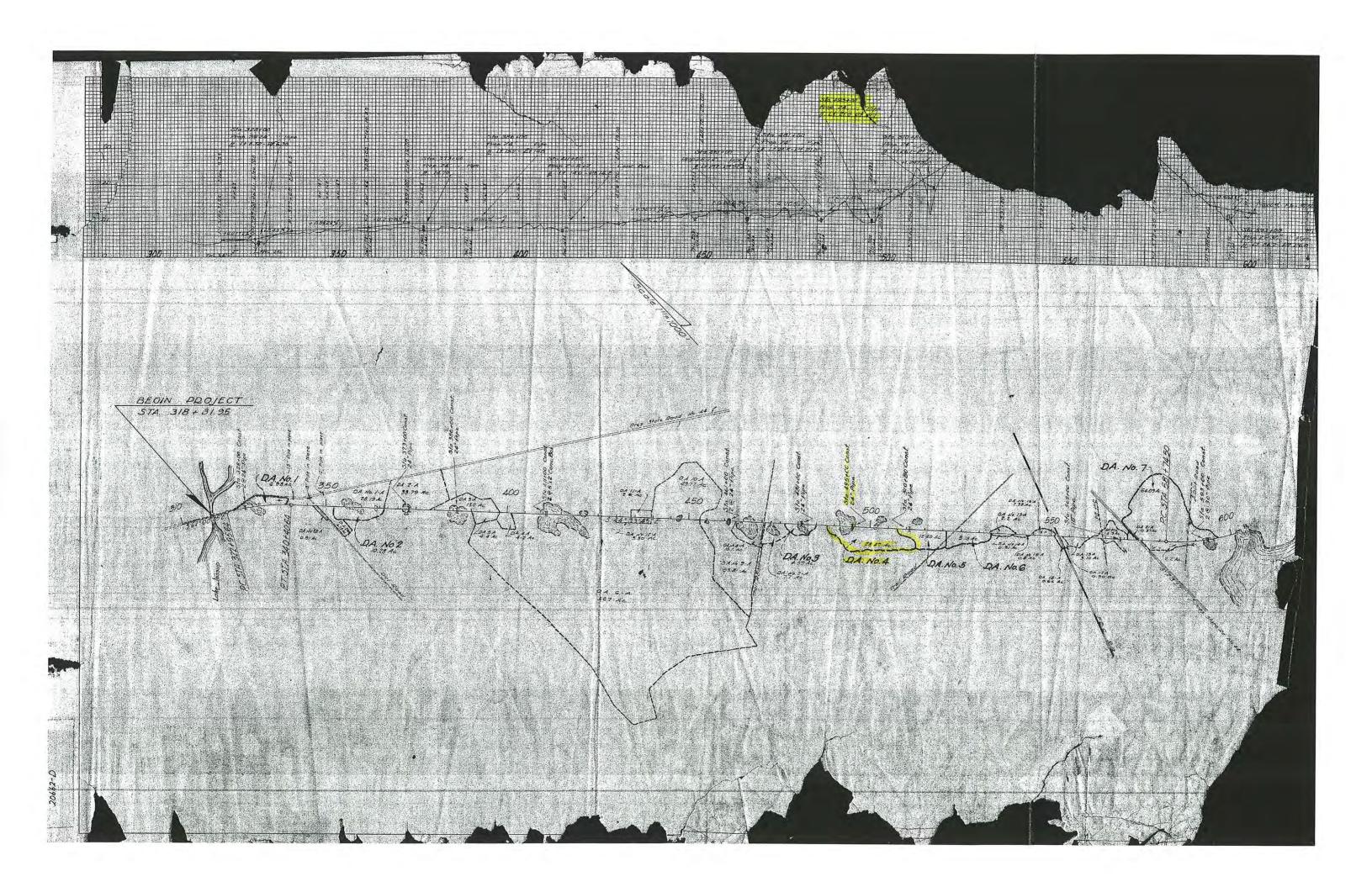
Note: Culvert replacement to be 24" RCP

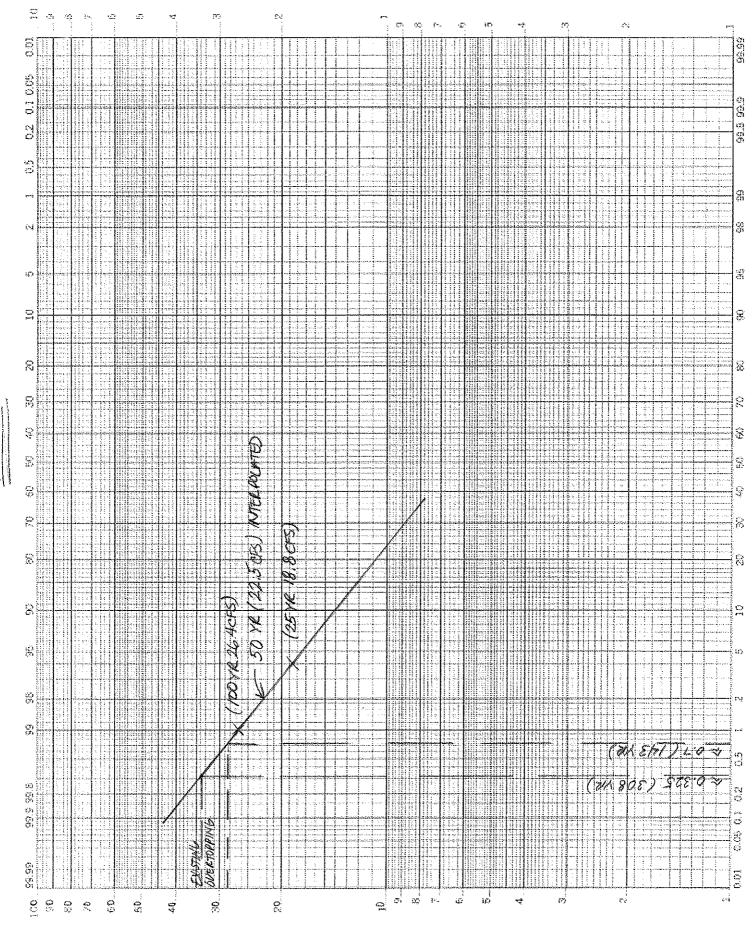
Assume allowable headwater (EOT) to be 6" below CL of Existing SR 46 = 26.5

Proposed Information

| | Extension | Invert |
|-----------------------------------|-----------|--------|
| | Length | (NAVD) |
| Upstream: | 75.3 ft | 20.10 |
| Downstream: | 15.7 ft | 19.90 |
| Total length of proposed culvert: | 170.0 ft | |







SID

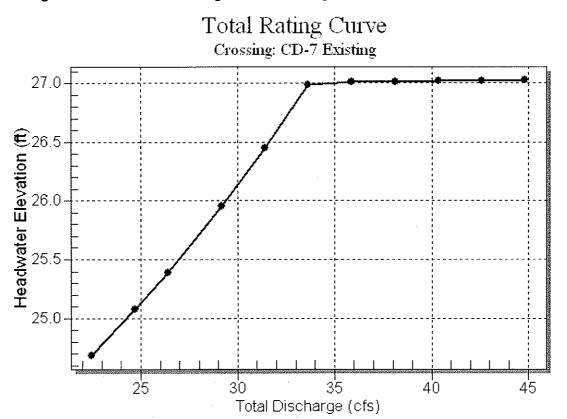
FREDVENCY

CD-7 Increases e Lago ender

HY-8 Culvert Analysis Report CD-7 (Existing 24" RCP)

| Headwater Elevation (ft) | Total Discharge (cfs) | CD-7 Existing Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------------------|-----------------------|----------------------------------|----------------------------|------------|
| 24.69 | 22.50 | 22.50 | 0.00 | 1 |
| 25.07 | 24.73 | 24.73 | 0.00 | 1 |
| 25.39 | 26.40 | 26.40 | 0.00 | 1 |
| 25.96 | 29.19 | 29.19 | 0.00 | 1 |
| 26.45 | 31.42 | 31.42 | 0.00 | 1 |
| 26.98 | 33.65 | 33.65 | 0.00 | 1 |
| 27.01 | 35.88 | 33.75 | 1.86 | 10 |
| 27.01 | 38.11 | 33.77 | 4.11 | 4 |
| 27.02 | 40.34 | 33.78 | 6.19 | 3 |
| 27,02 | 42.57 | 33.80 | 8.46 | 3 |
| 27.02 | 44.80 | 33.81 | 10.76 | 3 |

Table 1 - Summary of Culvert Flows at Crossing: CD-7 Existing



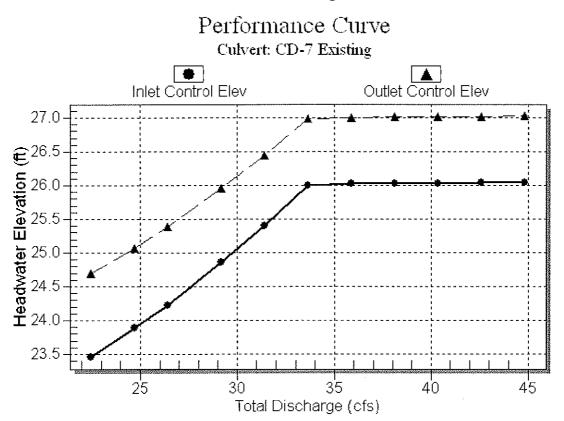
Rating Curve Plot for Crossing: CD-7 Existing

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (fl) | Outlet Velocity (fl/s) | Tailwater Velocity (fl/s) |
|-----------------------------|-------------------------------|--------------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|------------------------------|---------------------------------|
| 22.50 | 22.50 | 24.69 | 3.361 | 4.587 | 4-FFf | 2.000 | 1.678 | 2.000 | 2.830 | 7.162 | 0.000 |
| 24.73 | 24.73 | 25.07 | 3.782 | 4.973 | 4-FFf | 2.000 | 1.744 | 2.000 | 2.830 | 7,872 | 0.000 |
| 26.40 | 26.40 | 25.39 | 4,127 | 5.286 | 4-FFf | 2.000 | 1.793 | 2.000 | 2.830 | 8.403 | 0.000 |
| 29.19 | 29.19 | 25.96 | 4.757 | 5.855 | 4-FFf | 2.000 | 1.876 | 2.000 | 2.830 | 9.291 | 0.000 |
| 31.42 | 31.42 | 26.45 | 5.308 | 6.351 | 4-FFf | 2.000 | 1.941 | 2.000 | 2.830 | 10.001 | 0.000 |
| 33.65 | 33.65 | 26.98 | 5.898 | 6.883 | 4-FFf | 2.000 | 2.000 | 2.000 | 2.830 | 10,711 | 0.000 |
| 35.88 | 33.75 | 27.01 | 5.924 | 6.907 | 4-FFf | 2.000 | 2.000 | 2.000 | 2.830 | 10.741 | 0.000 |
| 38.11 | 33.77 | 27.01 | 5.929 | 6.912 | 4-FFf | 2.000 | 2.000 | 2.000 | 2.830 | 10.748 | • 0.000 |
| 40.34 | 33.78 | 27.02 | 5,935 | 6.917 | 4-FFf | 2.000 | 2.000 | 2.000 | 2.830 | 10.754 | 0.000 |
| 42.57 | 33.80 | 27.02 | 5.939 | 6.920 | 4-FFf | 2.000 | 2.000 | 2.000 | 2.830 | 10.759 | 0.000 |
| 44.80 | 33.81 | 27.02 | 5.943 | 6.924 | 4-FFf | 2.000 | 2.000 | 2,000 | 2.830 | 10.764 | 0.000 |

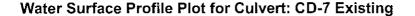
Table 2 - Culvert Summary Table: CD-7 Existing

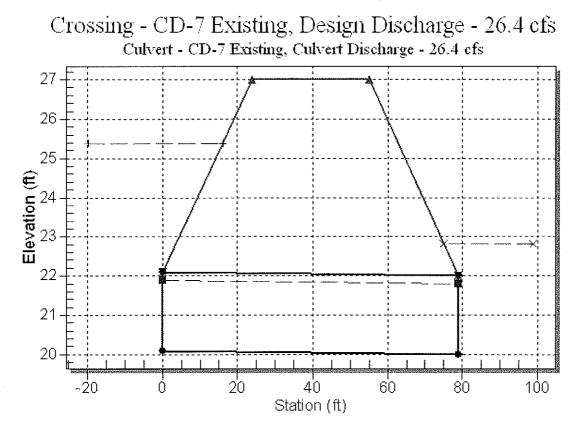
Inlet Elevation (invert): 20.10 ft, Outlet Elevation (invert): 20.00 ft

Culvert Length: 79.00 ft, Culvert Slope: 0.0013



Culvert Performance Curve Plot: CD-7 Existing





Site Data - CD-7 Existing

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 20.10 ft Outlet Station: 79.00 ft Outlet Elevation: 20.00 ft Number of Barrels: 1

Culvert Data Summary - CD-7 Existing

Barrel Shape: Circular Barrel Diameter: 2.00 ft Barrel Material: Concrete Barrel Manning's n: 0.0120 Inlet Type: Conventional Inlet Edge Condition: Square Edge with Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-7 Existing)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
|------------|-------------------------|------------|
| 22.50 | 22.83 | 2.83 |
| 24.73 | 22.83 | 2.83 |
| 26.40 | 22.83 | 2.83 |
| 29.19 | 22.83 | 2.83 |
| 31.42 | 22.83 | 2.83 |
| 33.65 | 22.83 | 2.83 |
| 35.88 | 22.83 | 2.83 |
| 38.11 | 22.83 | 2.83 |
| 40.34 | 22.83 | 2.83 |
| 42.57 | 22.83 | 2.83 |
| 44.80 | 22.83 | 2.83 |

Tailwater Channel Data - CD-7 Existing

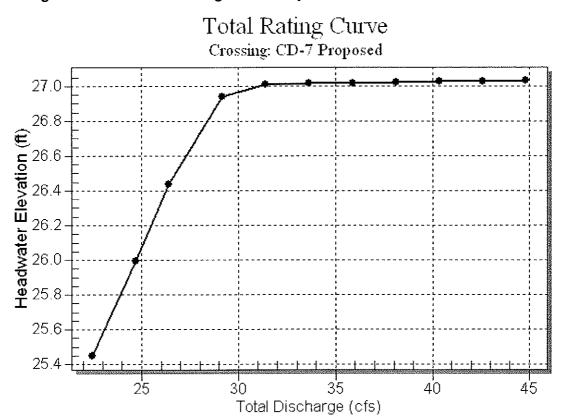
Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 22.83 ft

Roadway Data for Crossing: CD-7 Existing

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 1000.00 ft Crest Elevation: 27.00 ft Roadway Surface: Paved Roadway Top Width: 31.00 ft HY-8 Culvert Analysis Report CD-7 (Proposed 24" RCP)

| Headwater Elevation (ft) | Total Discharge (cfs) | CD-7 Proposed Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------------------|-----------------------|----------------------------------|----------------------------|------------|
| 25.45 | 22.50 | 22.50 | 0.00 | 1 |
| 25.99 | 24.73 | 24.73 | 0.00 | 1 |
| 26.44 | 26.40 | 26.40 | 0.00 | 1 |
| 26.94 | 29.19 | 28.19 | 0.00 | 50 |
| 27.01 | 31.42 | 28.42 | 2.78 | 15 |
| 27.01 | 33.65 | 28.44 | 5.04 | 4 |
| 27.02 | 35.88 | 28.45 | 7.13 | 3 |
| 27.02 | 38.11 | 28.46 | 9.39 | 3 |
| 27.03 | 40.34 | 28.47 | 11.68 | 3 |
| 27.03 | 42.57 | 28.48 | 13.95 | 3 |
| 27.03 | 44.80 | 28.49 | 16.21 | 3 |

Table 1 - Summary of Culvert Flows at Crossing: CD-7 Proposed



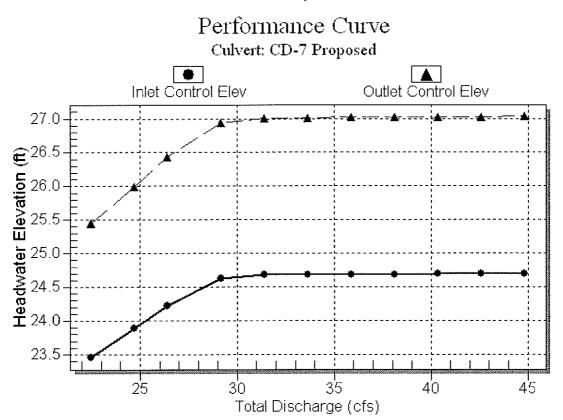
Rating Curve Plot for Crossing: CD-7 Proposed

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | inlet Control Depth (fl) | Outlet Control Depth (ff) | Flow Type | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
|-----------------------------|-------------------------------|--------------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|------------------------------|---------------------------------|
| 22.50 | 22.50 | 25.45 | 3.361 | 5,350 | 4-FFf | 2.000 | 1.678 | 2.000 | 2.830 | 7.162 | 0.000 |
| 24.73 | 24.73 | 25.99 | 3.782 | 5.895 | 4-FFf | 2.000 | 1.744 | 2.000 | 2.830 | 7,872 | 0,000 |
| 26.40 | 26.40 | 26.44 | 4.127 | 6.336 | 4-FFf | 2.000 | 1.793 | 2.000 | 2,830 | 8.403 | 0.000 |
| 29.19 | 28.19 | 26.94 | 4.523 | 6.841 | 4-FFf | 2.000 | 1.846 | 2.000 | 2.830 | 8.972 | 0.000 |
| 31.42 | 28.42 | 27.01 | 4.577 | 6.910 | 4-FFf | 2.000 | 1.853 | 2.000 | 2.830 | 9.047 | 0.000 |
| 33.65 | 28.44 | 27.01 | 4.581 | 6.914 | 4-FFf | 2.000 | 1.854 | 2.000 | 2.830 | 9,052 | 0.000 |
| 35.88 | 28.45 | 27.02 | 4.584 | 6.918 | 4-FFf | 2.000 | 1.854 | 2.000 | 2.830 | 9.056 | 0.000 |
| 38.11 | 28.46 | 27.02 | 4.587 | 6.922 | 4-FFf | 2.000 | 1.854 | 2.000 | 2.830 | 9.060 | 0.000 |
| 40.34 | 28.47 | 27.03 | 4.589 | 6.925 | 4-FFf | 2.000 | 1.855 | 2.000 | 2.830 | 9.064 | 0.000 |
| 42.57 | 28.48 | 27.03 | 4.592 | 6.928 | 4-FFf | 2.000 | 1.855 | 2.000 | 2.830 | 9.067 | 0.000 |
| 44.80 | 28.49 | 27.03 | 4.594 | 6.931 | 4-FFf | 2.000 | 1.855 | 2.000 | 2.830 | 9.070 | 0.000 |

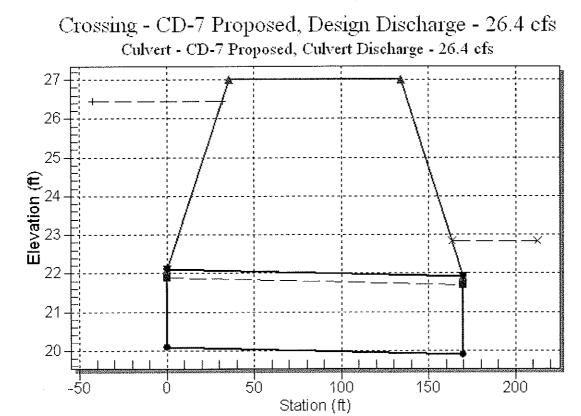
Table 2 - Culvert Summary Table: CD-7 Proposed

Inlet Elevation (invert): 20.10 ft, Outlet Elevation (invert): 19.90 ft

Culvert Length: 170.00 ft, Culvert Slope: 0.0012



Culvert Performance Curve Plot: CD-7 Proposed



Water Surface Profile Plot for Culvert: CD-7 Proposed



Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 20.10 ft Outlet Station: 170.00 ft Outlet Elevation: 19.90 ft Number of Barrels: 1

Culvert Data Summary - CD-7 Proposed

Barrel Shape: Circular Barrel Diameter: 2.00 ft Barrel Material: Concrete Barrel Manning's n: 0.0120 Inlet Type: Conventional Inlet Edge Condition: Square Edge with Headwall Inlet Depression: None

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
|------------|-------------------------|------------|
| 22.50 | 22.83 | 2.83 |
| 24.73 | 22.83 | 2.83 |
| 26.40 | 22.83 | 2.83 |
| 29.19 | 22.83 | 2.83 |
| 31.42 | 22.83 | 2.83 |
| 33.65 | 22.83 | 2.83 |
| 35.88 | 22.83 | 2.83 |
| 38.11 | 22.83 | 2.83 |
| 40.34 | 22.83 | 2.83 |
| 42.57 | 22.83 | 2.83 |
| 44.80 | 22.83 | 2.83 |

Table 3 - Downstream Channel Rating Curve (Crossing: CD-7 Proposed)

Tailwater Channel Data - CD-7 Proposed

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 22.83 ft

Roadway Data for Crossing: CD-7 Proposed

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 1000.00 ft Crest Elevation: 27.00 ft Roadway Surface: Paved Roadway Top Width: 98.00 ft

| Project: | SR 46 PD&E Study (SR 415 to CR 426) | Design By: <u>DEP</u> | Date: | 8/7/2012 |
|----------|-------------------------------------|-----------------------|---------|----------|
| FIN No.: | 240216-4-28-01 | Checked by: DTL | Date: 9 | relia |
| Subject: | CD-8; 24" RCP (Sta 326+72.92) | | | |

Existing Culvert

Note: Based on the Record of Conversation document dated Feb. 7th, 2012 between URS and FDOT Maintenance Office (Jim Wood), there is no recorded history of flooding problems associated with CD-8. Based on the URS site visit conducted on Feb. 12th, 2012 the Endwall was buried. It appears that the sandy soils on the embankment have washed into the front of the Endwall to bury the pipe. The existing concrete culvert has been lined with a plastic pipe insert to protect the roadway base due to leaks in the existing RCP joints. For the purpose of the PD&E Study, the existing culvert analysis shall ignare the plastic pipe insert as our understanding is this was a temporary solution. We will also ignore the burried Endwall as we understand this condition shall be cleaned up by the maintenance department. The tailwater shall be assumed at the crown of the existing endwall. Approximate historical drainage area is 12.4 acres per existing SR 46 Plans. Due to no record of flooding at CD-8, Velocity Method shall be used for the analysis.

| Velocity (v) = | <u>6 ft/s</u> | (Since no history of problems is known) | | |
|---|--|--|--|---|
| Culvert Diameter: No of culverts: Exist culvert length: | <u>2 ft</u> <u>1</u> 100.0 ft | | Material | : <u>RCP</u> |
| Avge flowline elev upstream: | 31.60 | (NAVD) | (32.6 NGVD) | <u>Per Existing SR 46 Plans</u> |
| Avge flowline elev downstream: | <u>25.10</u> ′ | (NAVD) | (26.1 NGVD) | Per Existing SR 46 Plans |
| Longitudinal slope: | 0.065000 | = | <u>6.5000%</u> | 2 |
| Tailwater: | <u>27.10</u> | {NAVD} | <u>Endwall Bur</u> | ried, Crown assumed, |
| | Culvert Diameter: No of culverts: Exist culvert length: Avge flowline elev upstream: Avge flowline elev downstream: Longitudinal slope: | Culvert Diameter: <u>2 ft</u> No of culverts: <u>1</u> Exist culvert length: <u>100.0 ft</u> Avge flowline elev upstream: <u>31.60</u> Avge flowline elev downstream: <u>25.10</u> Longitudinal slope: 0.065000 | Culvert Diameter: <u>2 ft</u> No of culverts: <u>1</u> Exist culvert length: <u>100.0 ft</u> Avge flowline elev upstream: <u>31.60</u> (NAVD) Avge flowline elev downstream: <u>25.10</u> (NAVD) Longitudinal slope: 0.065000 = | Culvert Diameter: <u>2 ft</u> No of culverts: <u>1</u> Exist culvert length: <u>100.0 ft</u> Avge flowline elev upstream: <u>31.60</u> (NAVD) (32.6 NGVD) Avge flowline elev downstream: <u>25.10</u> (NAVD) (26.1 NGVD) Longitudinal slope: 0.065000 = <u>6.5000%</u> |

Estimate discharge & Overtopping & HW for existing and proposed:

Area of culvert (A): <u>3.1 sa ft</u>

| Frequency | Factor | Q = A x v | HW Stage | HW Stage |
|-----------|--------|------------|----------|----------|
| | | | Existing | Proposed |
| | | | (Note 2) | (Note 3) |
| (yr) | | cu ft/s | | |
| 25 | | 18.8 | | |
| 50 | | 22.5 (Note | 34.9 | 34,92 |
| | | 1) | | |
| 100 | 1.4 | 26.4 | 35.66 | 35.69 |
| 500 | 1.7 | 44.8 | 41.15 | 41.2 |

| Overtopping | | | | | |
|-------------|----------|----------|--|--|--|
| | Existing | Proposed | | | |
| Elev (NAVD) | 44.50 | 44.50 | | | |
| Q* (cfs) | 52.86 | 52.71 | | | |
| Freq (yr) | >500 | >500 | | | |

* From HY 8 culvert analysis

Note 1: Interpolated from Discharge vs Frequency graph (existing)

Note 2: Values obtained from HY 8 model of existing Culvert

Note 3: Values obtained from HY 8 model of proposed extension Culvert

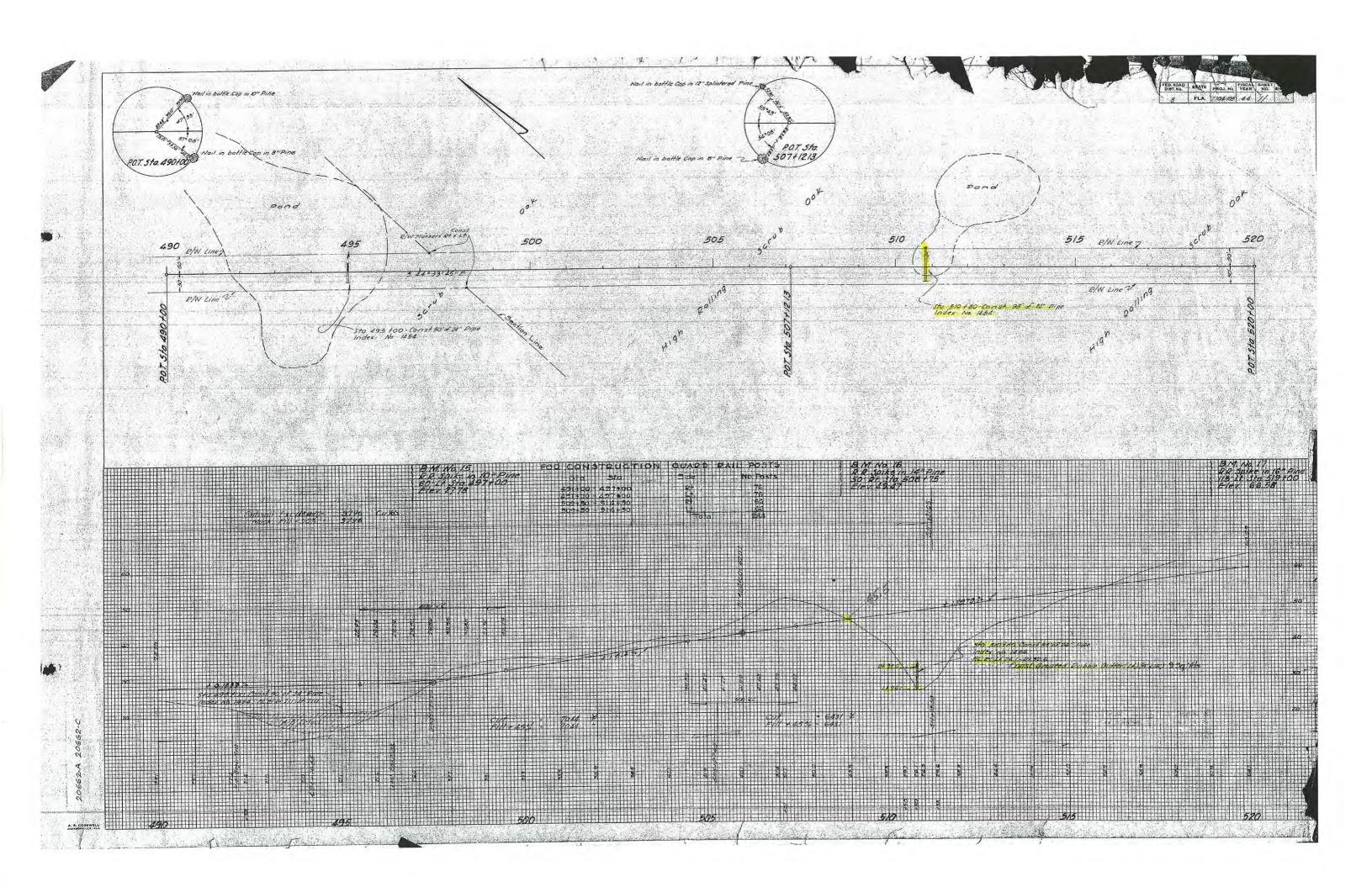
Proposed Culvert

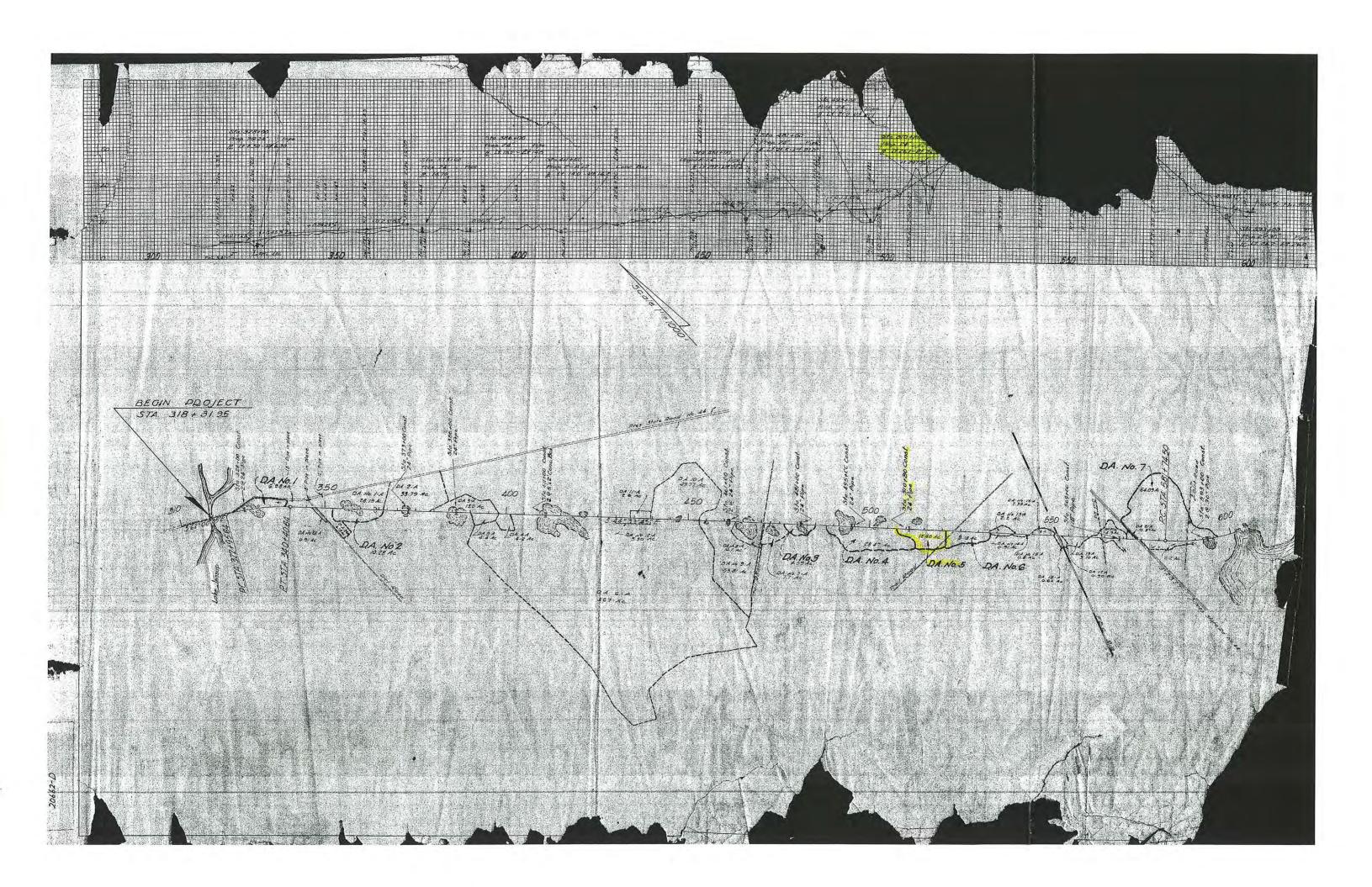
Note: Cuvert replacement to be 24" RCP

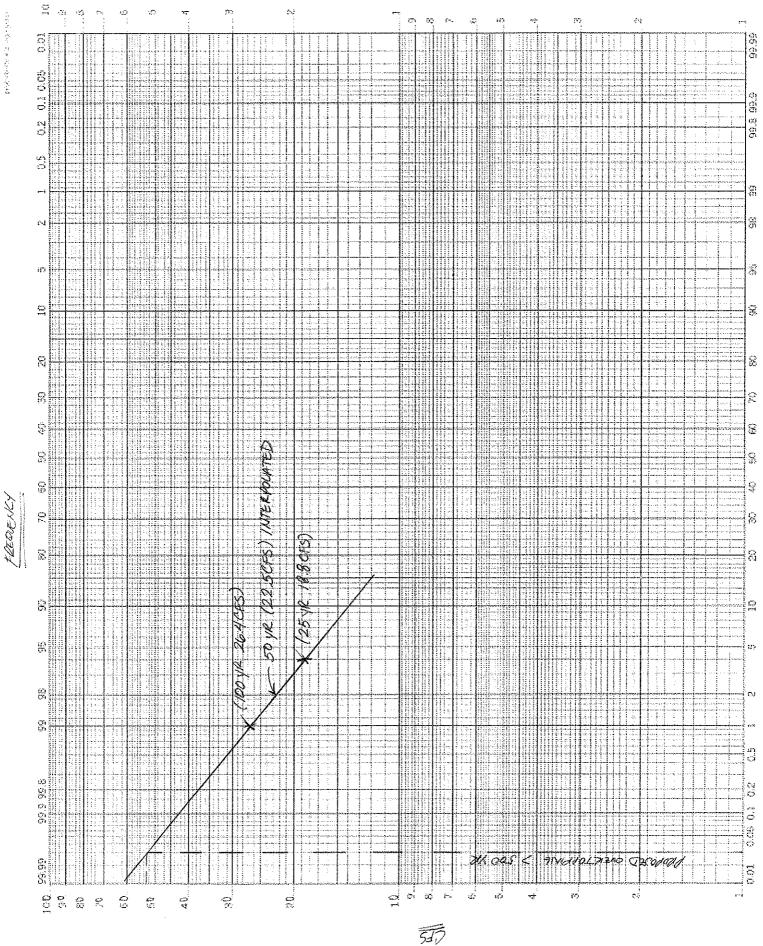
Assume allowable headwater (EOT) to be 6" below CL of Existing SR 46 = 44

Proposed Information

| | Extension | Invert |
|-----------------------------------|-----------|--------|
| | Length | (NAVD) |
| Upstream: | 67.6 ft | 31.60 |
| Downstream: | 2.4 ft | 25.10 |
| Total length of proposed culvert: | 170.0 ft | |





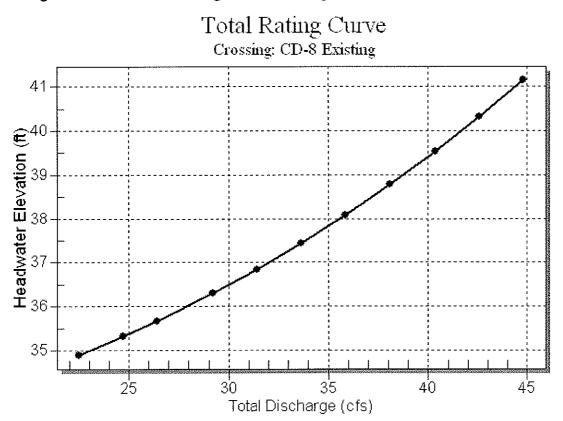


CD-B Production of system

HY-8 Culvert Analysis Report CD-8 (Existing 24" RCP)

| Headwater Elevation (ft) | Total Discharge (cfs) | CD-8 Existing Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------------------|-----------------------|----------------------------------|----------------------------|------------|
| 34.90 | 22.50 | 22.50 | 0.00 | 1 |
| 35.32 | 24.73 | 24.73 | 0.00 | 1 |
| 35.66 | 26.40 | 26.40 | 0.00 | 1 |
| 36.29 | 29.19 | 29.19 | 0.00 | 1 |
| 36.84 | 31.42 | 31.42 | 0.00 | 1 |
| 37.43 | 33.65 | 33.65 | 0.00 | 1 |
| 38.08 | 35.88 | 35.88 | 0.00 | 1 |
| 38.79 | 38,11 | 38.11 | 0.00 | 1 |
| 39.53 | 40.34 | 40.34 | 0.00 | 1 |
| 40.32 | 42.57 | 42.57 | 0.00 | 1 |
| 41.15 | 44.80 | 44.80 | 0.00 | 1 |

Table 1 - Summary of Culvert Flows at Crossing: CD-8 Existing



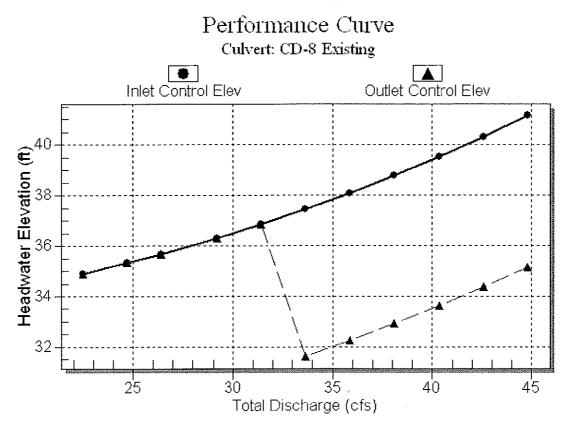
Rating Curve Plot for Crossing: CD-8 Existing

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Iniet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (fVs) | Tailwater Velocity (ft/s) |
|-----------------------------|-------------------------------|--------------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|-----------------------------|---------------------------------|
| 22.50 | 22.50 | 34.90 | 3.298 | 3.298 | 5-S1f | 0.827 | 1.678 | 1.678 | 2.000 | 8.020 | 0.000 |
| 24.73 | 24.73 | 35.32 | 3.719 | 3.719 | 5-S1f | 0.871 | 1.744 | 1.744 | 2.000 | 8.531 | 0.000 |
| 26.40 | 26.40 | 35.66 | 4.063 | 4.063 | 5-S1f | 0.904 | 1.793 | 1.793 | 2.000 | 8.893 | 0.000 |
| 29,19 | 29.19 | 36.29 | 4.694 | 4.694 | 5-S1f | 0,959 | 1,876 | 1.876 | 2.000 | 9.602 | 0.000 |
| 31.42 | 31.42 | 36.84 | 5.244 | 5.244 | 1-S1f | 1.002 | 1.941 | 1.941 | 2,000 | 10,156 | 0.000 |
| 33.65 | 33.65 | 37.43 | 5.834 | 0.037 | 5-S2n | 1.044 | 2.000 | 1.119 | 2.000 | 18.620 | 0.000 |
| 35.88 | 35.88 | 38.08 | 6.484 | 0.660 | 5-S2n | 1.085 | 2,000 | 1.165 | 2.000 | 18.898 | 0.000 |
| 38.11 | 38.11 | 38.79 | 7.186 | 1.323 | 5-S2n | 1.127 | 2.000 | 1.212 | 2.000 | 19.132 | 0.000 |
| 40.34 | 40.34 | 39.53 | 7.932 | 2.027 | 5-S2n | 1.168 | 2.000 | 1.260 | 2.000 | 19.372 | 0.000 |
| 42.57 | 42.57 | 40.32 | 8.719 | 2.770 | 5-S2n | 1.210 | 2.000 | 1.308 | 2.000 | 19.584 | 0.000 |
| 44.80 | 44.80 | 41.15 | 9.549 | 3,553 | 5-S2n | 1.253 | 2.000 | 1.352 | 2.000 | 19.845 | 0.000 |

Table 2 - Culvert Summary Table: CD-8 Existing

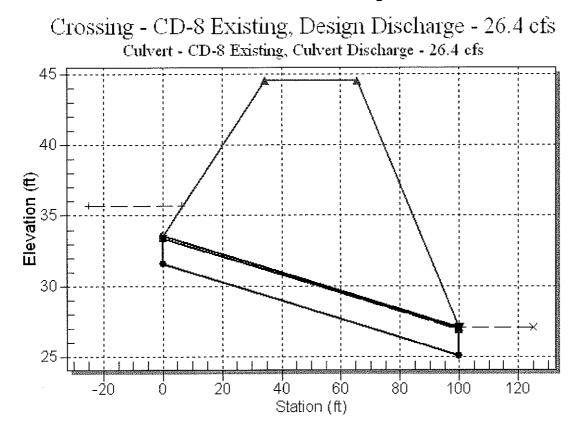
Inlet Elevation (invert): 31.60 ft, Outlet Elevation (invert): 25.10 ft

Culvert Length: 100.21 ft, Culvert Slope: 0.0650



Culvert Performance Curve Plot: CD-8 Existing

Water Surface Profile Plot for Culvert: CD-8 Existing



Site Data - CD-8 Existing

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 31.60 ft Outlet Station: 100.00 ft Outlet Elevation: 25.10 ft Number of Barrels: 1

Culvert Data Summary - CD-8 Existing

Barrel Shape: Circular Barrel Diameter: 2.00 ft Barrel Material: Concrete Barrel Manning's n: 0.0120 Inlet Type: Conventional Inlet Edge Condition: Square Edge with Headwall Inlet Depression: None

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
|------------|-------------------------|------------|
| 22.50 | 27.10 | 2.00 |
| 24.73 | 27.10 | 2.00 |
| 26.40 | 27.10 | 2.00 |
| 29.19 | 27.10 | 2.00 |
| 31.42 | 27.10 | 2.00 |
| 33.65 | 27.10 | 2,00 |
| 35.88 | 27.10 | 2.00 |
| 38.11 | 27.10 | 2.00 |
| 40.34 | 27.10 | 2.00 |
| 42.57 | 27.10 | 2.00 |
| 44.80 | 27.10 | 2.00 |

Table 3 - Downstream Channel Rating Curve (Crossing: CD-8 Existing)

Tailwater Channel Data - CD-8 Existing

Tailwater Channel Option:Enter Constant Tailwater ElevationConstant Tailwater Elevation:27.10 ft

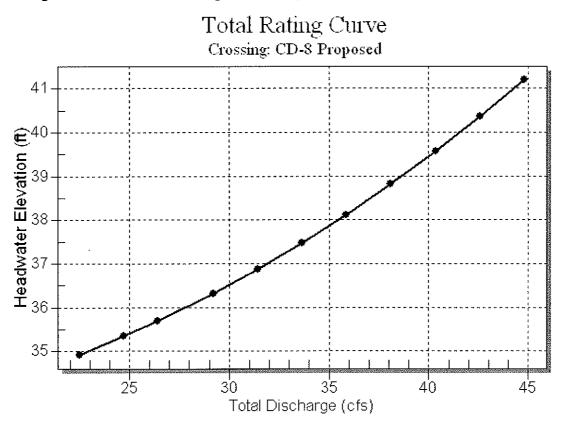
Roadway Data for Crossing: CD-8 Existing

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 1000.00 ft Crest Elevation: 44.50 ft Roadway Surface: Paved Roadway Top Width: 31.00 ft HY-8 Culvert Analysis Report CD-8 (Proposed 24" RCP)

| Headwater Elevation (ft) | Total Discharge (cfs) | CD-8 Proposed Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------------------|-----------------------|----------------------------------|----------------------------|------------|
| 34.92 | 22.50 | 22.50 | 0.00 | 1 |
| 35.35 | 24.73 | 24.73 | 0.00 | 1 |
| 35.69 | 26.40 | 26.40 | 0.00 | 1 |
| 36.32 | 29.19 | 29.19 | 0.00 | 1 |
| 36.87 | 31.42 | 31.42 | 0.00 | 1 |
| 37.46 | 33.65 | 33.65 | 0.00 | 1 |
| 38.11 | 35.88 | 35.88 | 0.00 | 1 |
| 38.82 | 38.11 | 38.11 | 0.00 | 1 |
| 39.57 | 40.34 | 40.34 | 0.00 | 1 |
| 40.36 | 42.57 | 42.57 | 0.00 | 1 |
| 41.20 | 44.80 | 44.80 | 0.00 | 1 |

Table 1 - Summary of Culvert Flows at Crossing: CD-8 Proposed

,



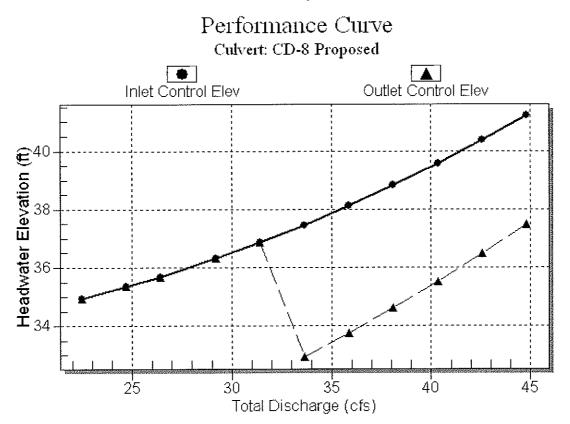
Rating Curve Plot for Crossing: CD-8 Proposed

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (fl) | Flow Type | Normal Depth (ft) | Critical Depth (fl) | Outlet Depth (fl) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
|-----------------------------|-------------------------------|--------------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|------------------------------|---------------------------------|
| 22.50 | 22.50 | 34.92 | 3.324 | 3.324 | 5-S1f | 0.961 | 1.678 | 1.678 | 2.000 | 8.020 | 0.000 |
| 24.73 | 24.73 | 35.35 | 3.745 | 3.745 | 5-S1f | 1.017 | 1,744 | 1,744 | 2.000 | 8,531 | 0.000 |
| 26.40 | 26.40 | 35.69 | 4.090 | 4.090 | 5-S1f | 1.058 | 1,793 | 1.793 | 2.000 | 8.893 | 0.000 |
| 29.19 | 29.19 | 36.32 | 4.720 | 4,720 | 5-S1f | 1,126 | 1.876 | 1.876 | 2.000 | 9.602 | 0.000 |
| 31.42 | 31.42 | 36.87 | 5.271 | 5.271 | 1-S1f | 1.180 | 1.941 | 1.941 | 2.000 | 10.156 | 0.000 |
| 33.65 | 33.65 | 37,46 | 5.861 | 1.357 | 5-S2n | 1.235 | 2.000 | 1,235 | 2.000 | 16,514 | 0.000 |
| 35.88 | 35.88 | 38.11 | 6.514 | 2.159 | 5-S2n | 1.291 | 2.000 | 1.324 | 2.000 | 16.282 | 0.000 |
| 38.11 | 38.11 | 38.82 | 7.221 | 3.013 | 5-S2n | 1.347 | 2.000 | 1.349 | 2.000 | 16.924 | 0.000 |
| 40.34 | 40.34 | 39.57 | 7.971 | 3.919 | 5-S2n | 1,404 | 2.000 | 1.405 | 2.000 | 17.106 | 0.000 |
| 42.57 | 42.57 | 40.36 | 8.763 | 4.876 | 5-S2n | 1.470 | 2.000 | 1.510 | 2.000 | 16.770 | 0.000 |
| 44.80 | 44.80 | 41.20 | 9.597 | 5.885 | 5-S2n | 1.537 | 2.000 | 1.539 | 2.000 | 17.304 | 0.000 |

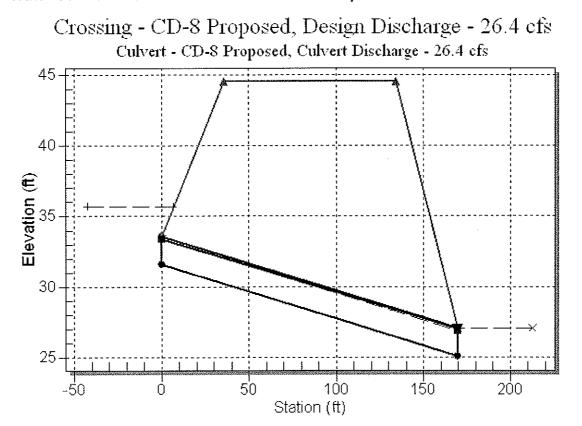
Table 2 - Culvert Summary Table: CD-8 Proposed

Inlet Elevation (invert): 31.60 ft, Outlet Elevation (invert): 25.10 ft

Culvert Length: 170.12 ft, Culvert Slope: 0.0382



Culvert Performance Curve Plot: CD-8 Proposed



Water Surface Profile Plot for Culvert: CD-8 Proposed

Site Data - CD-8 Proposed

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 31.60 ft Outlet Station: 170.00 ft Outlet Elevation: 25.10 ft Number of Barrels: 1

Culvert Data Summary - CD-8 Proposed

Barrel Shape: Circular Barrel Diameter: 2.00 ft Barrel Material: Concrete Barrel Manning's n: 0.0120 Inlet Type: Conventional Inlet Edge Condition: Square Edge with Headwall Inlet Depression: None

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) | |
|------------|-------------------------|------------|--|
| 22.50 | 27.10 | 2.00 | |
| 24.73 | 27.10 | 2.00 | |
| 26.40 | 27.10 | 2.00 | |
| 29.19 | 27.10 | 2.00 | |
| 31.42 | 27.10 | 2.00 | |
| 33.65 | 27.10 | 2.00 | |
| 35.88 | 27.10 | 2.00 | |
| 38.11 | 27.10 | 2.00 | |
| 40.34 | 27.10 | 2.00 | |
| 42.57 | 27.10 | 2.00 | |
| 44.80 | 27.10 | 2.00 | |

Table 3 - Downstream Channel Rating Curve (Crossing: CD-8 Proposed)

Tailwater Channel Data - CD-8 Proposed

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 27.10 ft

Roadway Data for Crossing: CD-8 Proposed

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 1000.00 ft Crest Elevation: 44.50 ft Roadway Surface: Paved Roadway Top Width: 98.00 ft

| Project: | SR 46 PD&E Study (SR 415 to CR 426) | Design By: <u>DEP</u> | Date: | <u>8/7/2012</u> |
|----------|-------------------------------------|-----------------------|-------|-----------------|
| FIN No.: | <u>240216-4-28-01</u> | | Date: | abolia |
| Subject: | CD-9: 18" RCP (Sta 384+60.16) | Checked by, b | Dule. | - for a f & and |

Existing Culvert

Note: Based on the Record of Conversation document dated Feb. 7th, 2012 between URS and FDOT Maintenance Office (Jim Wood), there is no recorded history of flooding problems associated with CD-9. Based on the URS site visit conducted on Feb. 12th, 2012 there are no apparent erosion problems. The existing concrete culvert has been lined with a plastic pipe insert to protect the roadway base due to leaks in the existing RCP joints. For the purpose of the PD&E Study, the existing culvert analysis shall ignore the plastic pipe insert as our understanding is this was a temporary solution. Approximate historical drainage area is 5.9 acres per existing SR 46 Plans. Due to no record of flooding at CD-9, Velocity Method shall be used for the analysis.

| Method used: | Velocity (v) = | <u>6 ft/s</u> | (Since no | history of pro | blems is known) |
|-----------------------|---|-----------------------------------|-----------|-------------------|------------------------------|
| Existing Information: | Culvert Diameter: No of culverts: Exist culvert length: | <u>1.5</u> <u>1</u> 74.0 ft | | Material | : <u>RCP</u> |
| | Avge flowline elev upstream: | 58.50 | (NAVD) | (59.5 NGVD) | Per Existing SR 46 Plans |
| | Avge flowline elev downstream: | <u>58.40</u> ′ | (NAVD) | (59.4 NGVD) | Per Existing SR 46 Plans |
| | Longitudinal slope: | 0.001351 | = | <u>0.1351%</u> | 2 |
| | Tailwater: | <u>59.90</u> | (NAVD) | <u>Assume Cra</u> | <u>own of Pipe, no stain</u> |
| | | | | <u>mark locat</u> | <u>ed on Endwall</u> |

1.8 s<u>q.ft</u>

Estimate discharge & Overtopping & HW for existing and proposed:

Area af culvert (A):

| Frequency | Factor | Q=Axv | HW Stage | HW Stage |
|-----------|--------|------------|----------|----------|
| | | | Existing | Propased |
| | | | (Note 2) | (Note 3) |
| (yr) | | cu ft/s | | |
| 25 | | 10.6 | | |
| 50 | ~~~~ | 12.5 (Note | 61.95 | 60.54 |
| | | 1) | | |
| 100 | 1.4 | 14.8 | 62.01 | 60.79 |
| 500 | 1.7 | 25.2 | 62.03 | 62.01 |

Note 1: Interpolated from Discharge vs Frequency graph (existing) Note 2: Values obtained from HY 8 model of existing CBC

Note 3: Values obtained from HY 8 model of proposed extension CBC

Proposed Culvert

Note: Culvert replacement to be 24" RCP

Assume allowable headwater (EOT) to be 6" below CL of Existing SR 46 = 61.5

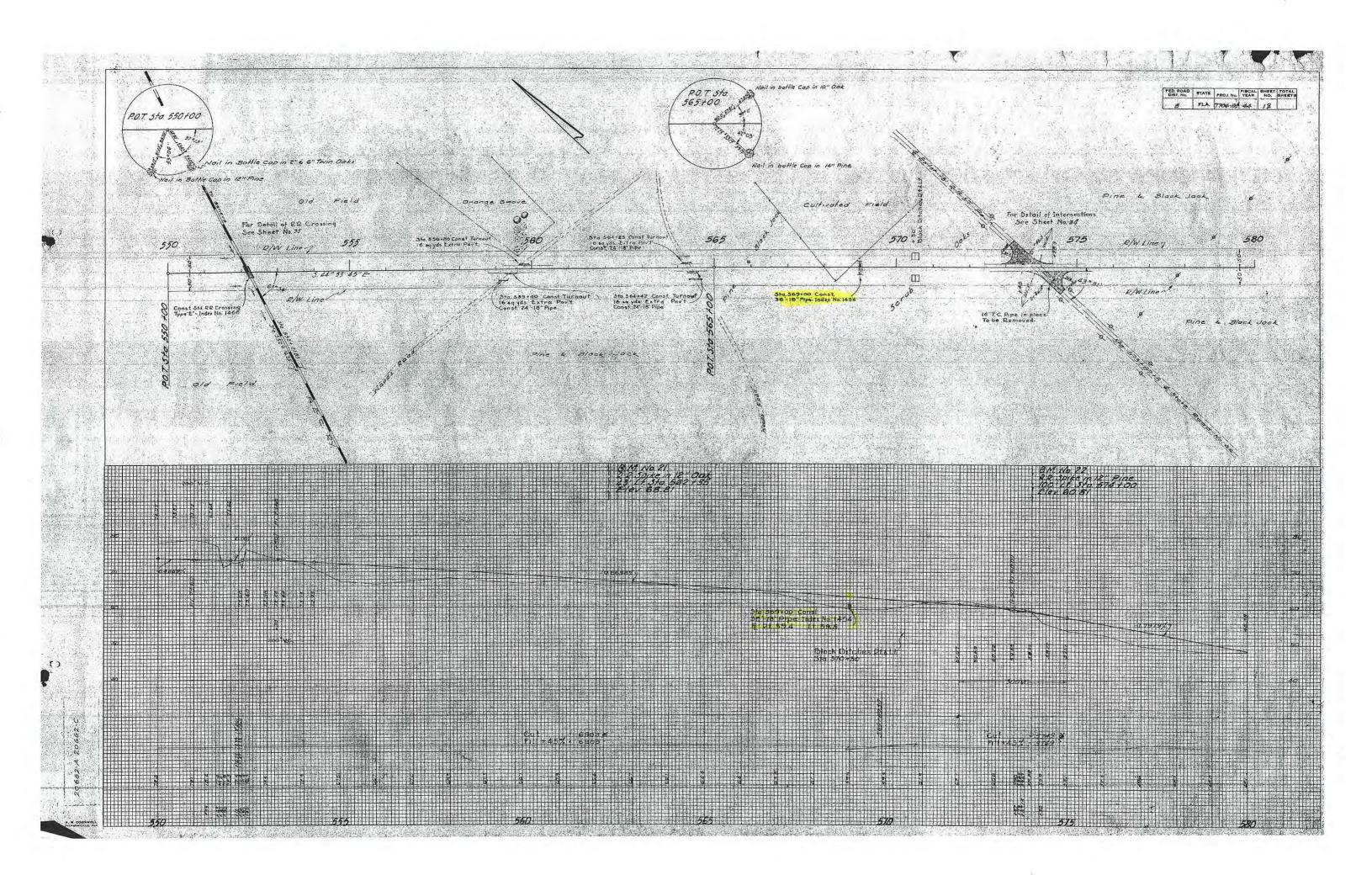
Proposed Information

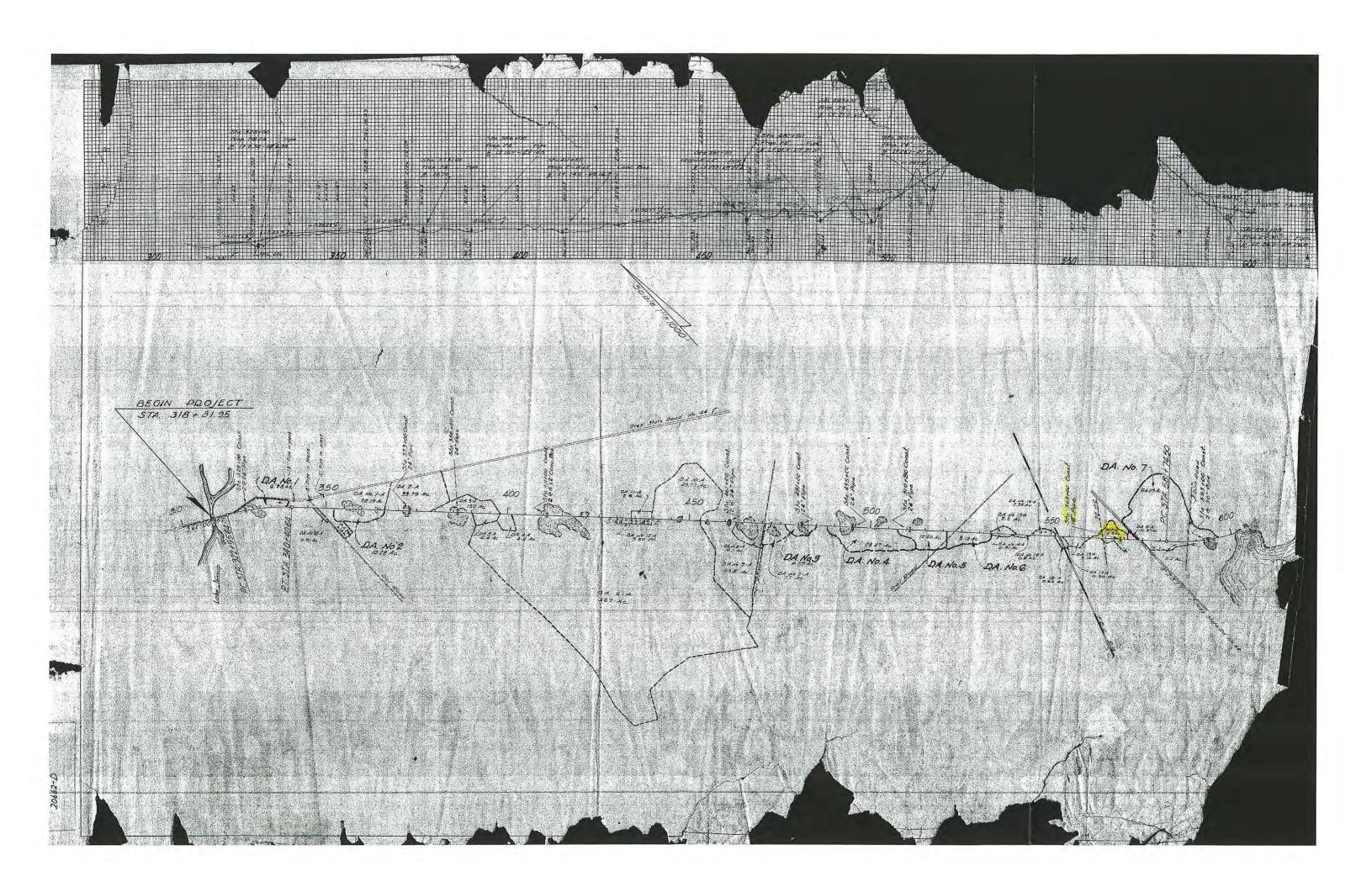
| | Extension | Invert |
|-----------------------------------|-----------|--------|
| | Length | (NAVD) |
| Upstream: | 9.3 ft | 58.00 |
| Downstream: | 20.7 ft | 57.90 |
| Total length of proposed culvert: | 104.0 ft | |

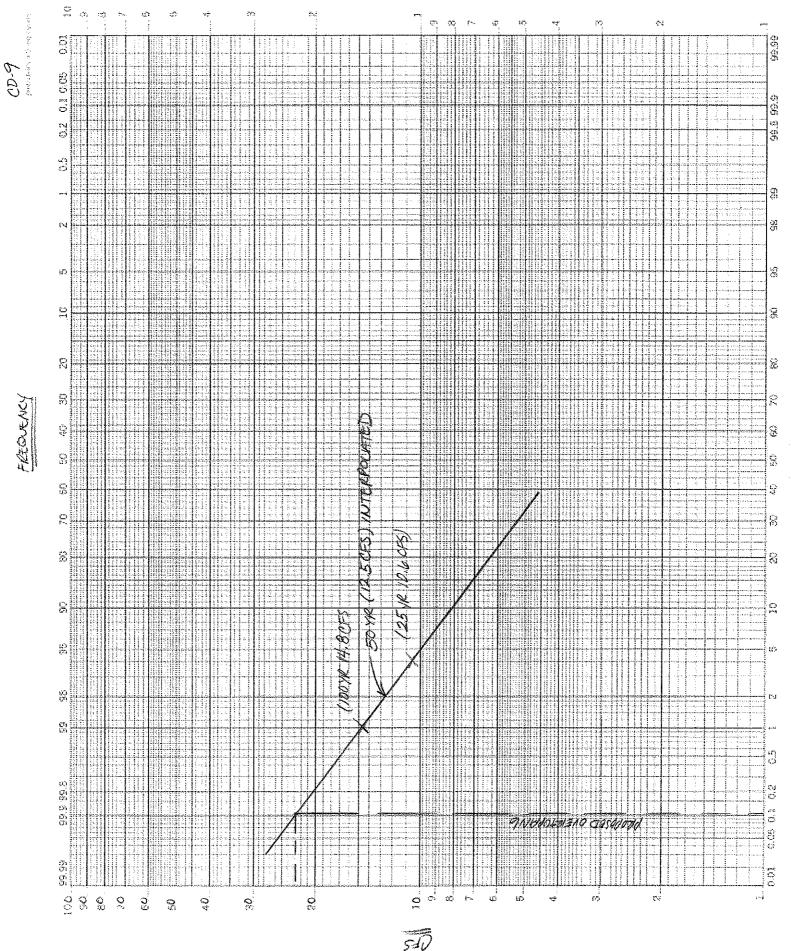
| | Overtopping |] |
|-------------|-------------|----------|
| | Existing | Proposed |
| Elev (NAVD) | 62 | 62.00 |
| Q* (cfs) | 12.64 | 22.68 |
| Freq (yr) | 50 | >500 |

* From HY 8 culvert analysis

I:\Projects\12722145 SR46 PDE\drainage\Cross Droins\CD-9\CD-9





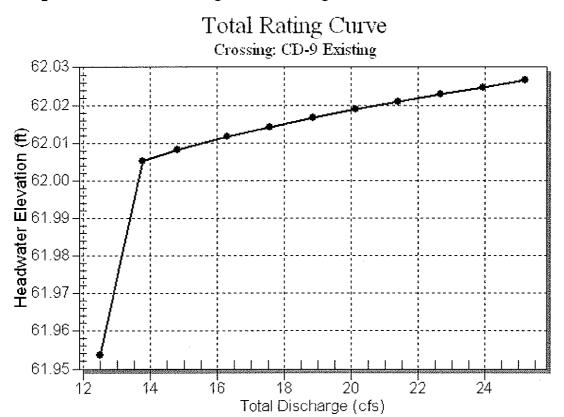


FRENENCY

HY-8 Culvert Analysis Report CD-9 (Existing 18" RCP)

| Headwater Elevation (ft) | Total Discharge (cfs) | CD-9 Existing Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------------------|-----------------------|----------------------------------|----------------------------|------------|
| 61.95 | 12.50 | 12.50 | 0.00 | 1 |
| 62.00 | 13.77 | 12.66 | 0.99 | 21 |
| 62.01 | 14.80 | 12.66 | 2.01 | 4 |
| 62.01 | 16.31 | 12.68 | 3.55 | 4 |
| 62.01 | 17.58 | 12.68 | 4.76 | 3 |
| 62.02 | 18.85 | 12.69 | 6.04 | 3 |
| 62.02 | 20.12 | 12.70 | 7.34 | 3 |
| 62.02 | 21.39 | 12.70 | 8.63 | 3 |
| 62.02 | 22.66 | 12.71 | 9.91 | 3 |
| 62.02 | 23.93 | 12.71 | 10.99 | 2 |
| 62.03 | 25.20 | 12.72 | 12.43 | 3 |

Table 1 - Summary of Culvert Flows at Crossing: CD-9 Existing



Rating Curve Plot for Crossing: CD-9 Existing

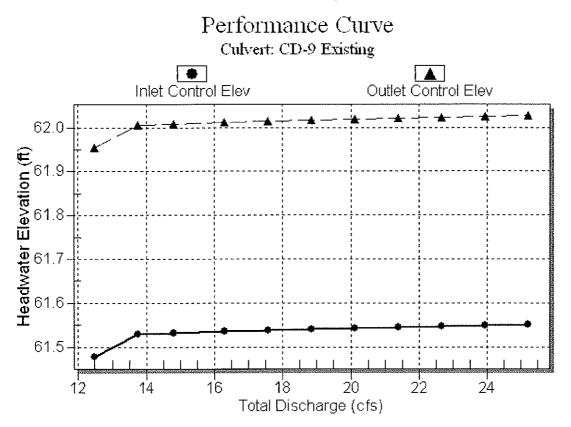
| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Iniet Controi Depth (ft) | Outlet Control Depth (fl) | Flow Type | Normal Depth (fl) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
|-----------------------------|-------------------------------|--------------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|------------------------------|---------------------------------|
| 12.50 | 12.50 | 61.95 | 2.978 | 3.453 | 4-FFf | 1.500 | 1.329 | 1.500 | 1.500 | 7.074 | 0.000 |
| 13.77 | 12.66 | 62,00 | 3.028 | 3.505 | 4-FFf | 1.500 | 1.336 | 1.500 | 1.500 | 7.162 | 0.000 |
| 14.80 | 12.66 | 62.01 | 3.031 | 3.508 | 4-FFf | 1.500 | 1.336 | 1.500 | 1.500 | 7.167 | 0.000 |
| 16,31 | 12.68 | 62.01 | 3.035 | 3.511 | 4-FFf | 1.500 | 1.337 | 1.500 | 1.500 | 7,173 | 0.000 |
| 17.58 | 12.68 | 62.01 | 3.037 | 3.514 | 4-FFf | 1.500 | 1.337 | 1.500 | 1.500 | 7,177 | 0.000 |
| 18.85 | 12.69 | 62.02 | 3.040 | 3.516 | 4-FFf | 1.500 | 1.337 | 1.500 | 1.500 | 7.181 | 0.000 |
| 20.12 | 12.70 | 62.02 | 3.042 | 3.519 | 4-FFf | 1.500 | 1.338 | 1.500 | 1.500 | 7.185 | 0.000 |
| 21.39 | 12.70 | 62.02 | 3.044 | 3.521 | 4-FFf | 1.500 | 1.338 | 1.500 | 1.500 | 7.189 | 0.000 |
| 22.66 | 12.71 | 62.02 | 3.046 | 3.523 | 4-FFf | 1,500 | 1.338 | 1.500 | 1.500 | 7.192 | 0.000 |
| 23.93 | 12.71 | 62.02 | 3.047 | 3.524 | 4-FFf | 1.500 | 1.338 | 1.500 | 1.500 | 7.195 | 0.000 |
| 25.20 | 12.72 | 62.03 | 3.049 | 3.526 | 4-FFf | 1.500 | 1.339 | 1.500 | 1.500 | 7.198 | 0.000 |

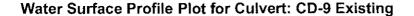
Table 2 - Culvert Summary Table: CD-9 Existing

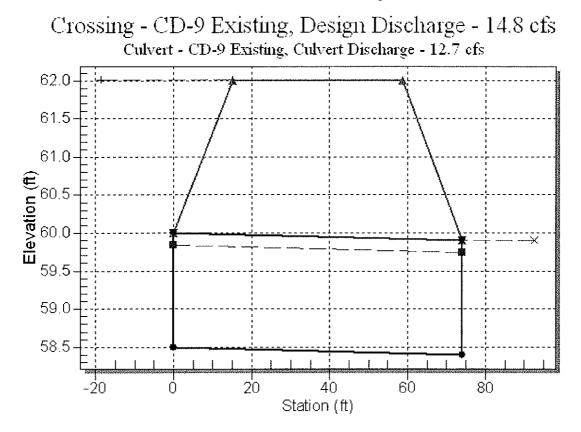
Inlet Elevation (invert): 58.50 ft, Outlet Elevation (invert): 58.40 ft

Culvert Length: 74.00 ft, Culvert Slope: 0.0014

Culvert Performance Curve Plot: CD-9 Existing







Site Data - CD-9 Existing

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 58.50 ft Outlet Station: 74.00 ft Outlet Elevation: 58.40 ft Number of Barrels: 1

Culvert Data Summary - CD-9 Existing

Barrel Shape: Circular Barrel Diameter: 1.50 ft Barrel Material: Concrete Barrel Manning's n: 0.0120 Inlet Type: Conventional Inlet Edge Condition: Square Edge with Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-9 Existing)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
|------------|-------------------------|------------|
| 12.50 | 59.90 | 1.50 |
| 13.77 | 59.90 | 1.50 |
| 14.80 | 59.90 | 1.50 |
| 16.31 | 59.90 | 1.50 |
| 17.58 | 59.90 | 1.50 |
| 18.85 | 59.90 | 1.50 |
| 20.12 | 59.90 | 1.50 |
| 21.39 | 59.90 | 1.50 |
| 22.66 | 59.90 | 1.50 |
| 23.93 | 59.90 | 1.50 |
| 25.20 | 59.90 | 1.50 |

Tailwater Channel Data - CD-9 Existing

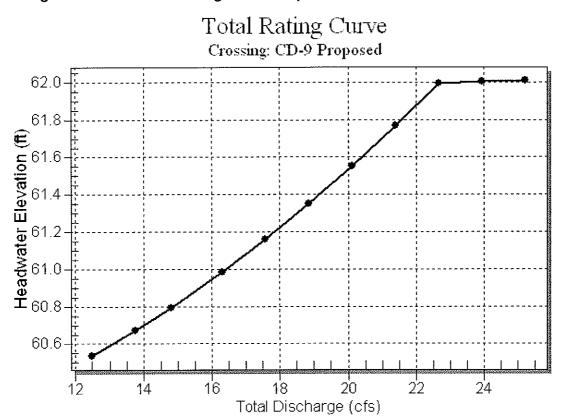
Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 59.90 ft

Roadway Data for Crossing: CD-9 Existing

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 1000.00 ft Crest Elevation: 62.00 ft Roadway Surface: Paved Roadway Top Width: 43.40 ft HY-8 Culvert Analysis Report CD-9 (Proposed 24" RCP)

| Headwater Elevation (ft) | Total Discharge (cfs) | CD-9 Proposed Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------------------|-----------------------|----------------------------------|----------------------------|------------|
| 60.54 | 12.50 | 12.50 | 0.00 | 1 |
| 60.67 | 13.77 | 13.77 | 0.00 | 1 |
| 60.79 | 14.80 | 14.80 | 0.00 | 1 |
| 60.99 | 16.31 | 16.31 | 0.00 | 1 |
| 61.16 | 17.58 | 17.58 | 0.00 | 1 |
| 61.35 | 18.85 | 18.85 | 0.00 | 1 |
| 61.55 | 20.12 | 20.12 | 0.00 | 1 |
| 61.77 | 21.39 | 21.39 | 0.00 | 1 |
| 62.00 | 22.66 | 22.66 | 0.00 | 1 |
| 62.01 | 23.93 | 22.71 | 1.06 | 7 |
| 62.01 | 25.20 | 22.73 | 2.34 | 4 |

Table 1 - Summary of Culvert Flows at Crossing: CD-9 Proposed



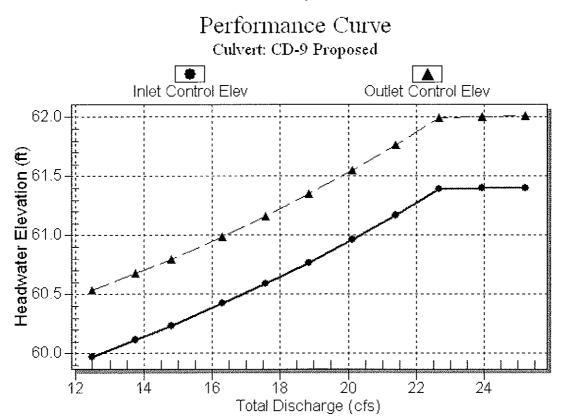
Rating Curve Plot for Crossing: CD-9 Proposed

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
|-----------------------------|-------------------------------|--------------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|------------------------------|---------------------------------|
| 12,50 | 12.50 | 60.54 | 1.973 | 2.538 | 4-FFf | 2.000 | 1.267 | 2.000 | 2.000 | 3.979 | 0.000 |
| 13.77 | 13.77 | 60.67 | 2.115 | 2.674 | 4-FFf | 2.000 | 1.332 | 2.000 | 2.000 | 4.383 | 0.000 |
| 14.80 | 14.80 | 60.79 | 2.234 | 2.794 | 4-FFf | 2.000 | 1.385 | 2.000 | 2.000 | 4.711 | 0.000 |
| 16.31 | 16.31 | 60.99 | 2.420 | 2.986 | 4-FFf | 2.000 | 1.451 | 2.000 | 2.000 | 5.192 | 0.000 |
| 17.58 | 17.58 | 61.16 | 2.588 | 3.161 | 4-FFf | 2.000 | 1.505 | 2.000 | 2.000 | 5.596 | 0.000 |
| 18.85 | 18.85 | 61.35 | 2.768 | 3.350 | 4-FFf | 2.000 | 1.558 | 2.000 | 2.000 | 6.000 | 0.000 |
| 20.12 | 20.12 | 61.55 | 2.961 | 3.552 | 4-FFf | 2.000 | 1.608 | 2.000 | 2.000 | 6.404 | 0.000 |
| 21.39 | 21.39 | 61.77 | 3.169 | 3.768 | 4-FFf | 2.000 | 1.646 | 2,000 | 2.000 | 6,809 | 0.000 |
| 22.66 | 22.66 | 62.00 | 3.390 | 3.996 | 4-FFf | 2.000 | 1.683 | 2.000 | 2.000 | 7.213 | 0.000 |
| 23.93 | 22.71 | 62.01 | 3.399 | 4.005 | 4-FFf | 2.000 | 1.685 | 2.000 | 2.000 | 7.228 | 0.000 |
| 25.20 | 22.73 | 62.01 | 3.402 | 4.008 | 4-FFf | 2.000 | 1.685 | 2.000 | 2.000 | 7,234 | 0.000 |

Table 2 - Culvert Summary Table: CD-9 Proposed

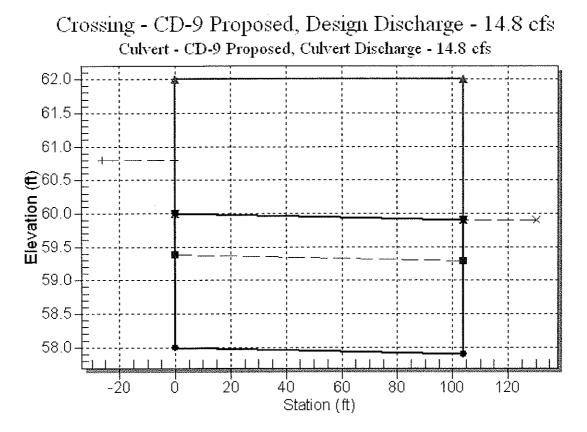
Inlet Elevation (invert): 58.00 ft, Outlet Elevation (invert): 57.90 ft

Culvert Length: 104.00 ft, Culvert Slope: 0.0010



Culvert Performance Curve Plot: CD-9 Proposed





Site Data - CD-9 Proposed

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 58.00 ft Outlet Station: 104.00 ft Outlet Elevation: 57.90 ft Number of Barrels: 1

Culvert Data Summary - CD-9 Proposed

Barrel Shape: Circular Barrel Diameter: 2.00 ft Barrel Material: Concrete Barrel Manning's n: 0.0120 Inlet Type: Conventional Inlet Edge Condition: Square Edge with Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-9 Proposed)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
|------------|-------------------------|------------|
| 12.50 | 59.90 | 2.00 |
| 13.77 | 59.90 | 2.00 |
| 14.80 | 59.90 | 2.00 |
| 16.31 | 59.90 | 2.00 |
| 17.58 | 59.90 | 2.00 |
| 18.85 | 59.90 | 2.00 |
| 20.12 | 59.90 | 2.00 |
| 21.39 | 59.90 | 2.00 |
| 22.66 | 59.90 | 2.00 |
| 23.93 | 59.90 | 2.00 |
| 25.20 | 59.90 | 2.00 |

Tailwater Channel Data - CD-9 Proposed

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 59.90 ft

Roadway Data for Crossing: CD-9 Proposed

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 1000.00 ft Crest Elevation: 62.00 ft Roadway Surface: Paved Roadway Top Width: 104.00 ft

APPENDIX E 100-Year Floodplain Analysis

SR 46 PD&E LOCATION HYDRAULICS REPORT

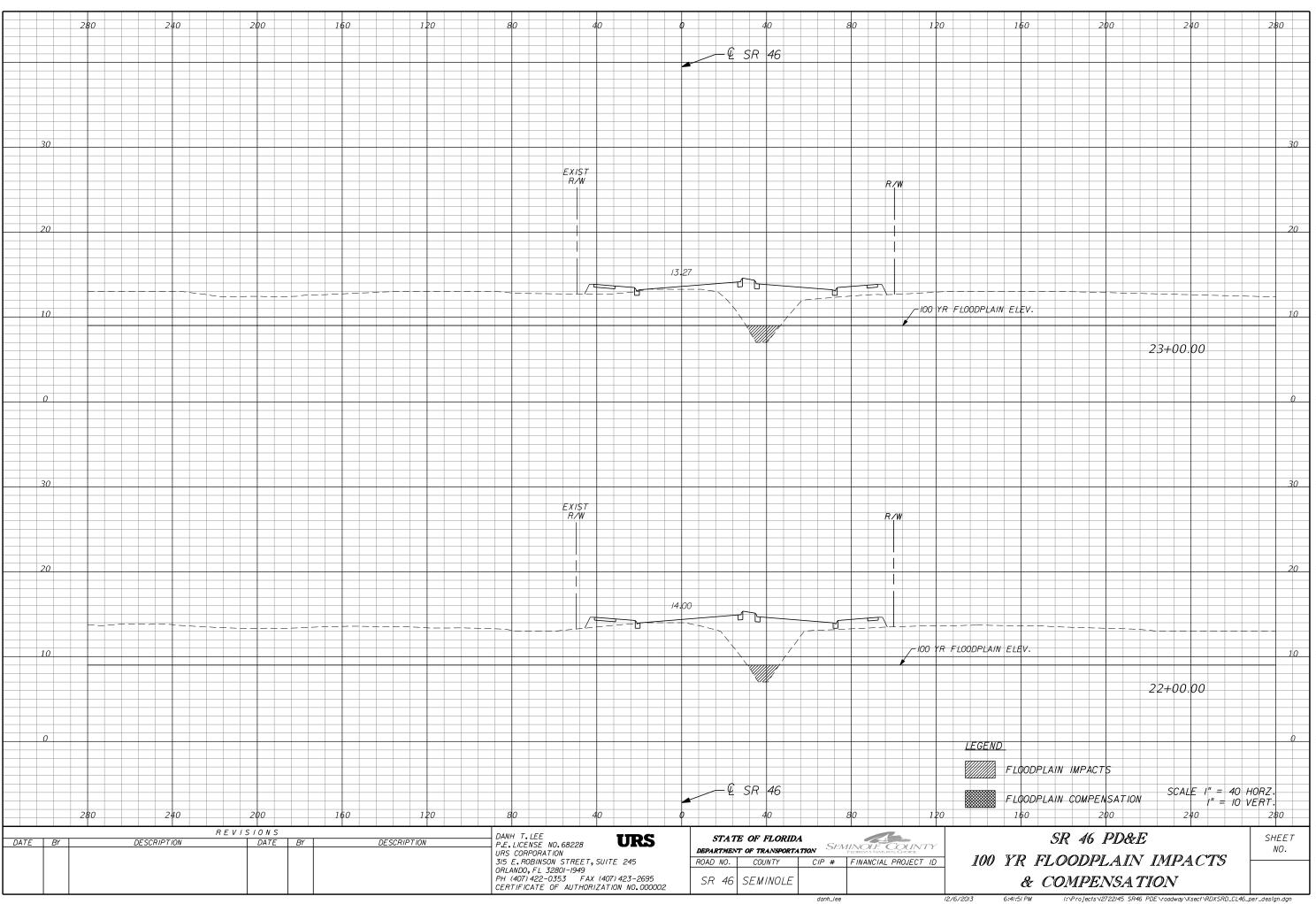
| URS | | | | | |
|----------------|--------------------|-----------------------------|----------|-----------|--|
| MADE BY: | DTL | DATE: | 11/26/13 | JOB NO. | |
| CHECKED BY: | DEP | DATE: | 12/19/13 | SHEET NO. | |
| CALCULATIONS F | OR SR 46 PD&F Floo | dplain Impacts/Compensation | | | |

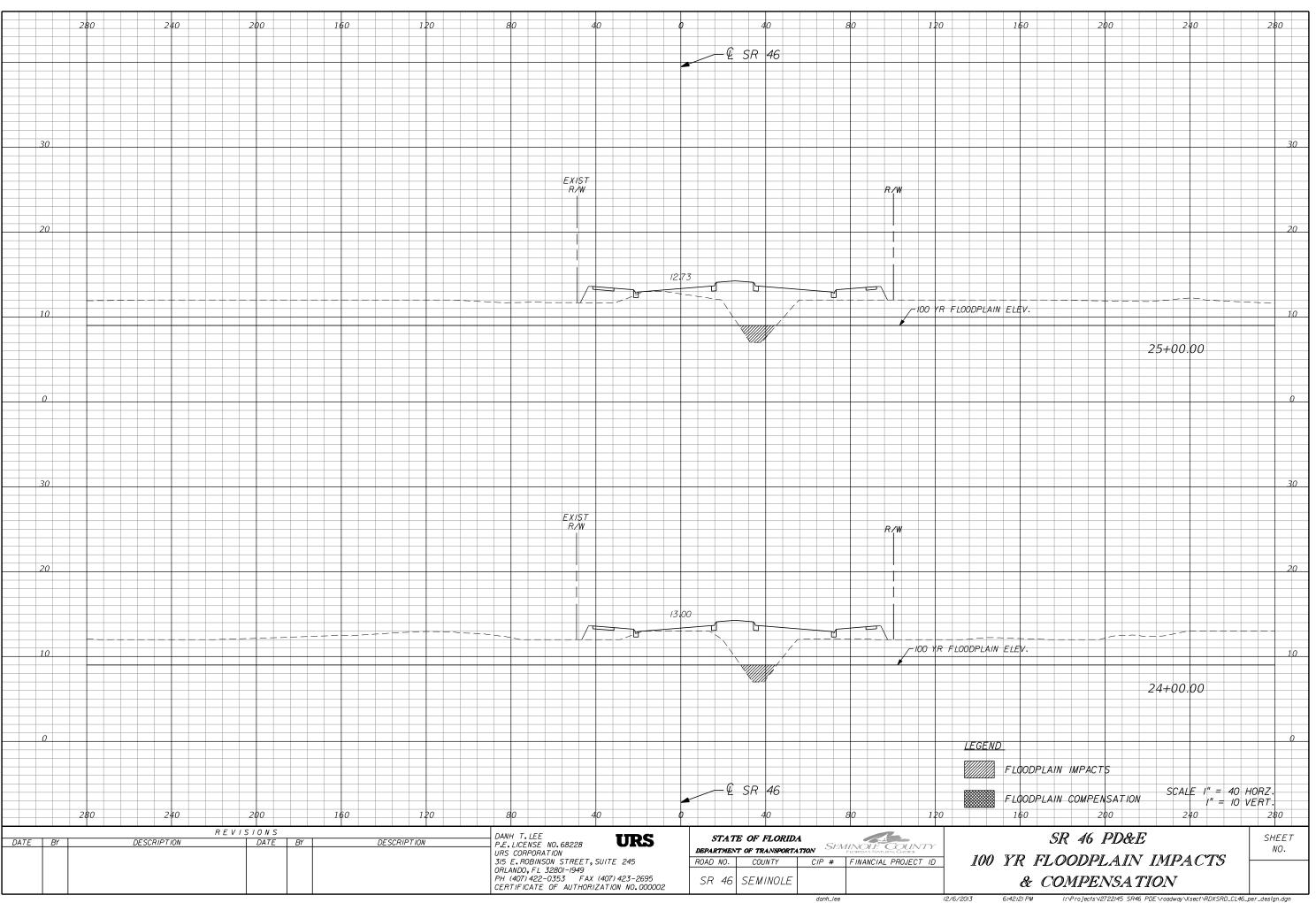
| Roadway Cross-Section | Impact (Fill) | Floodplain Compensation (Cut) Area (ft ²): | Floodplain Impact Net Area (ft ²): | Floodplain Impact Net Volume (ft ³): | Floodplain Impact Net Volume (ac-ft) |
|--------------------------|--------------------------|---|---|---|---|
| Station: | Area (ft ²): | | | | |
| | and the family shade of | Center Line for S | R 46 Widening | | |
| 22+00 | 19.23 | 0.00 | 19.23 | | |
| 23+00 | 21.32 | 0.00 | 21.32 | 2,027.25 | 0.05 |
| 24+00 | 22.42 | 0.00 | 22.42 | 2,186.75 | 0.05 |
| 25+00 | 22.91 | 0.00 | 22.91 | 2,266.13 | 0.05 |
| 26+00 | 0.00 | 0.00 | 0.00 | 1,145.25 | 0.03 |
| 27+00 | 33.08 + | 0.00 | 33.08 | 1,654.13 | 0.04 |
| 28+00 | 12.46 | 0.00 | 12.46 | 2,277.25 | 0.05 |
| 29+00 | 37.32 | 0.00 | 37.32 | 2,488.88 | 0.06 |
| 30+00 | 30.83 | 0.00 | 30.83 | 3,407.00 | 0.08 |
| 31+00 | 2.28 . | 0.00 | 2.28 | 1,655.13 | 0.04 |
| 32+00 | 59.09 | 0.00 | 59.09 | 3,068.38 | 0.07 |
| 33+00 | 147.05 | 0.00 | 147.05 | 10,307.13 | 0.24 |
| 34+00 | 94.61 | 0.00 | 94.61 | 12,083.25 | 0.28 |
| 35+00 | 218.45 | 0.00 | 218.45 | 15,653.13 | 0.36 |
| 36+00 | 297.11 | 0.00 | 297.11 | 25,778.00 | 0.59 |
| 37+00 | 175.48 | 0.00 | 175.48 | 23,629.50 | 0.54 |
| 38+00 | 274.54 | 0.00 | 274.54 | 22,500.75 | 0.52 |
| 39+00 | 278.36 | 0.00 | 278.36 | 27,644.50 | 0.63 |
| 40+00 | 275.50 - | 0.00 | 275.50 | 27,692.88 | 0.64 |
| 41+00 | 285.98 | 0.00 | 285.98 | 28,074.00 | 0.64 |
| 42+00 | 290.02 | 0.00 | 290.02 | 28,799.63 | 0.66 |
| 43+00 | 288.26 - | 0.00 | 288.26 | 28,913.88 | 0.66 |
| 44+00 | 291.59 | 0.00 | 291.59 | 28,992.50 | 0.67 |
| 45+00 | 328.28 | 0.00 | 328.28 | 30,993.25 | 0.71 |
| 46+00 | 296.62 | 0.00 | 296.62 | 31,244.63 | 0.72 |
| 47+00 | 300.84 | 0.00 | 300.84 | 29,872.75 | 0.69 |
| 48+00 | 272.93 - | 0.00 | 272.93 | 28,688.50 | 0.66 |
| 49+00 | 264.38 . | 0.00 | 264.38 | 26,865.50 | 0.62 |
| 50+00 | 282.57 | 0.00 | 282.57 | 27,347.38 | 0.63 |
| 51+00 | 252.87 | 0.00 | 252.87 | 26,771.63 | 0.61 |
| 52+00 | 258.46 - | 0.00 | 258.46 | 25,566.00 | 0.59 |
| 53+00 | 279.72 | 0.00 | 279.72 | 26,908.75 | 0.62 |
| 54+00 | 272.62 | 0.00 | 272.62 | 27,617.13 | 0.63 |
| 55+00 | 259.04 | 0.00 | 259.04 | 26,583.00 | 0.61 |
| 56+00 | 253.56 . | 0.00 | 253.56 | 25,629.75 | 0.59 |
| 57+00 | 251.34 | 0.00 | 251.34 | 25,244.63 | 0.58 |
| 58+00 | 234.30 - | 0,00 | 234.30 | 24,281.75 | 0.56 |
| 59+00 | 225.72 | 0.00 | 225.72 | 23,001.00 | 0.53 |
| 60+00 | 209.29 | 0.00 | 209.29 | 21,750.38 | 0.50 |
| 61+00 | 206.01 | 0.00 | 206.01 | 20,765.00 | 0.48 |
| 62+00 | 206.06 | 0.00 | 206.06 | 20,603.38 | 0.47 |
| 63+00 | 212.62 ' | 0.00 | 212.62 | 20,933.75 | 0.48 |
| 64+00 | 210.14 | 0.00 | 210.14 | 21,137.88 | 0.49 |
| 65+00 | 213.30 - | 0.00 | 213.30 | 21,171.75 | 0.49 |
| 66+00 | 190.69 | 0.00 | 190.69 | 20,199.13 | 0.46 |
| 67+00 | 199.30 | 0.00 | 199.30 | 19,499.25 | 0.45 |
| 68+00 | 206.36 | 0.00 | 206.36 | 20,282.88 | 0.47 |
| 69+00 | 189.59 | 0.00 | 189.59 | 19,797.38 | 0.45 |
| 70+00 | 180.60 | 0.00 | 180.60 | 18,509.63 | 0.42 |
| 71+00 | 215.75 | 0.00 | 215.75 | 19,817.63 | 0.45 |
| 72+00 | 207.11 | 0.00 | 207.11 | 21,142.88 | 0.49 |
| 73+00 | 204.30 | 0.00 | 204.30 | 20,570.25 | 0.47 |
| 74+00 | 196.96 | 0.00 | 196.96 | 20,063.00 | 0.46 |
| 75+00 | 176.25 | 0.00 | 176.25 | 18,660.38 | 0.43 |
| 76+00 | 140.45 | 0.00 | 140.45 | 15,834.50 | 0.36 |
| 77+00 | 221.73 · | 0.00 | 221.73 | 18,108.75 | 0.42 |
| 78+00 | 218.82 | 0.00 | 218.82 | 22,027.38 | 0.51 |
| 79+00 | 97.88 | 0.00 | 97.88 | 15,835.00 | 0.36 |
| 80+00 | 91.45 | 0.00 | 91.45 | 9,466.75 | 0.22 |
| 81+00 | 78.67 * | 0.00 | 78.67 | 8,506.00 | 0.20 |
| 82+00 | 72.47 | 0.00 | 72.47 | 7,556.63 | 0.17 |
| 83+00 | 82.02 | 0.00 | 82.02 | 7,724.13 | 0.18 |

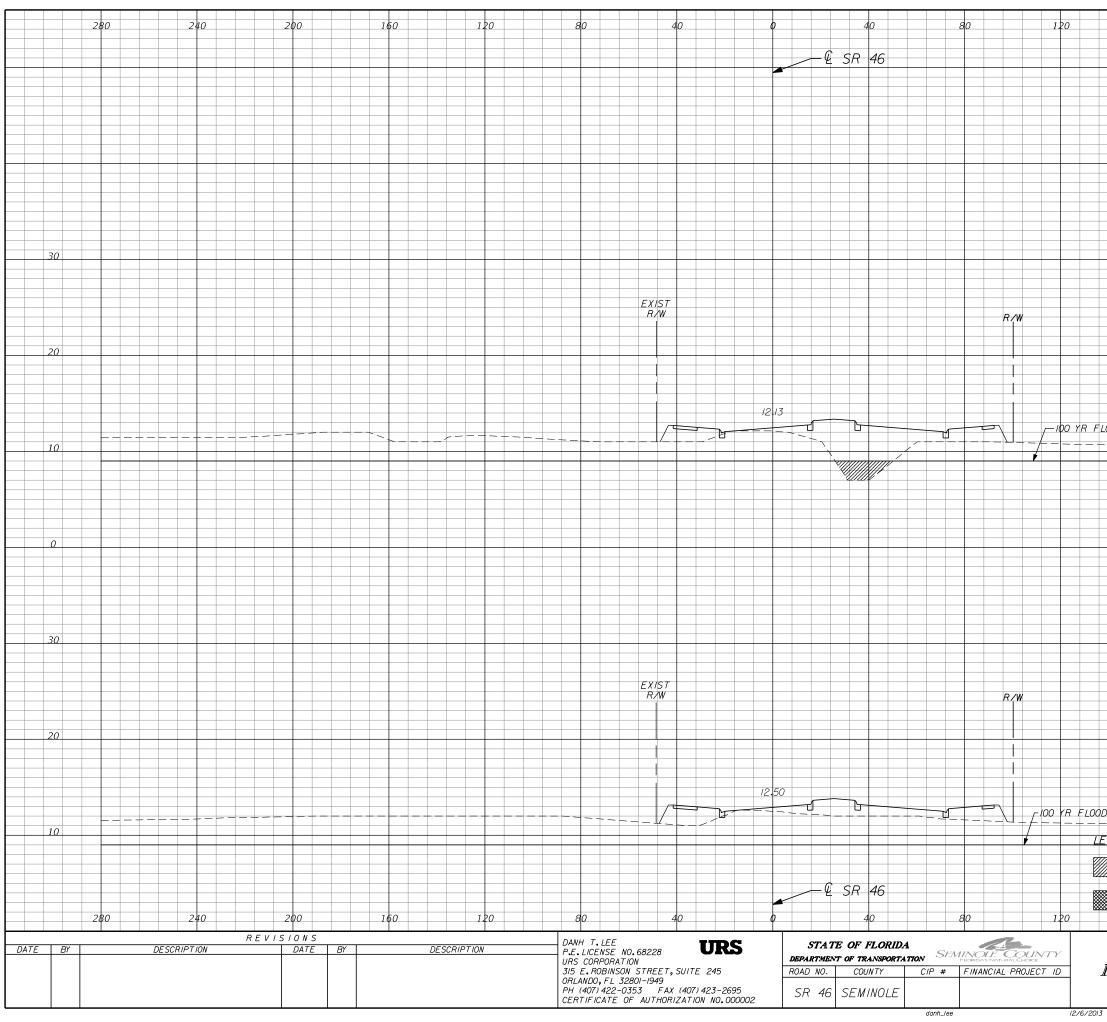
| URS MADE BY: CHECKED BY: CALCULATIONS FOR | DTL DCP SR 46 PD&E Floodpla | DATE: DATE: in Impacts/Compensation | 11/26/13 12/19/13 | JOB NO. SHEET NO. | |
|--|-----------------------------------|---|------------------------------|--------------------------------|--------------------|
| Roadway | Floodplain | Floodplain Compensation | Floodplain Impact | Floodplain Impact | Floodplain Impact |
| Cross-Section | Impact (Fill) | (Cut) Area (ft ²): | Net Area (ft ²): | Net Volume (ft ³): | Net Volume (ac-ft) |

| 84+00 | 56.11 | 0.00 | 56.11 | 6,906.25 | 0.16 |
|---------------|--------------------------|----------------|--------|--------------|-------|
| 85+00 | 86.93 | 0.00 | 86.93 | 7,151.75 | 0.16 |
| 86+00 | 87.51 | 0.00 | 87.51 | 8,722.00 | 0.20 |
| 87+00 | 87.24 | 0.00 | 87.24 | 8,737.63 | 0.20 |
| 88+00 | 84.60 | 0.00 | 84.60 | 8,592.00 | 0.20 |
| 89+00 | 98.80 | 0.00 | 98.80 | 9,170.13 | 0.21 |
| 90+00 | 104.68 | 0.00 | 104.68 | 10,174.25 | 0.23 |
| 91+00 | 76.38 | 0.00 | 76.38 | 9,053.13 | 0.21 |
| 92+00 | 12.27 | 0.00 | 12.27 | 4,432.25 | 0.10 |
| 93+00 | 6.16 | 0.00 | 6.16 | 921.38 | 0.02 |
| 94+00 | 48.91 | 0.00 | 48.91 | 2,753.75 | 0.06 |
| 95+00 | 35.95 | 0.00 | 35.95 | 4,243.00 | 0.10 |
| 96+00 | 30.04 | 0.00 | 30.04 | 3,299.25 | 0.08 |
| 97+00 | 33.83 | 0.00 | 33.83 | 3,193.13 | 0.07 |
| 98+00 | 31.30 | 0.00 | 31.30 | 3,256.13 | 0.07 |
| 99+00 | 33.13 | 0.00 | 33.13 | 3,221.25 | 0.07 |
| 100+00 | 33.37 | 0.00 | 33.37 | 3,324.75 | 0.08 |
| 101+00 | 35.75 | 0.00 | 35.75 | 3,455.88 | 0.08 |
| 102+00 | 32.34 | 0.00 | 32.34 | 3,404.50 | 0.08 |
| Centerline SR | 46 Widening - Station 2 | 2+00 to 102+00 | TOTAL: | 1,242,836.88 | 28.53 |
| 140+00 | 64.10 | 0.00 | 64.10 | | |
| 141+00 | 68.48 | 0.00 | 68.48 | 6,628.50 | 0.15 |
| 142+00 | 62.30 | 0.00 | 62.30 | 6,538.50 | 0.15 |
| 143+00 | 23.00 | 0.00 | 23.00 | 4,264.50 | 0.10 |
| 144+00 | 48.94 | 0.00 | 48.94 | 3,596.63 | 0.08 |
| 145+00 | 15.14 | 0.00 | 15.14 | 3,203.88 | 0.07 |
| 146+00 | 20.15 | 0.00 | 20.15 | 1,764.63 | 0.04 |
| 147+00 | 4.83 | 0.00 | 4.83 | 1,249.13 | 0.03 |
| 148+00 | 8.74 | 0.00 | 8.74 | 678.38 | 0.02 |
| 0 | 46 Widening - Station 14 | | TOTAL: | 27924.13 | 0.64 |

| | | Floodplain Impact Net Volume (ft ³): | Floodplain Impac Net Volume (ac-fl |
|--|--------|---|---------------------------------------|
| Centerline SR 46 Widening - Station 22+00 to 102+00 | TOTAL: | 1,242,836.88 | 28.53 |
| Centerline SR 46 Widening - Station 140+00 to 148+00 | TOTAL: | 27924.13 | 0.64 |

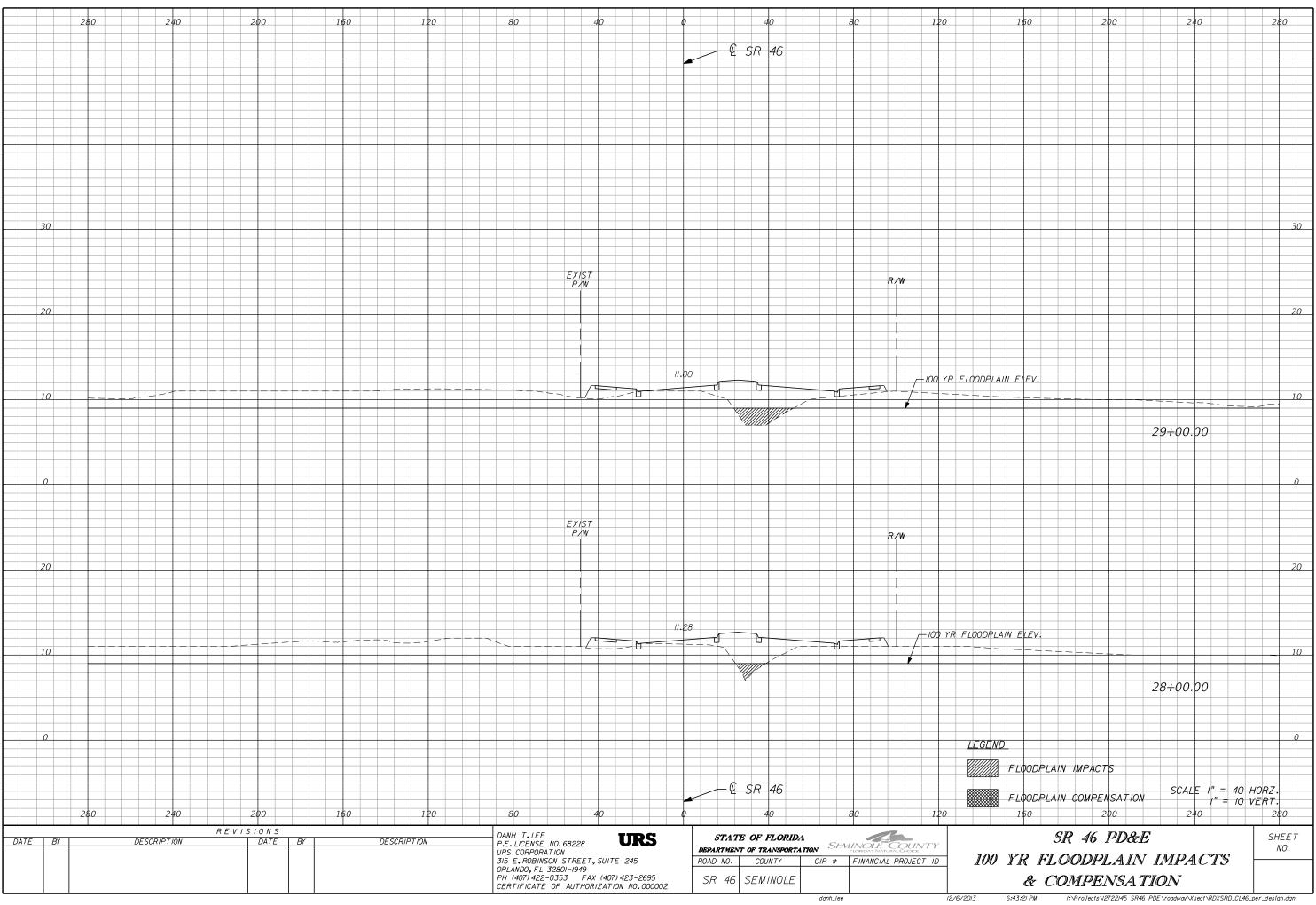


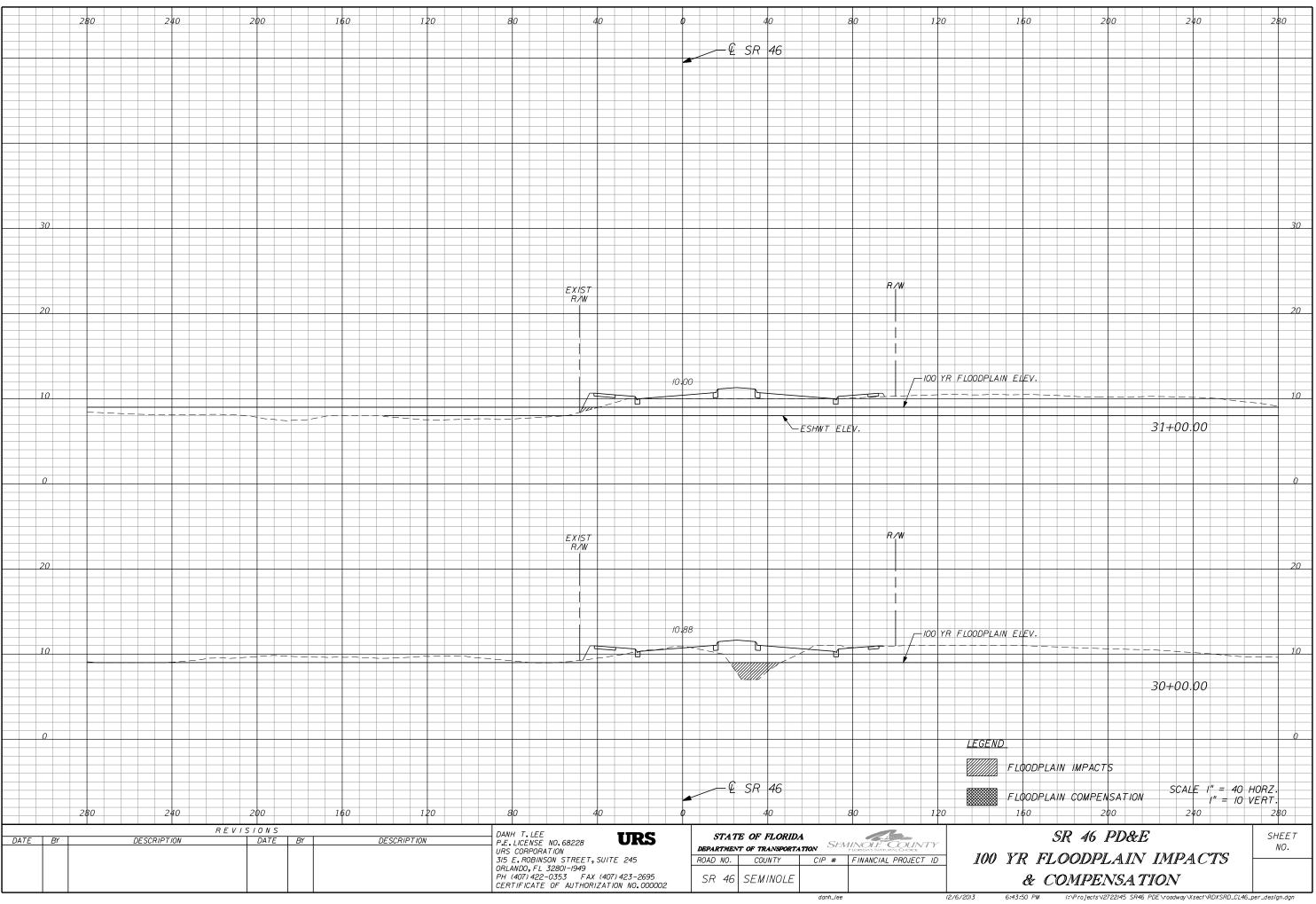


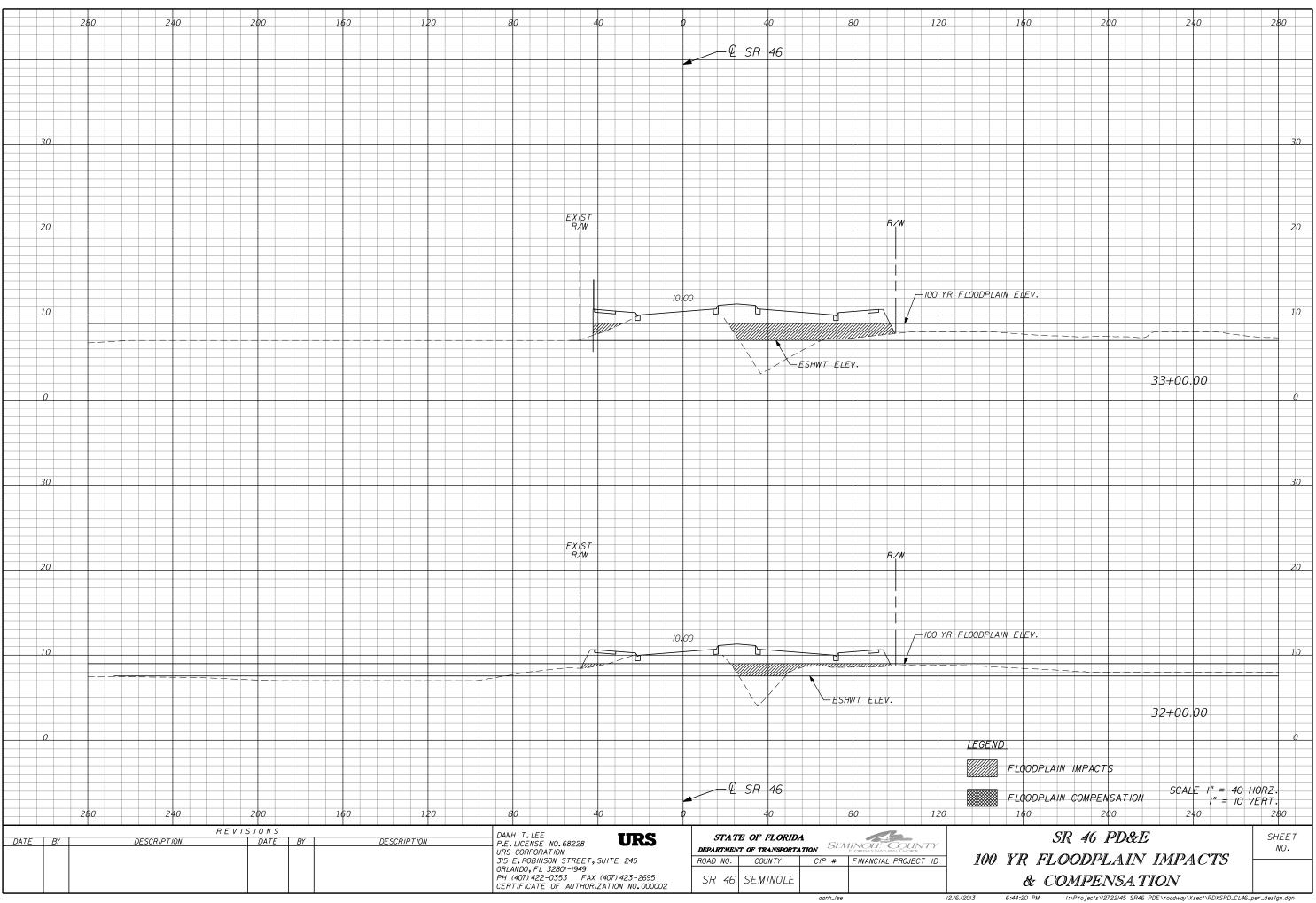


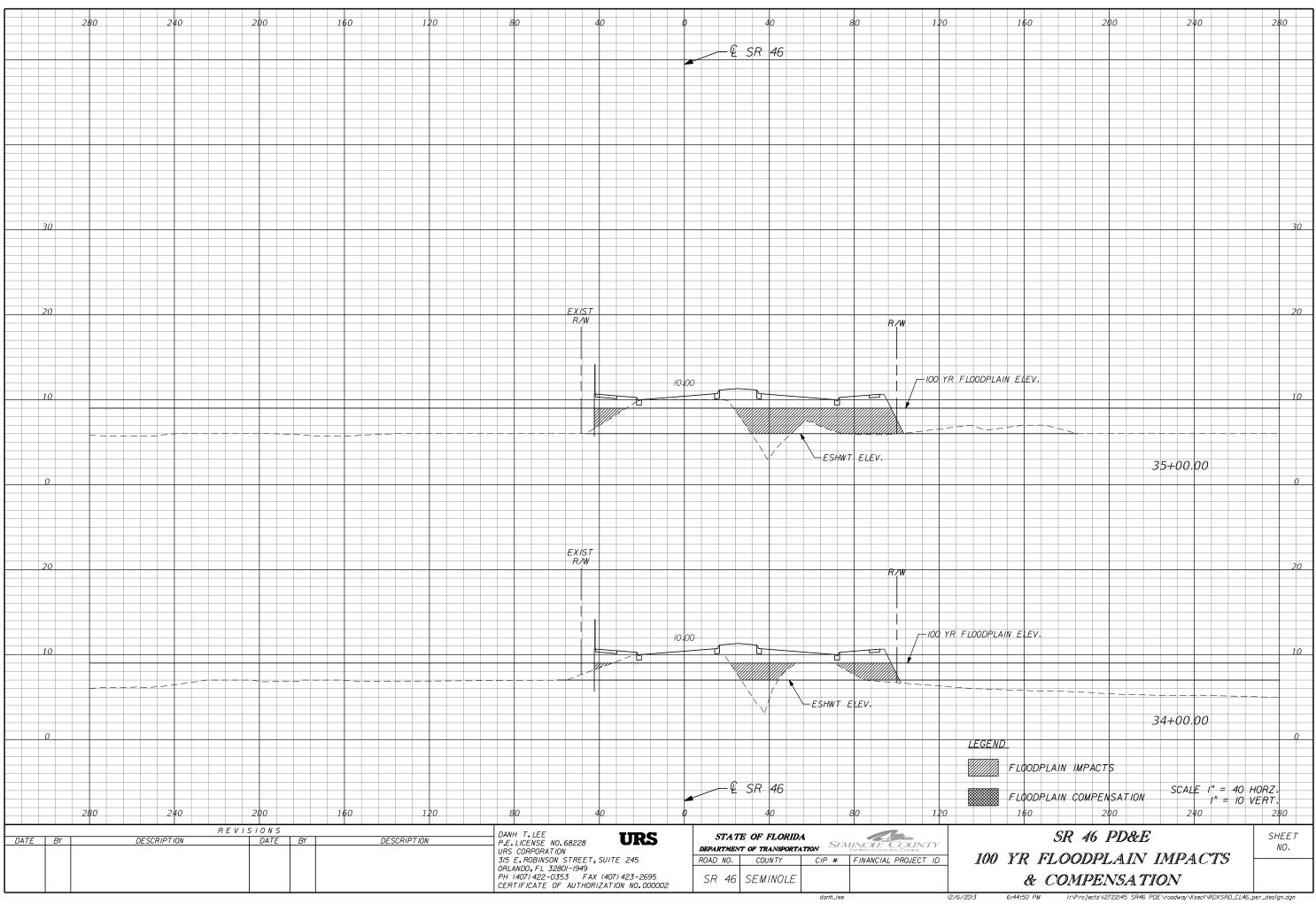
| | 10 | 50 | | | | 21 | 0 | | | | 24 | 40 | | | | 28 | 80 | |
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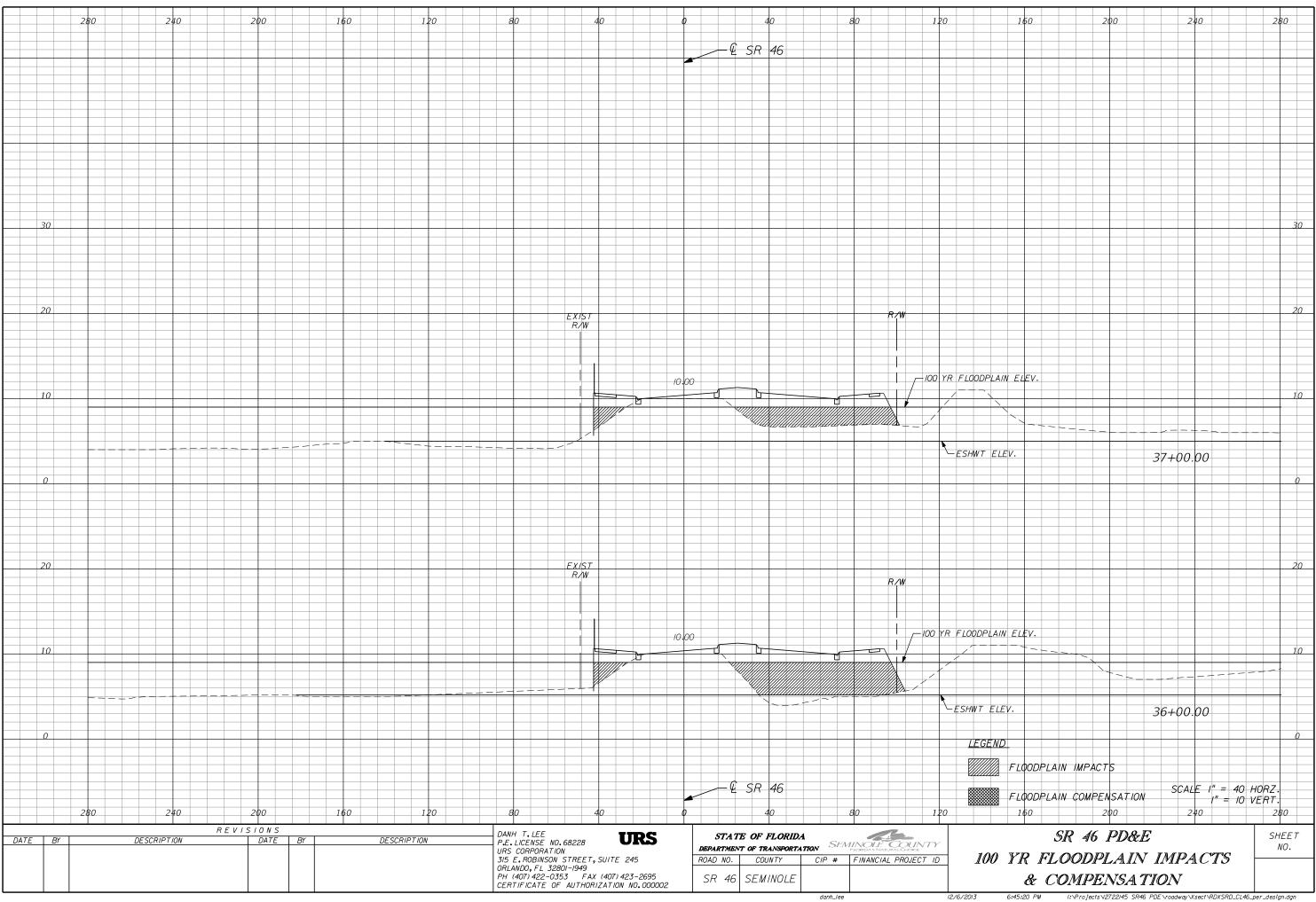
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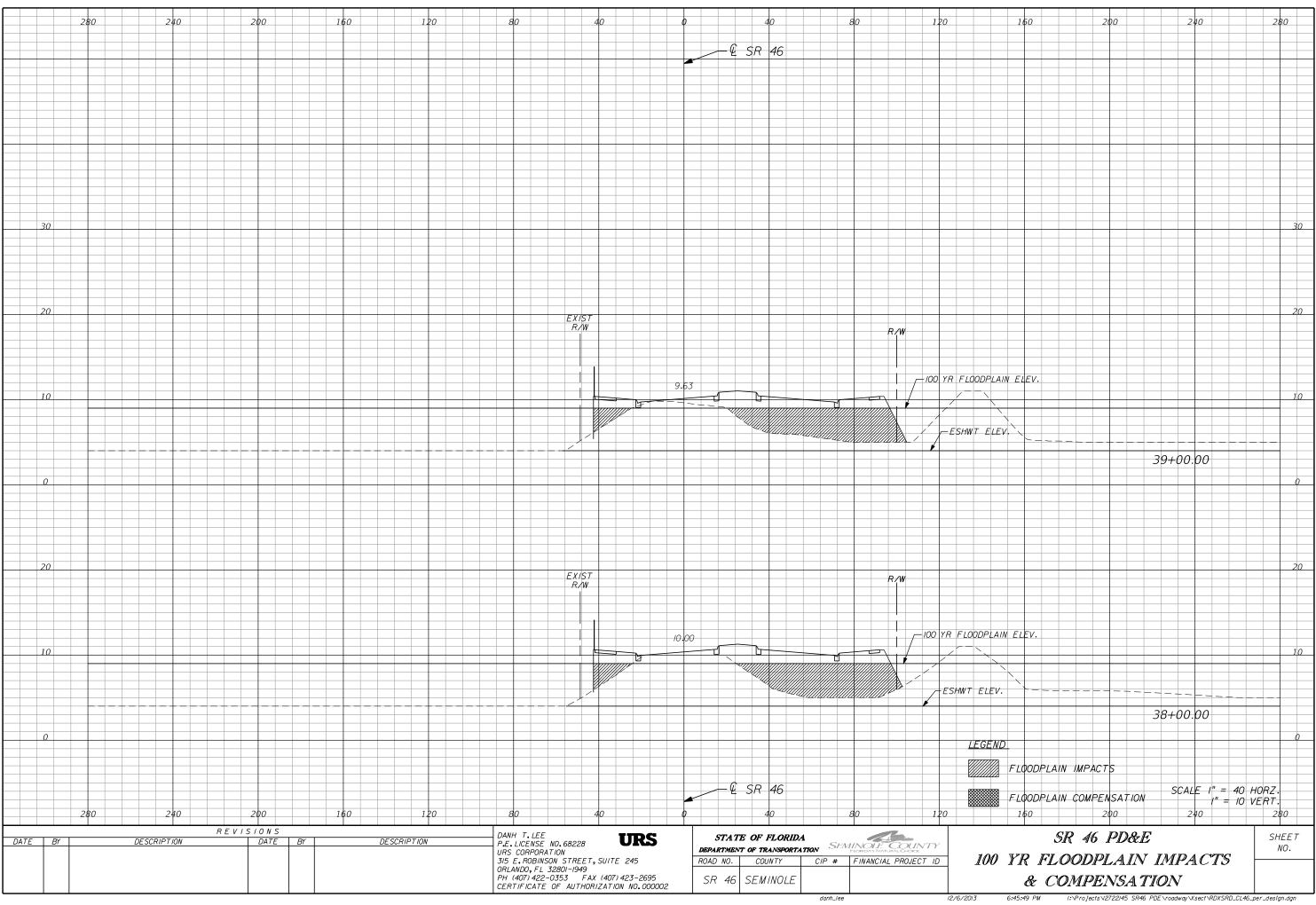


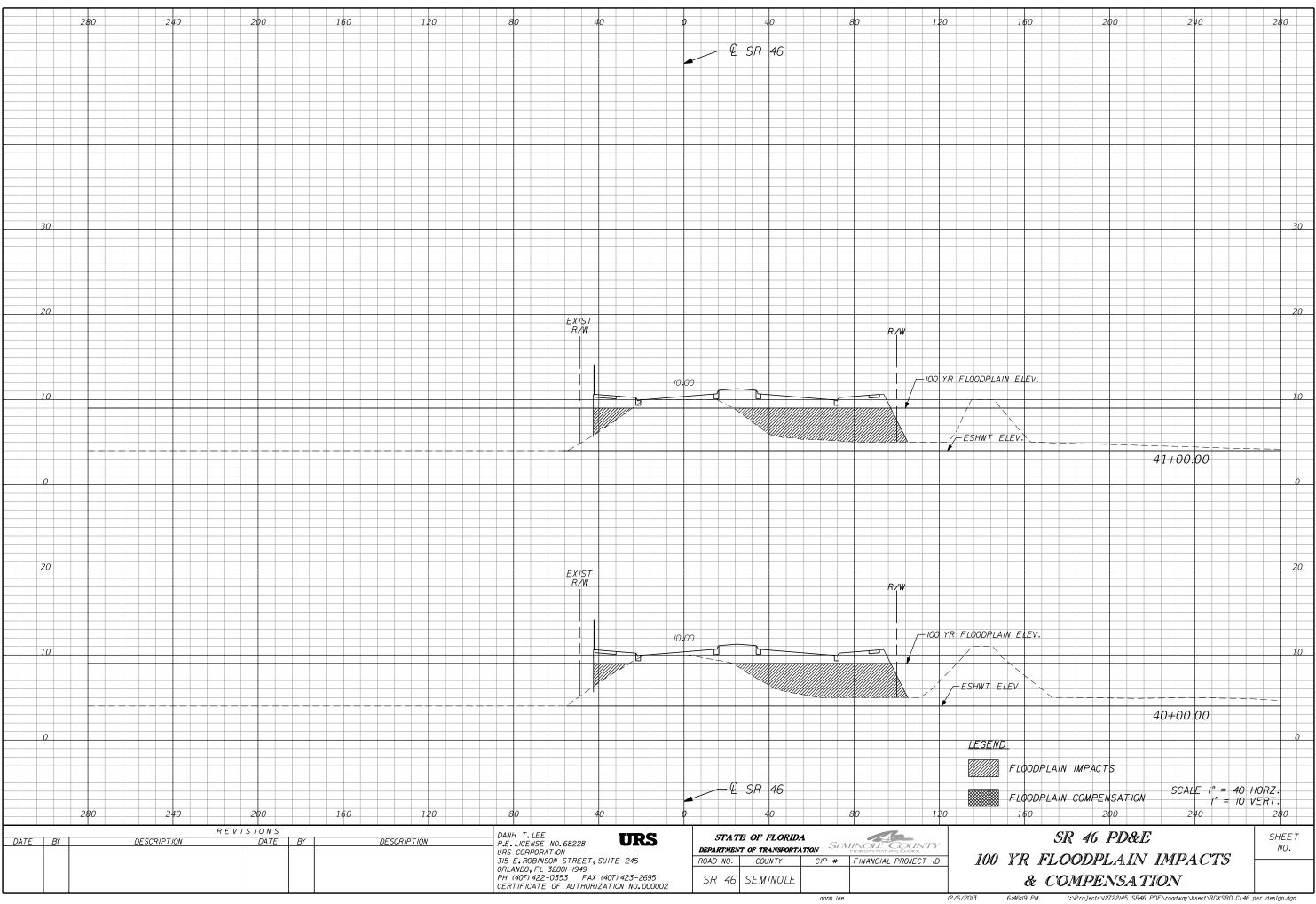


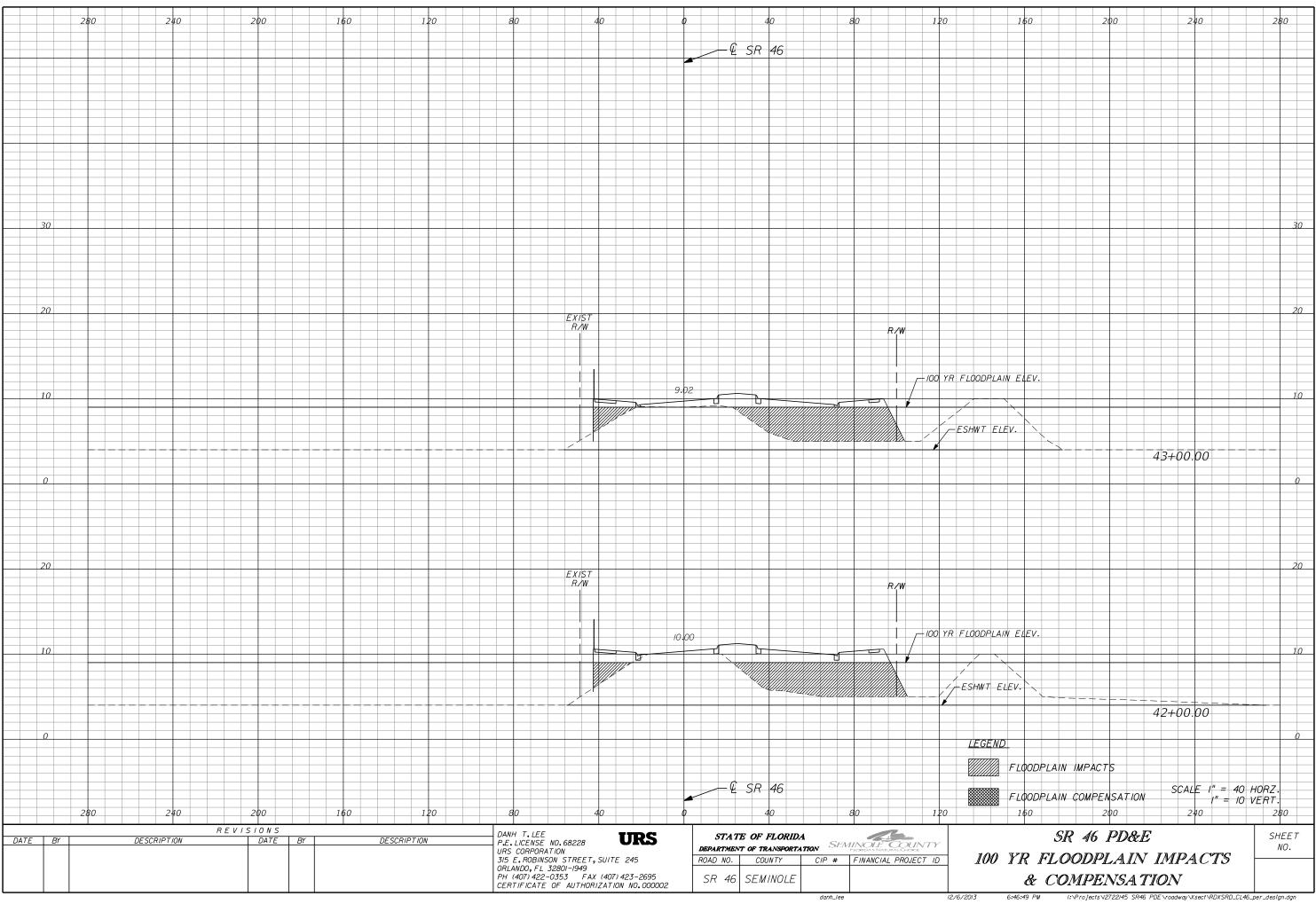


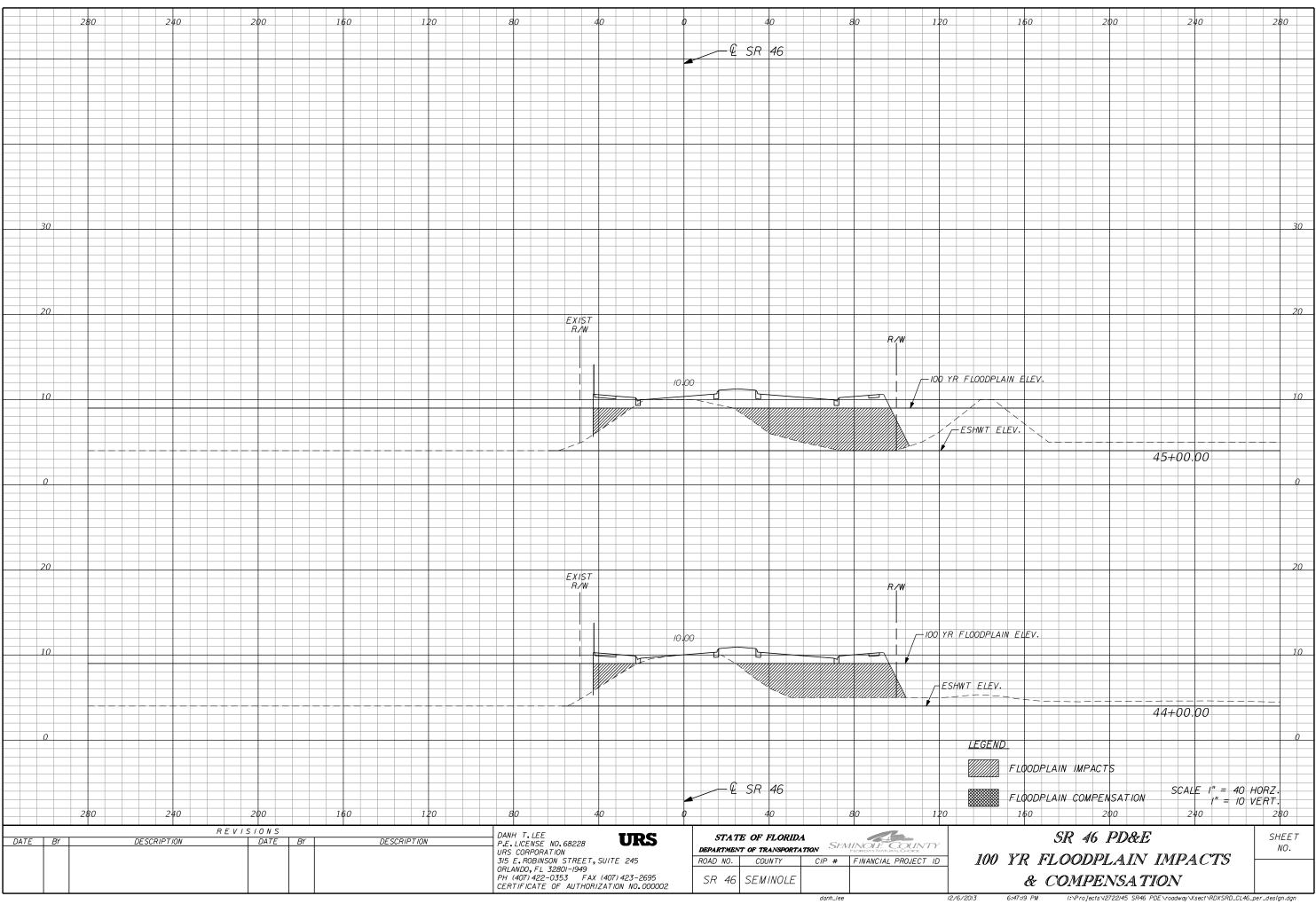


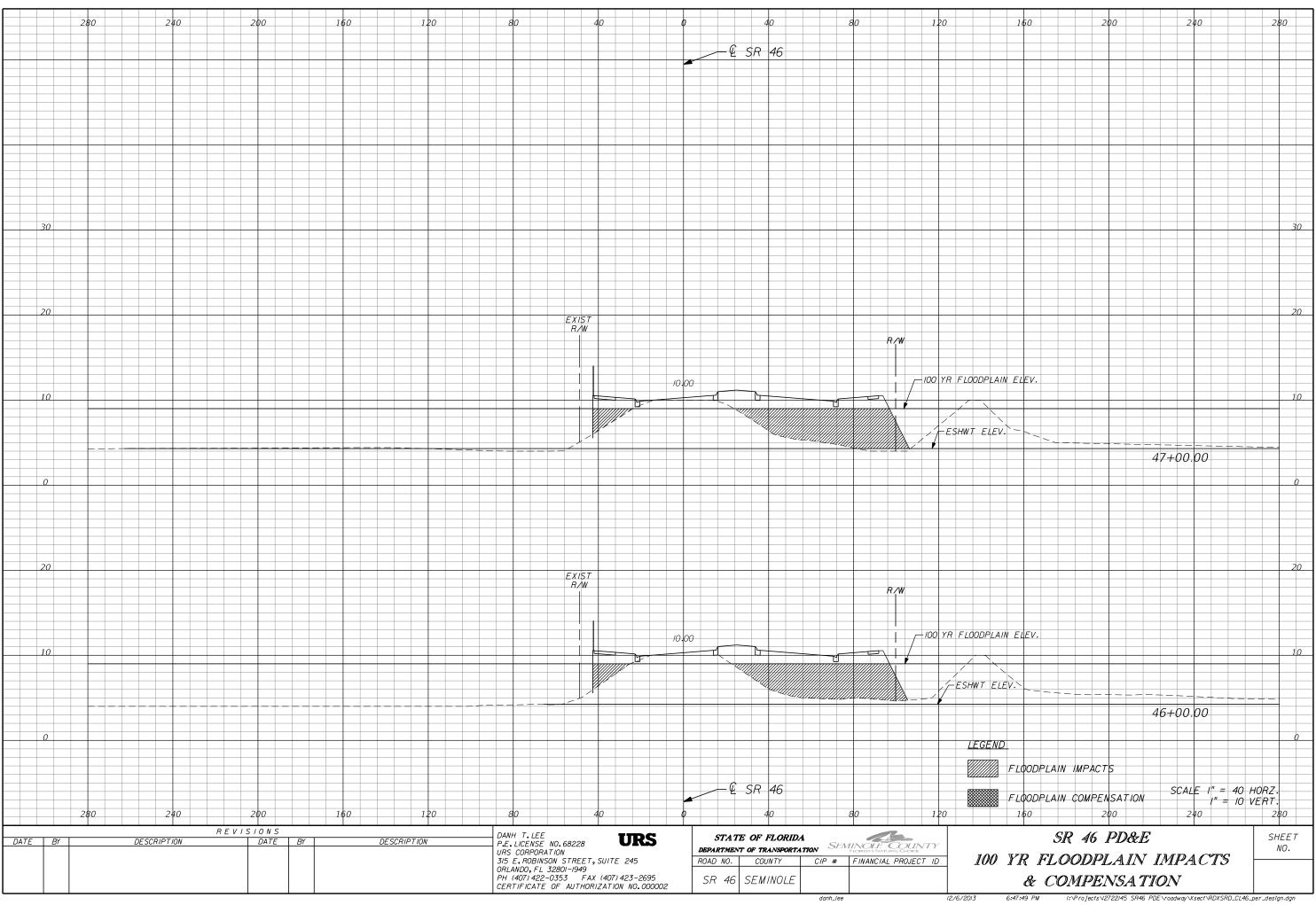


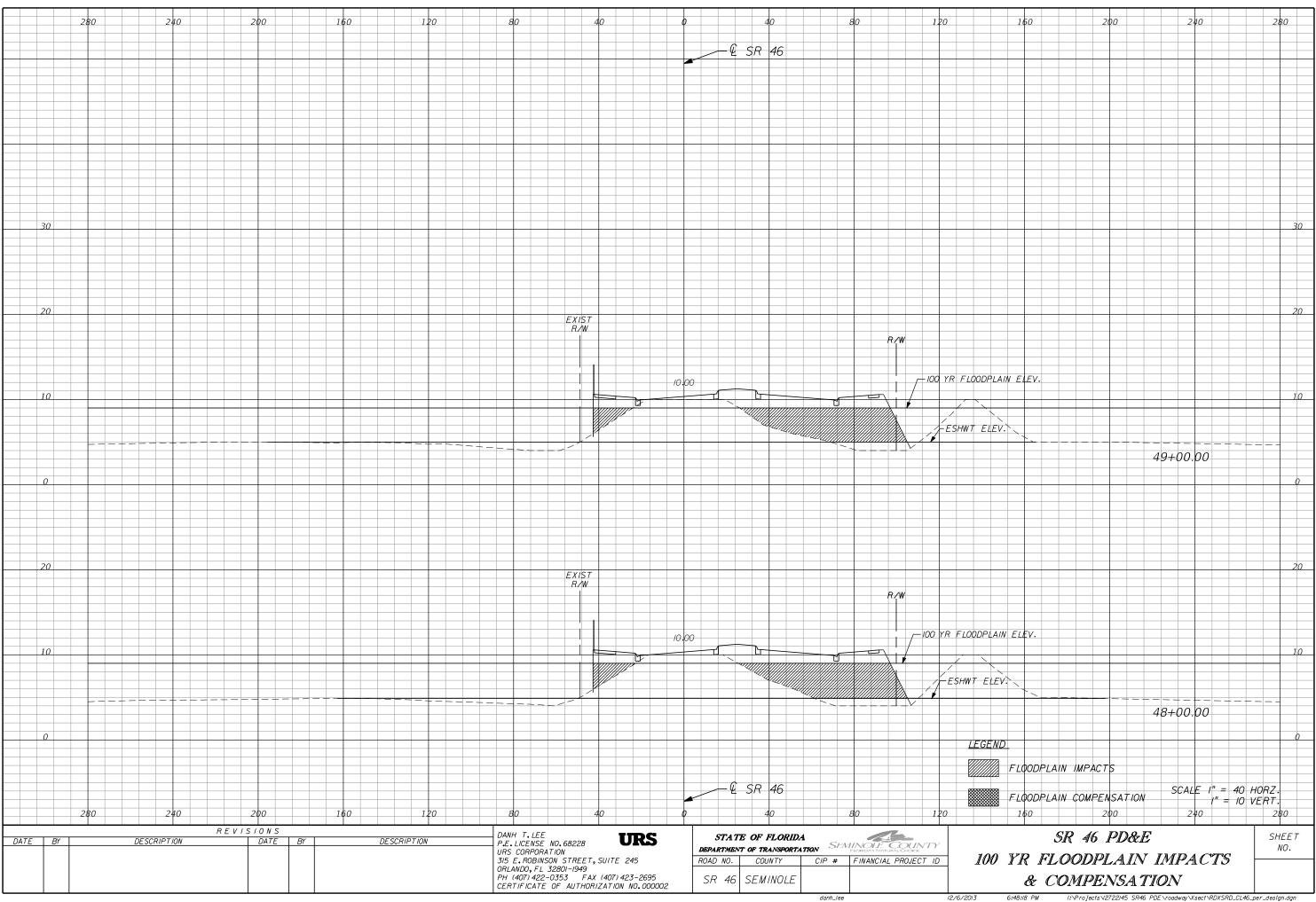


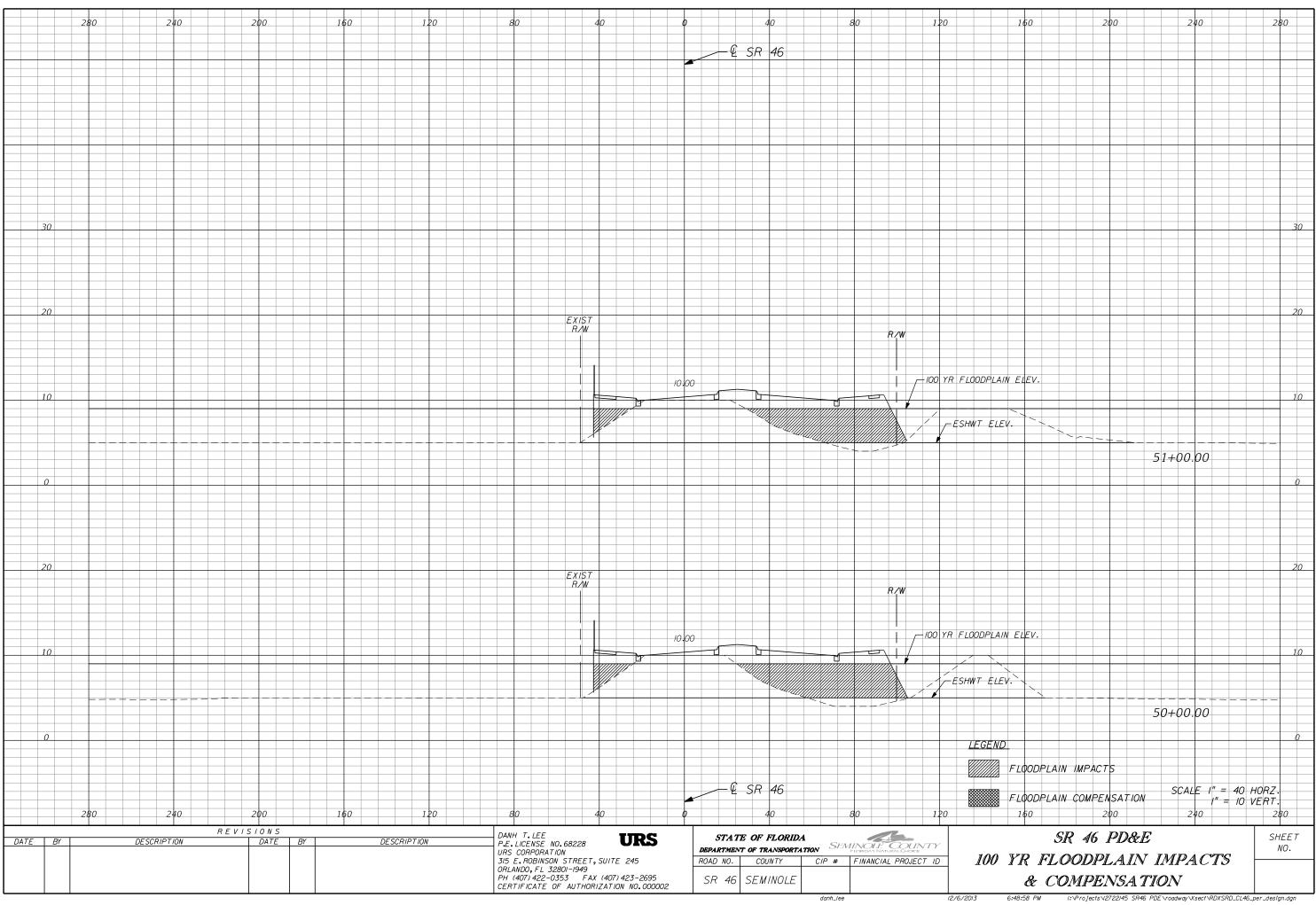


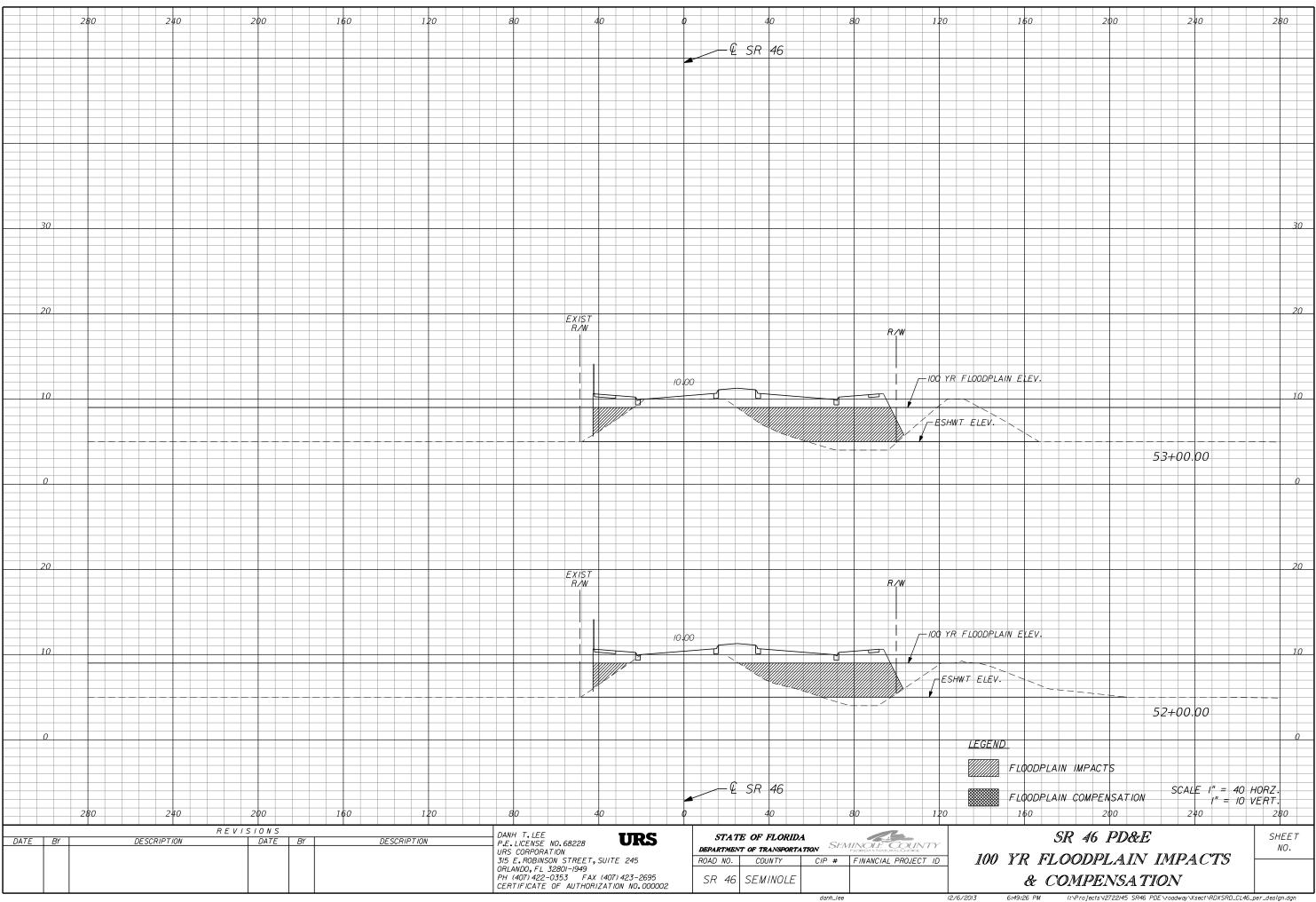


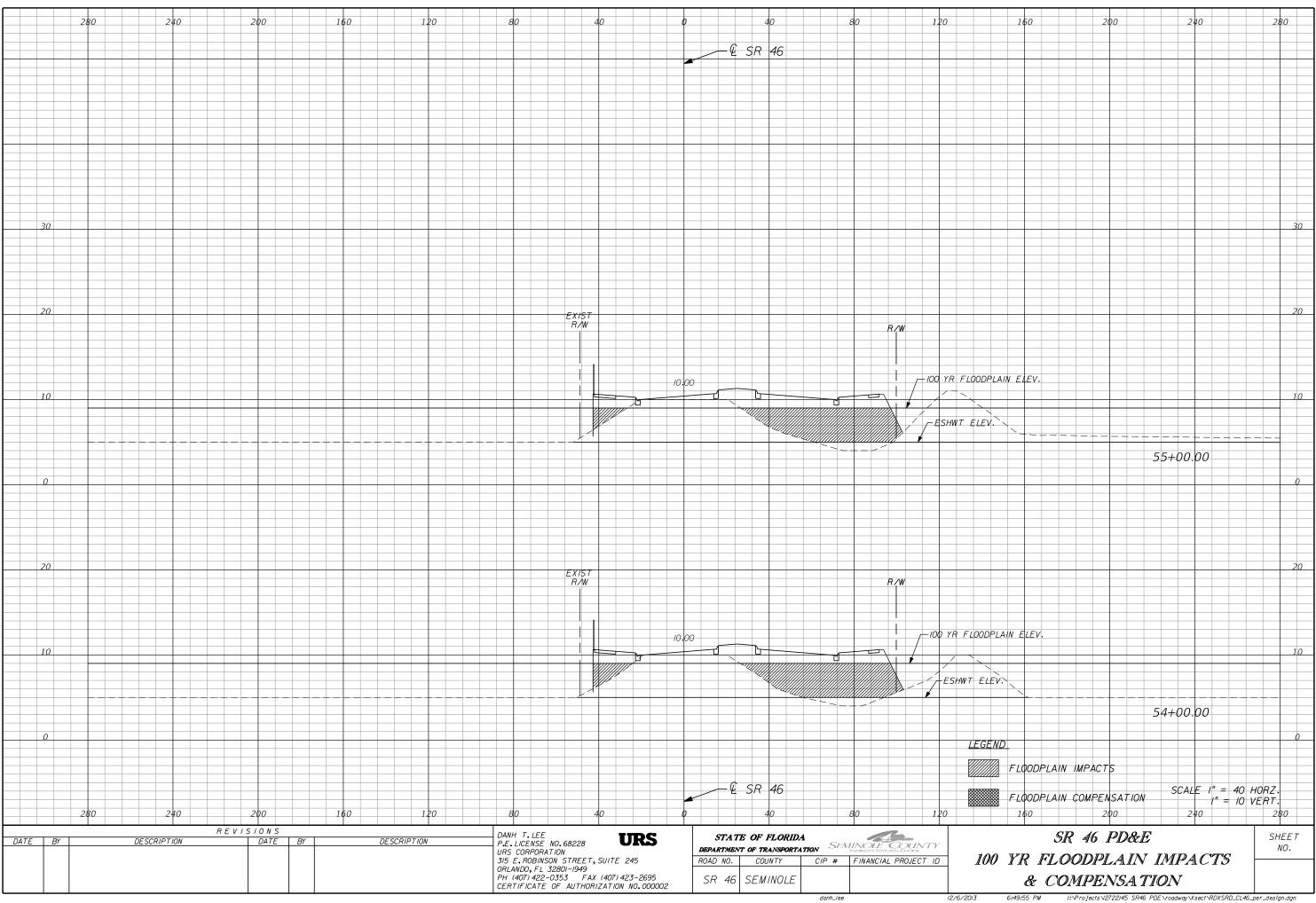


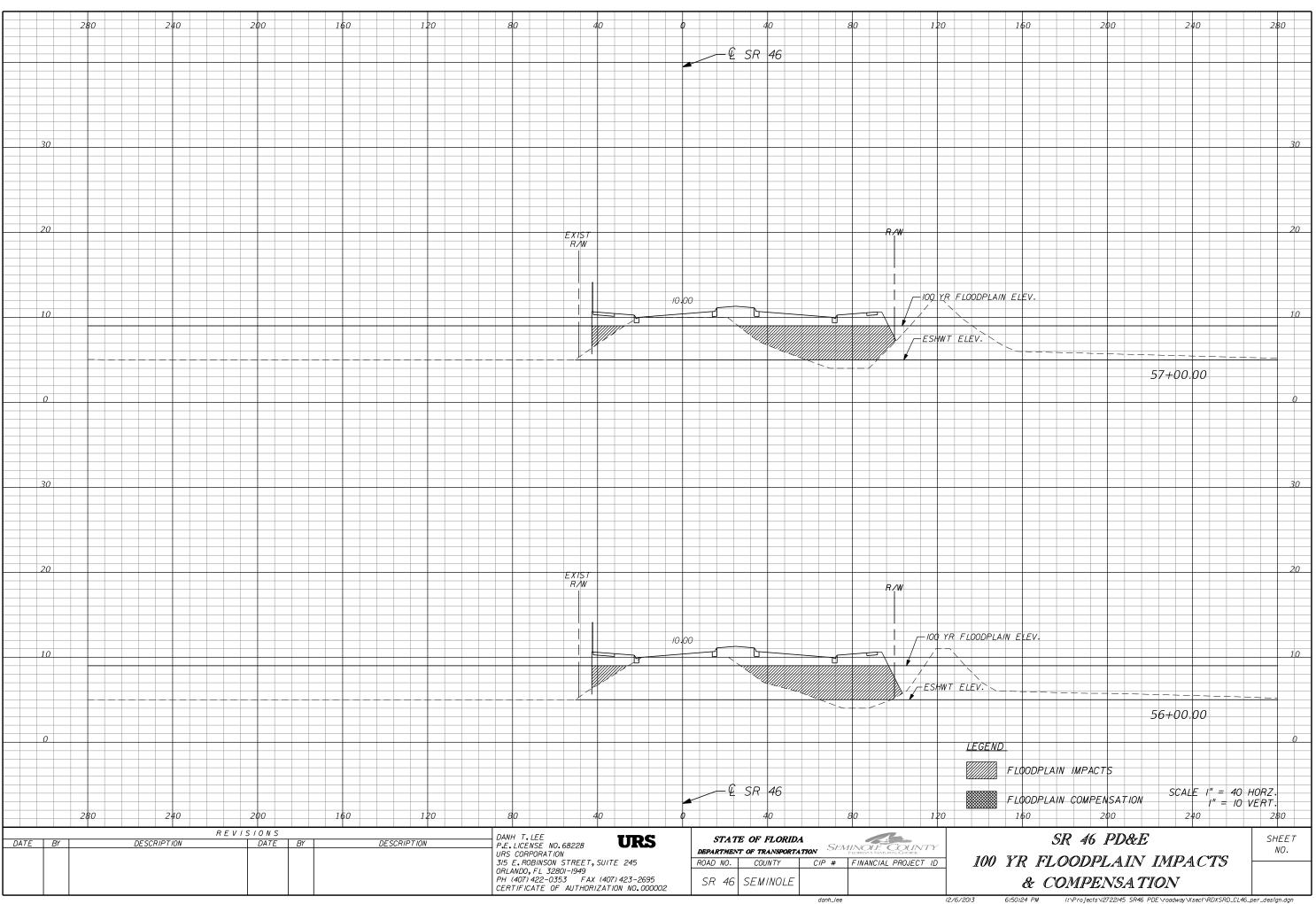


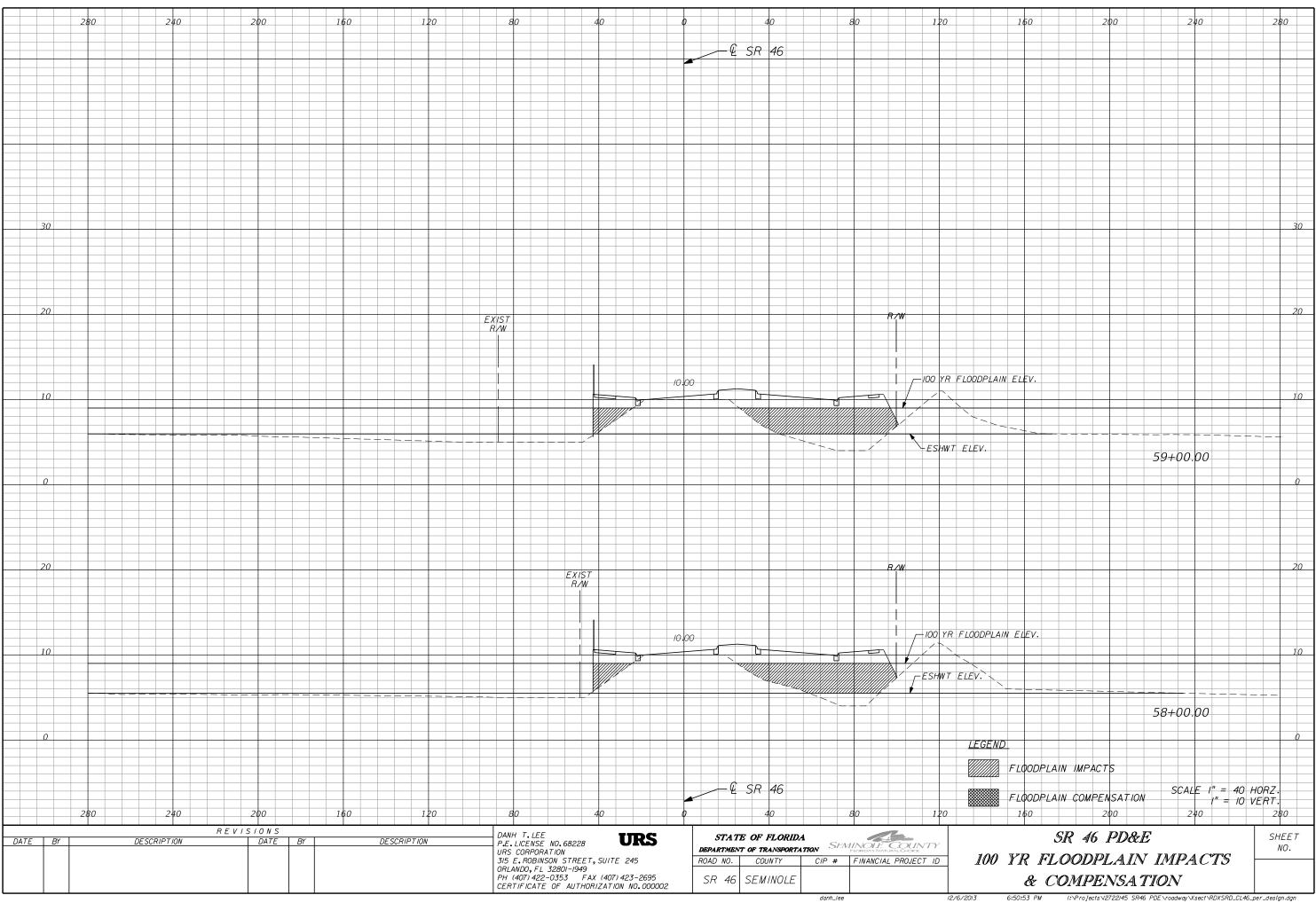


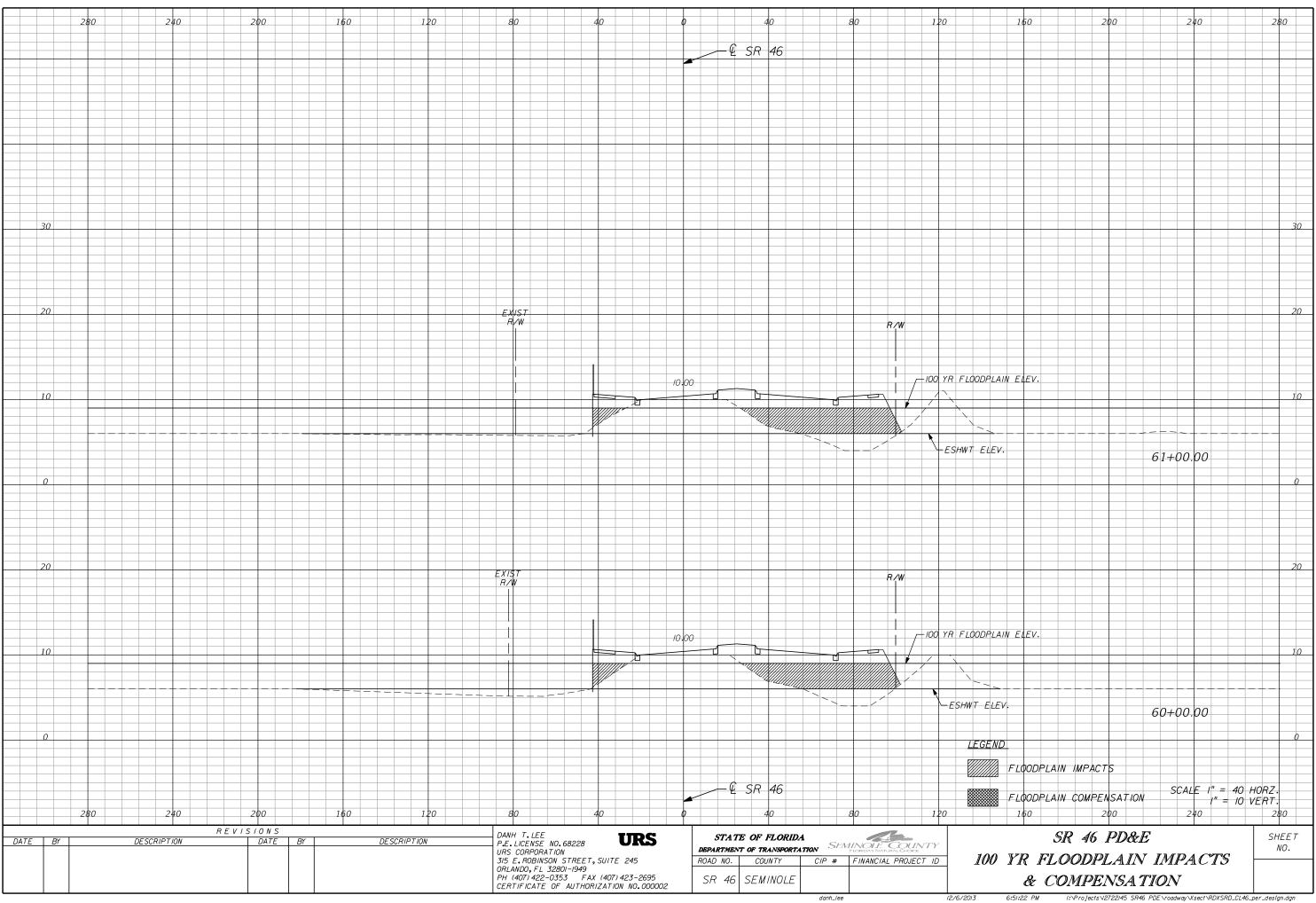


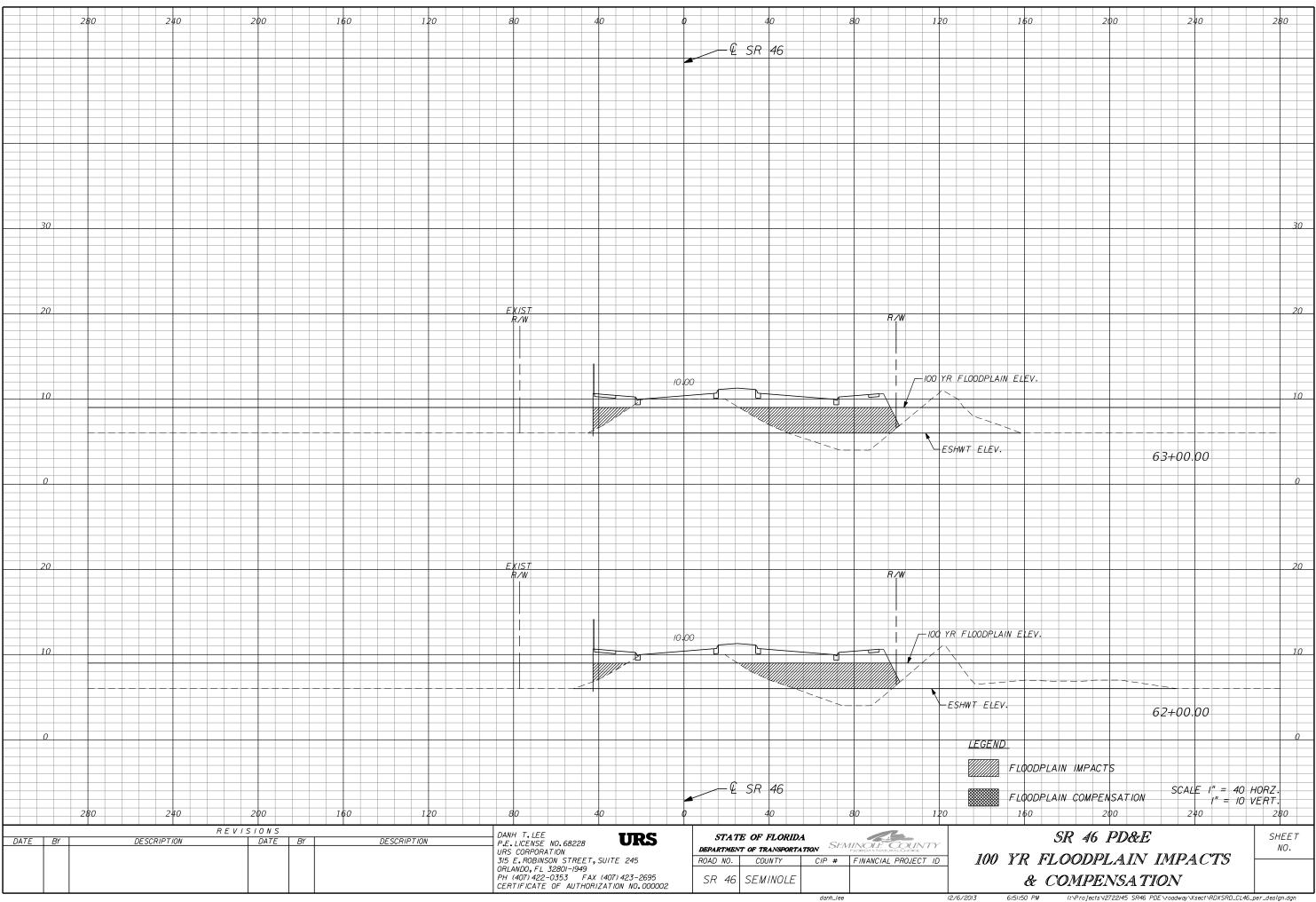


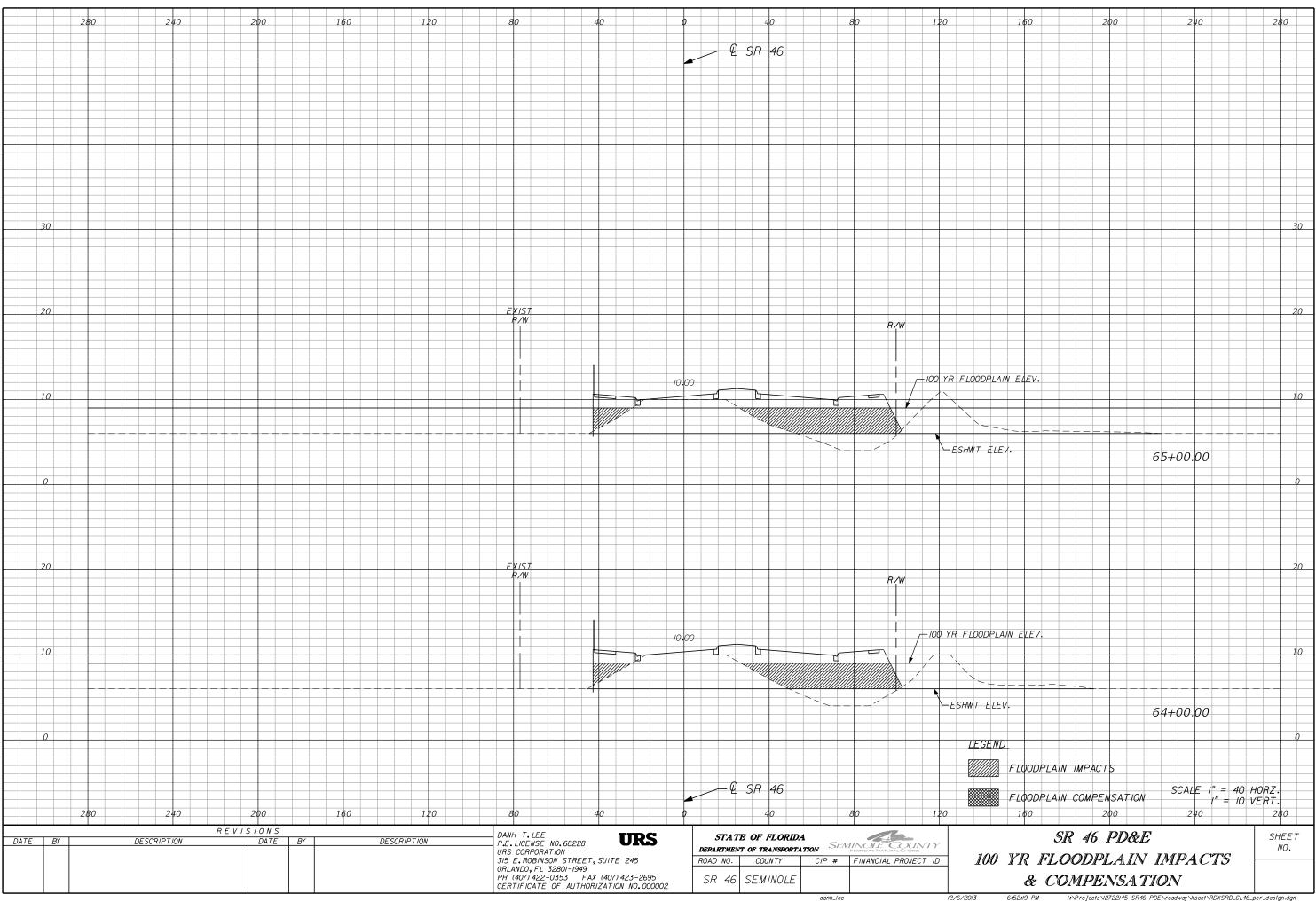


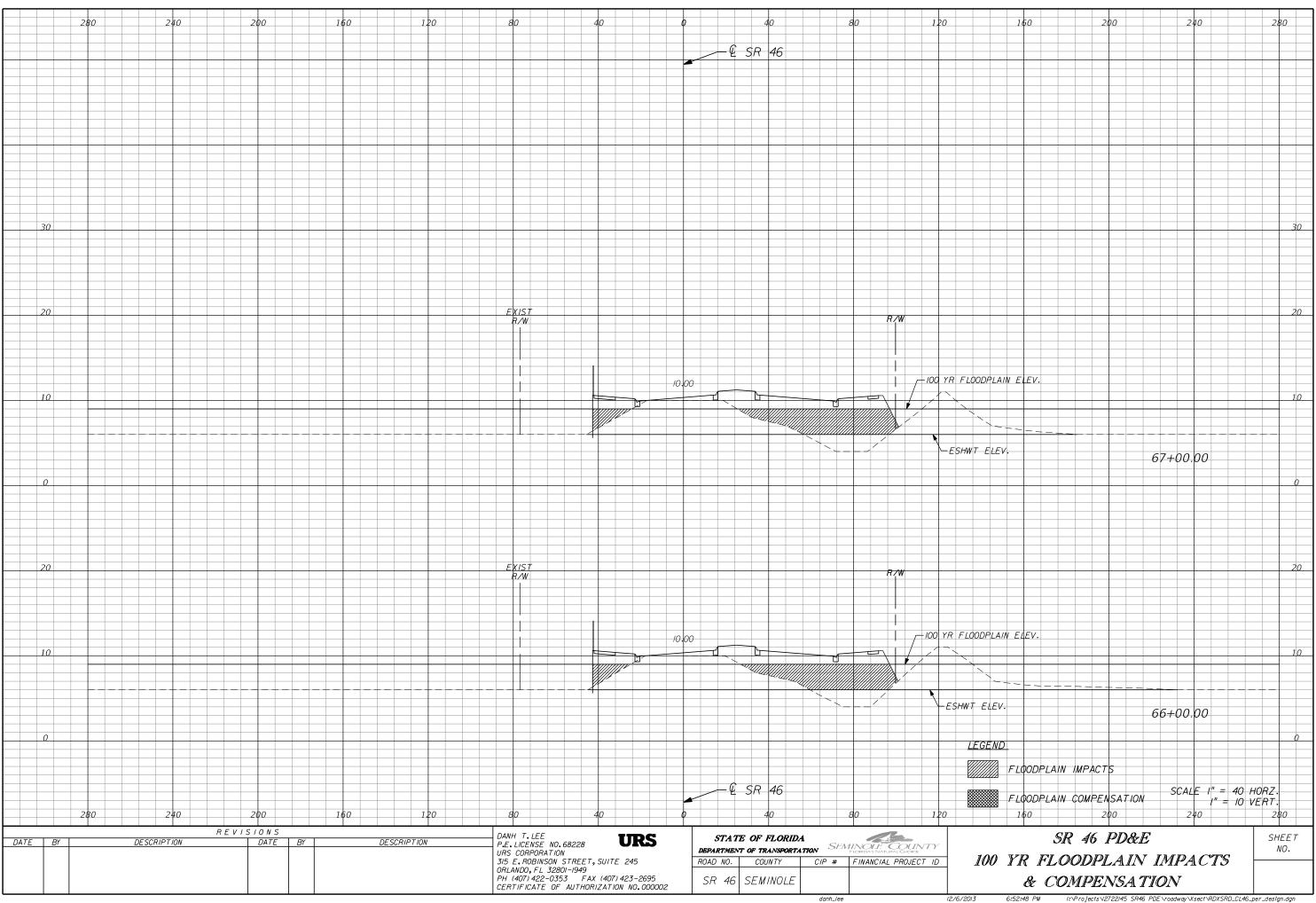


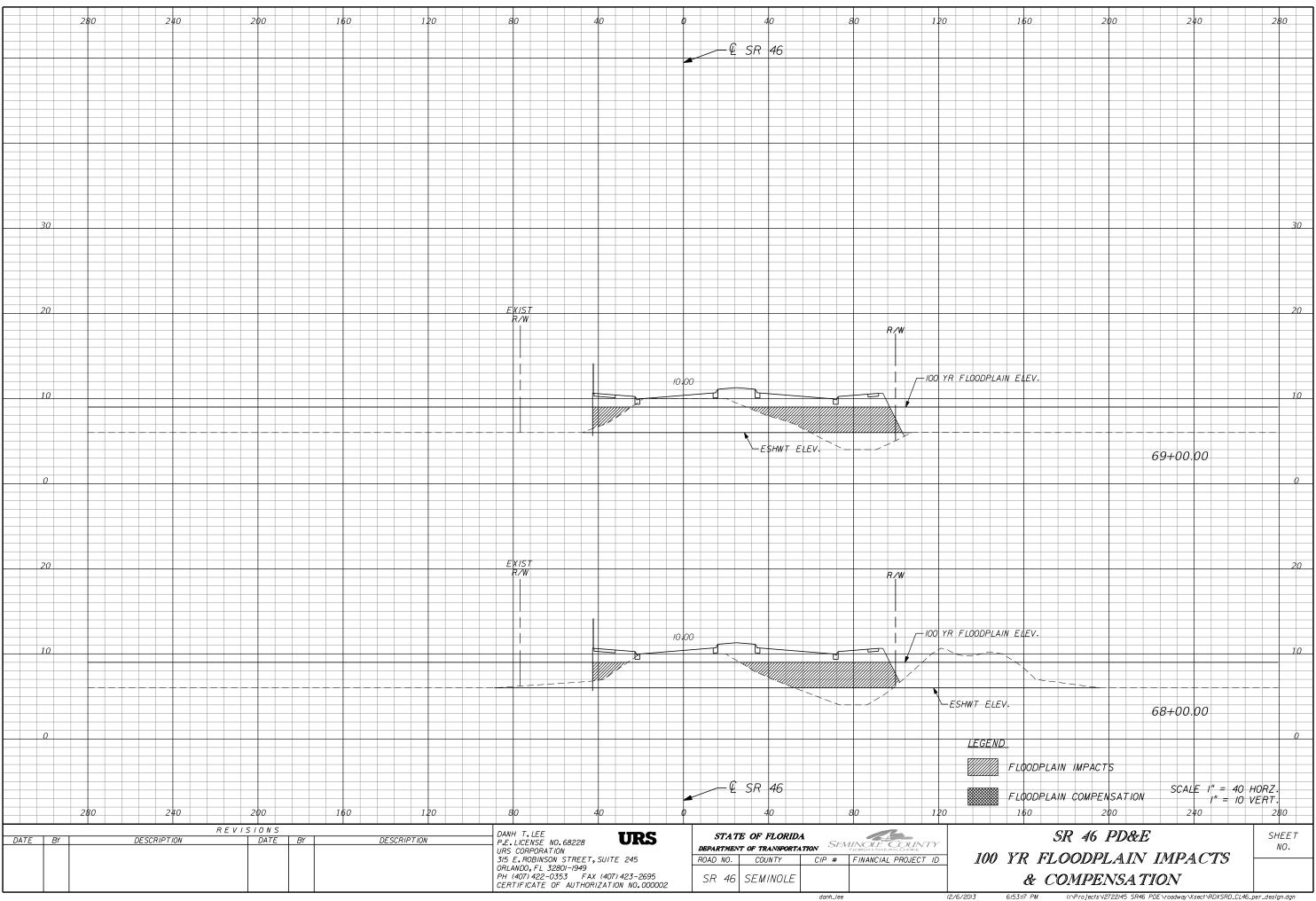


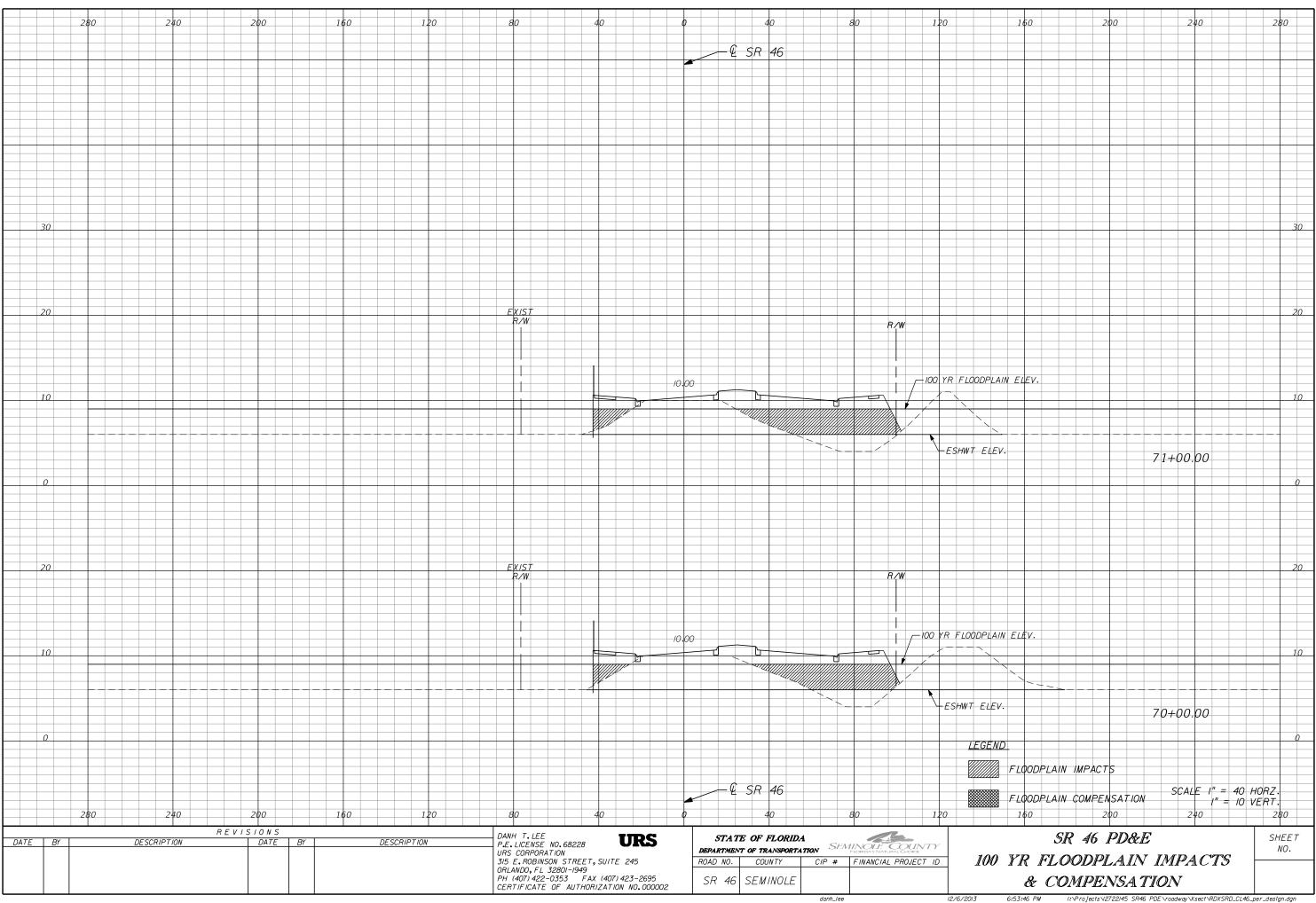


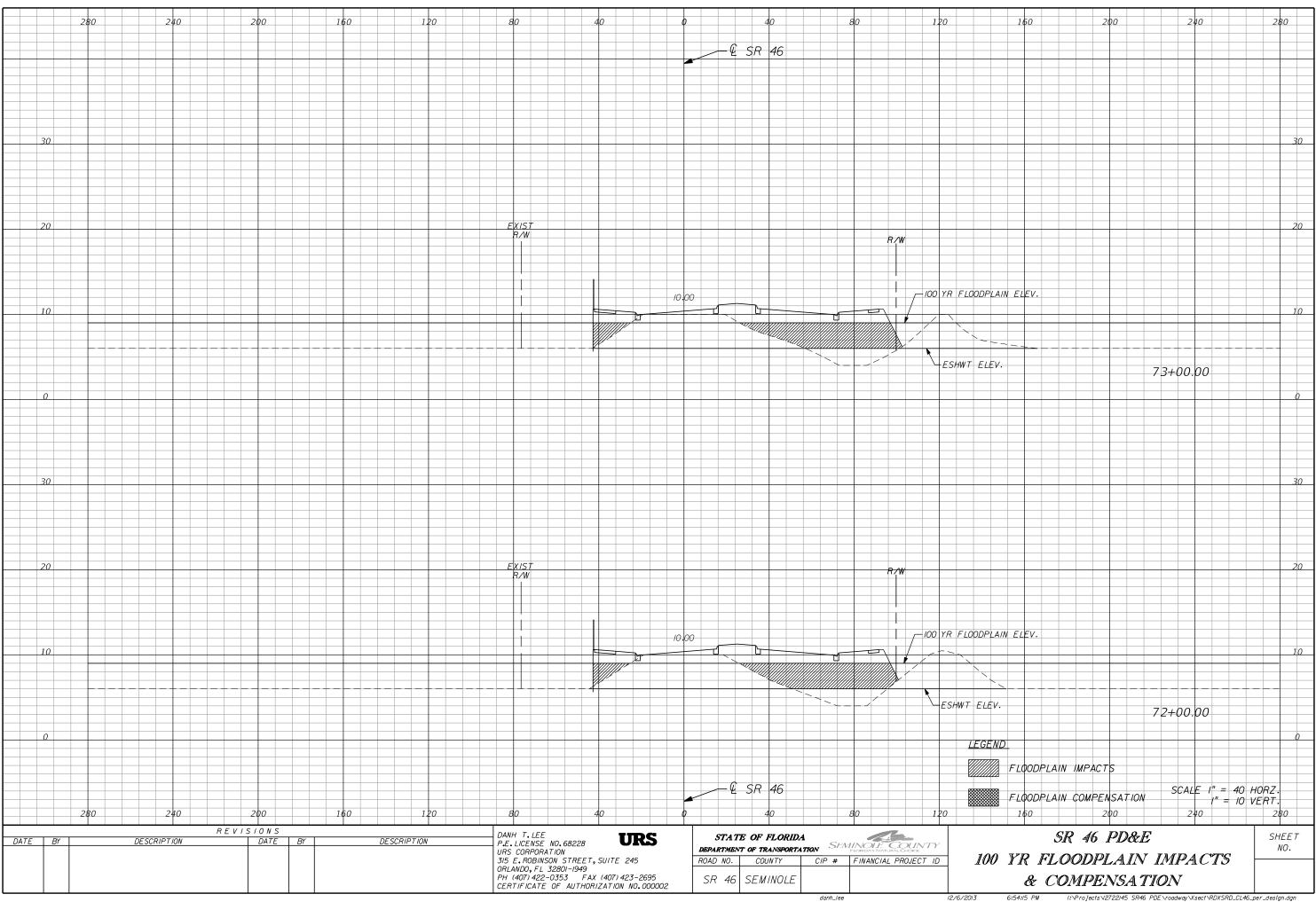


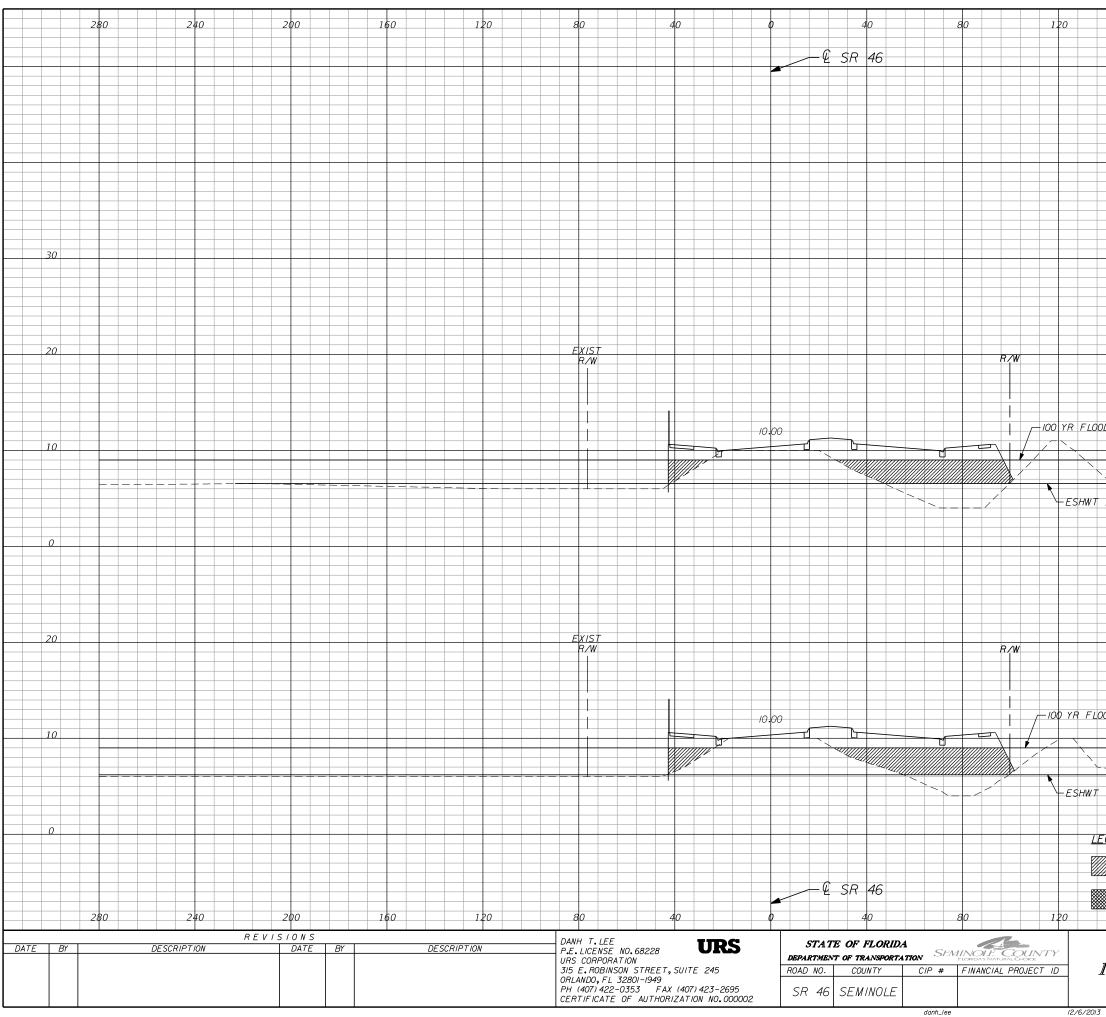






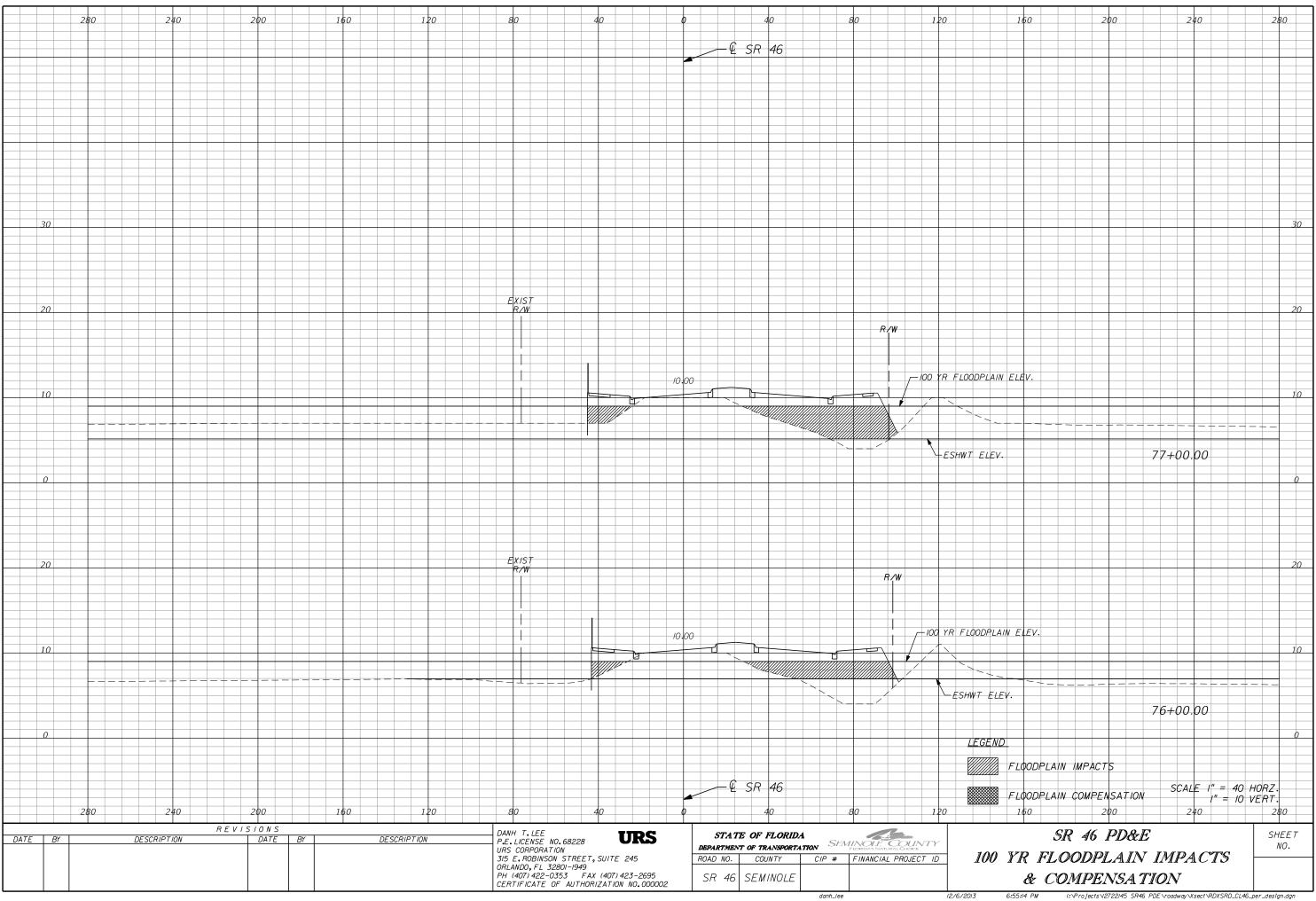


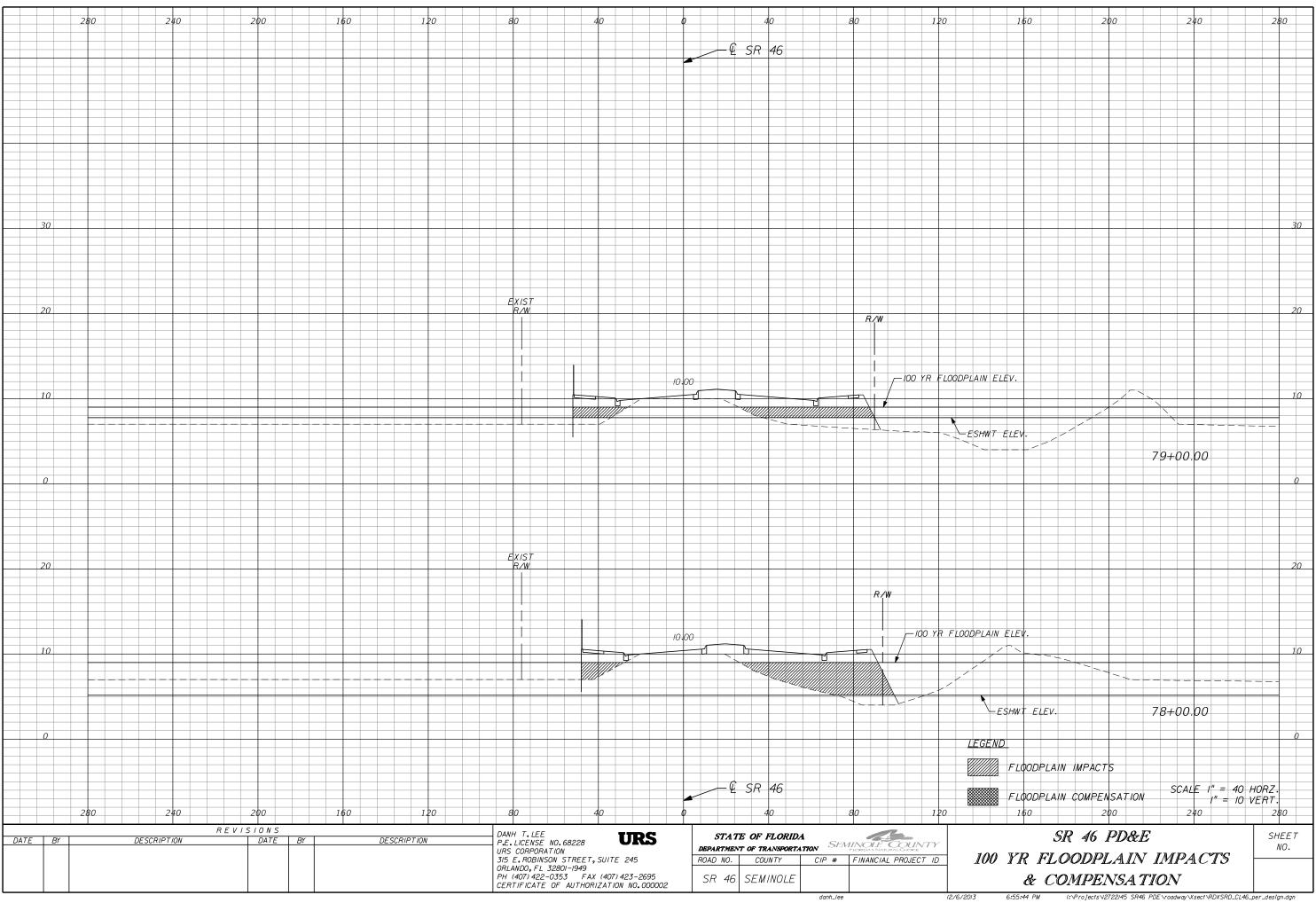


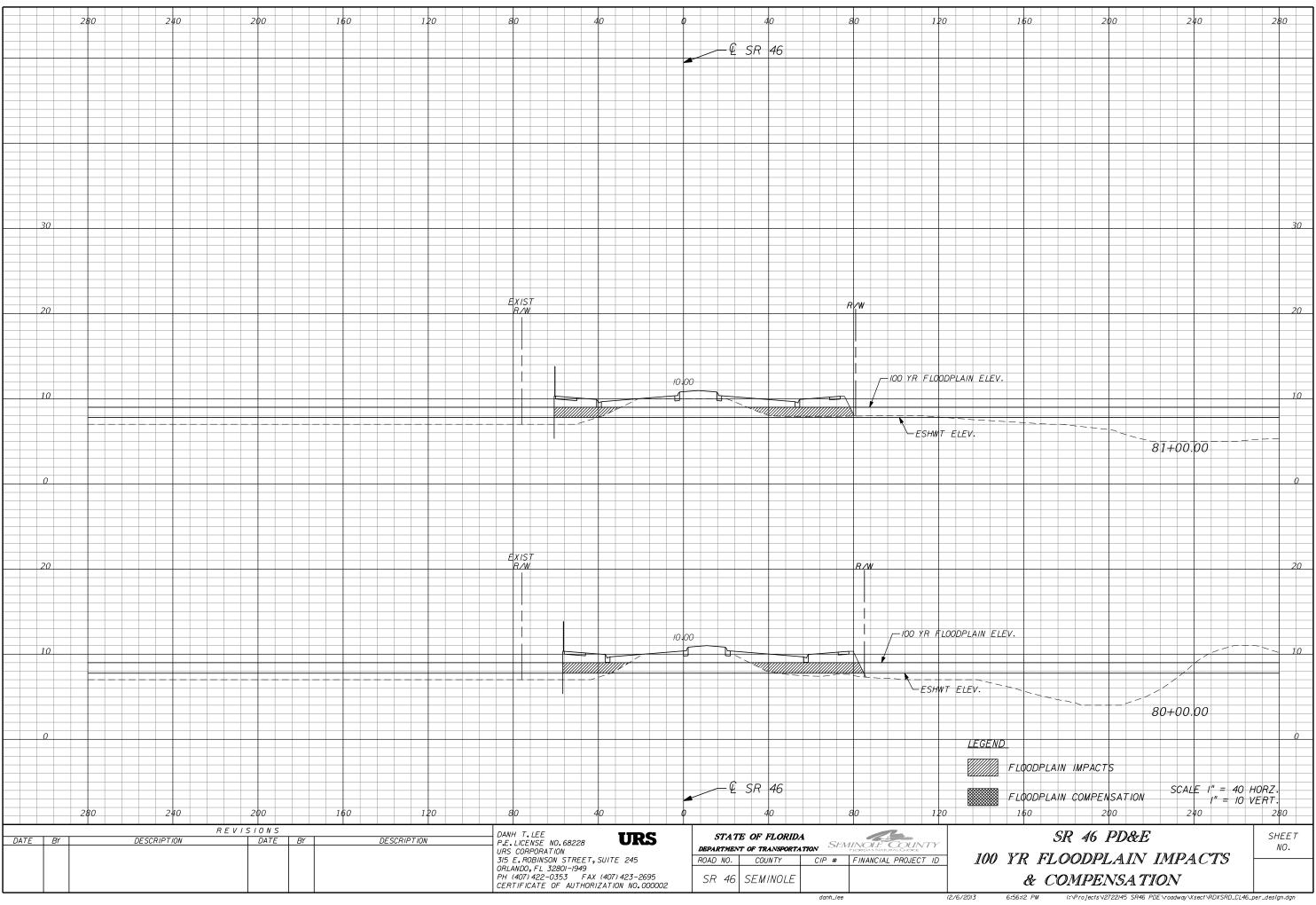


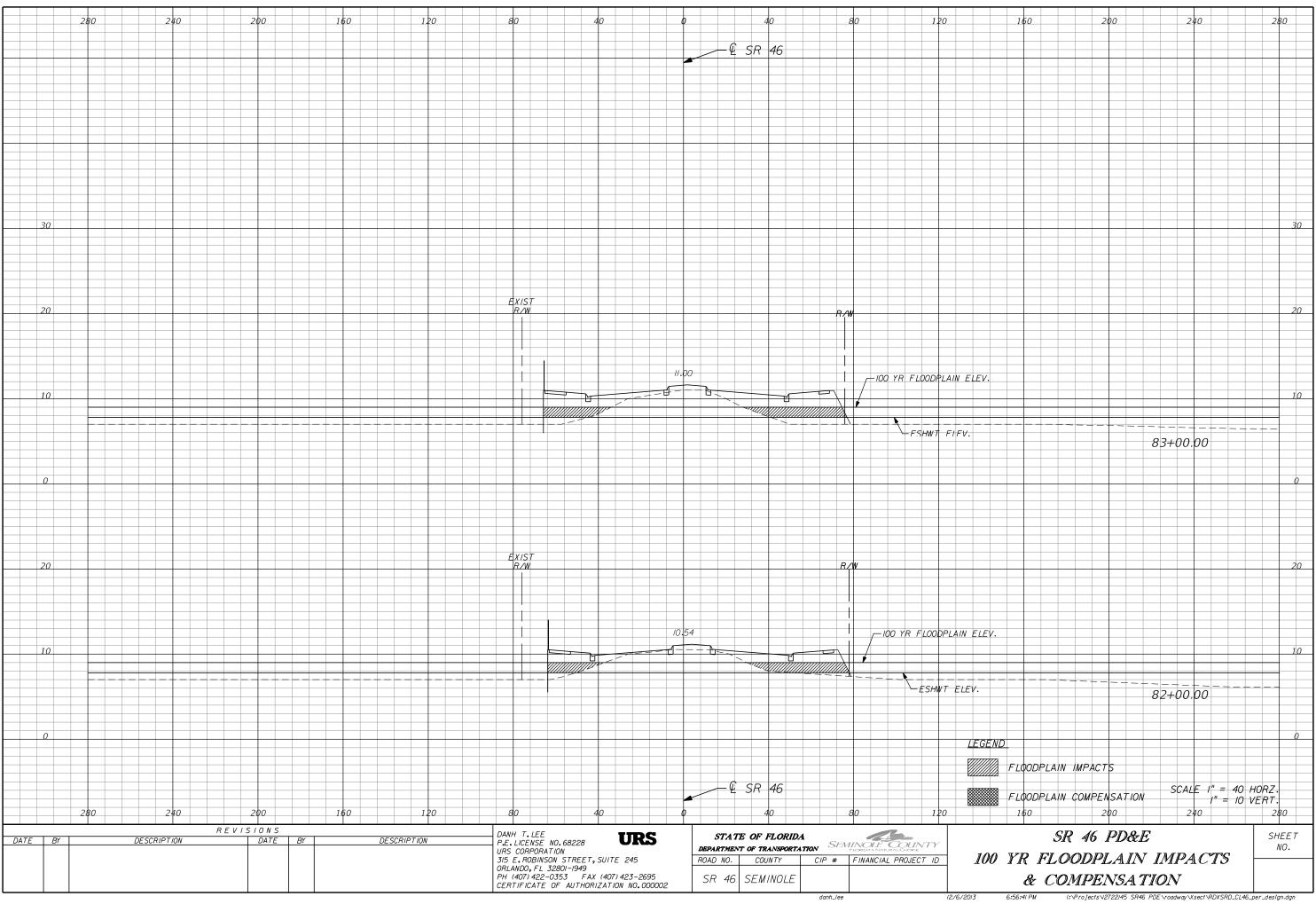
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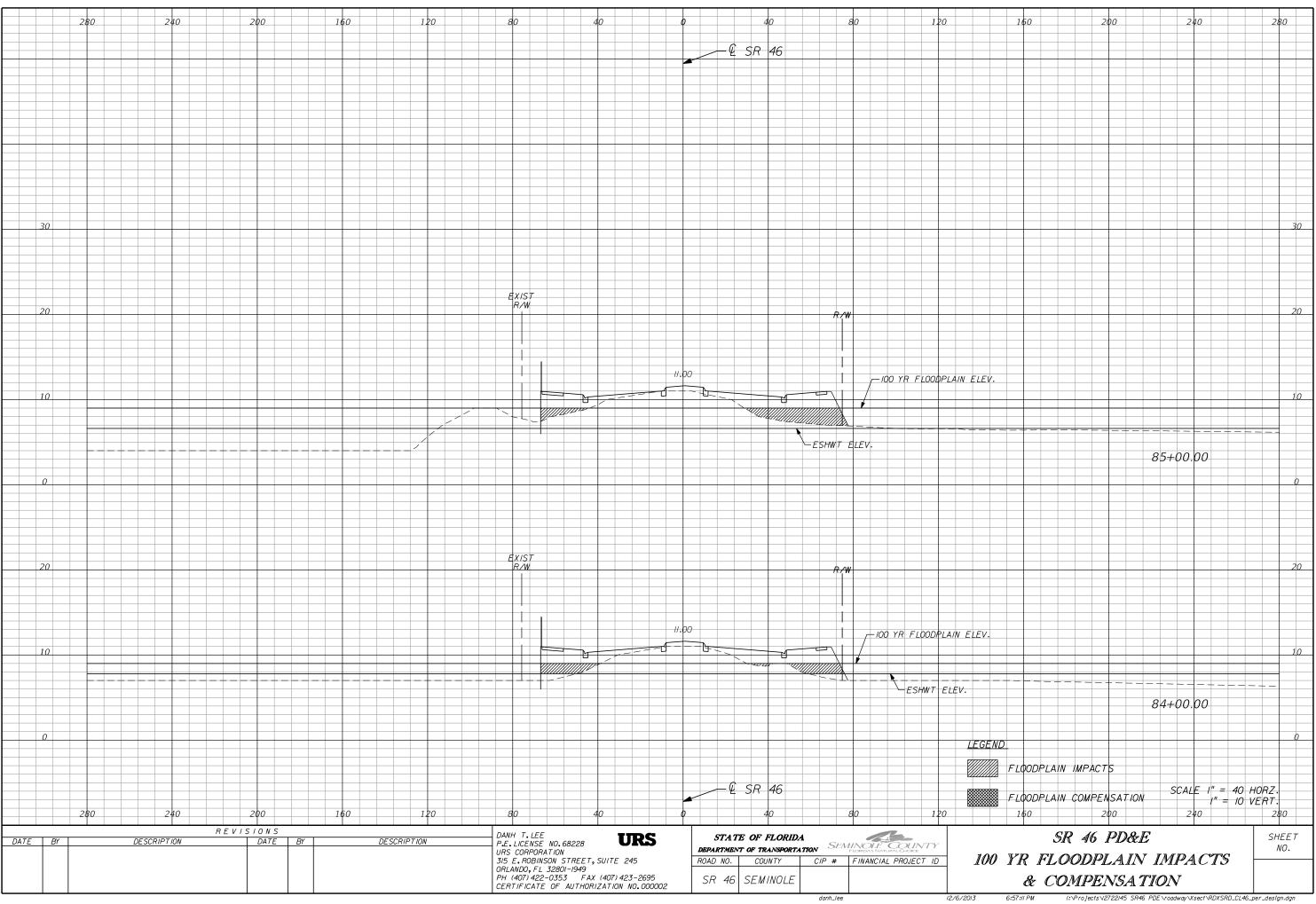
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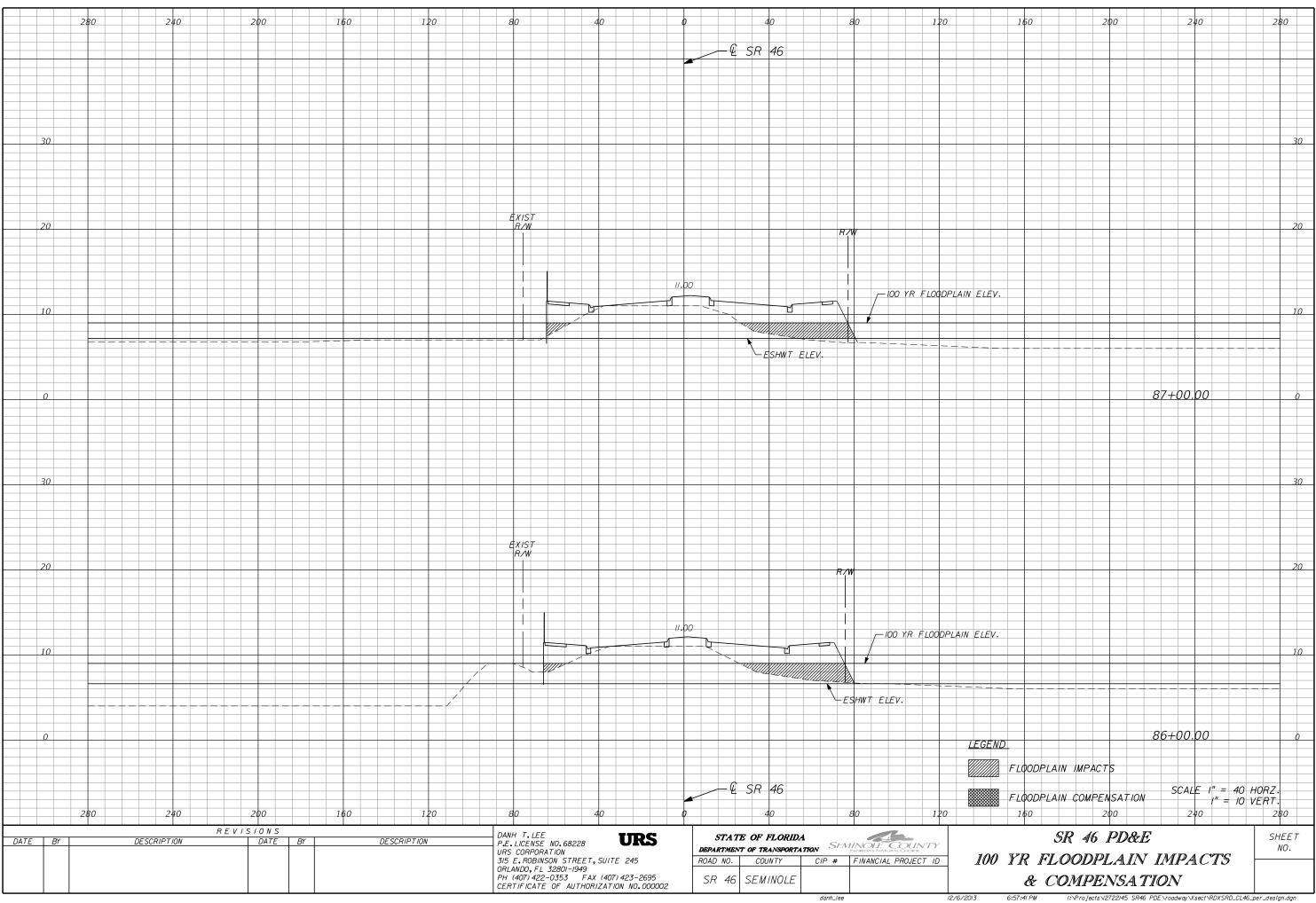


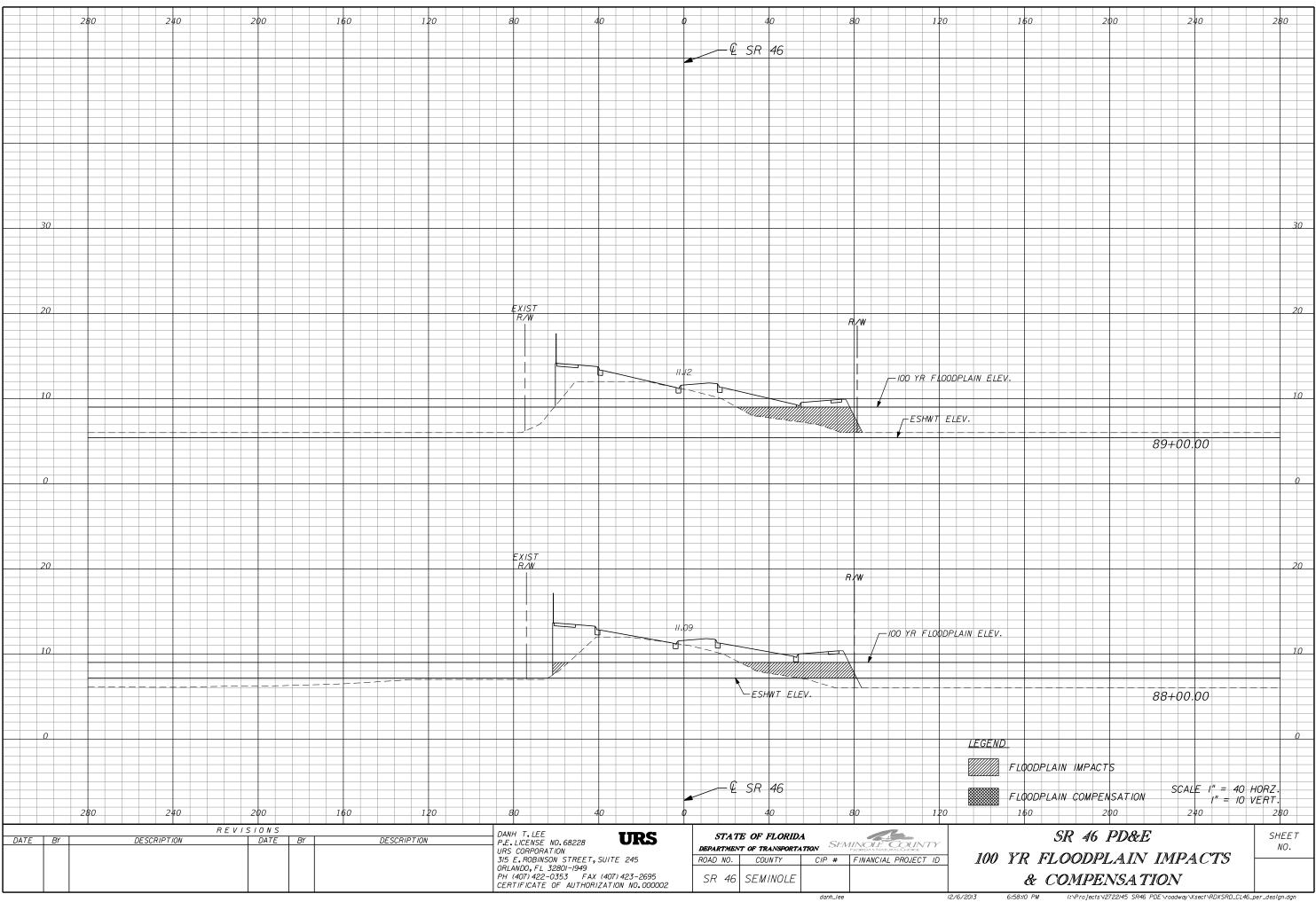


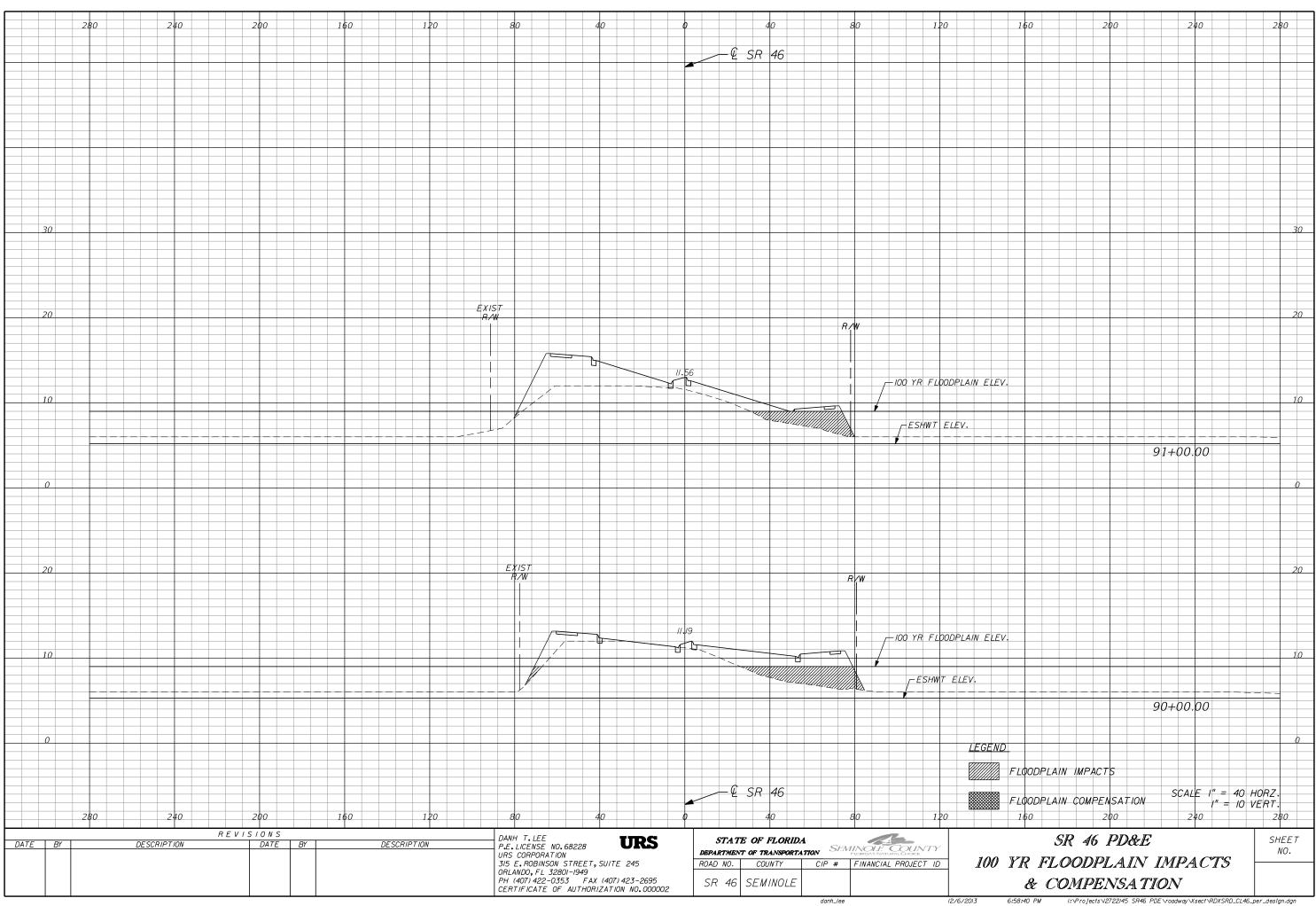


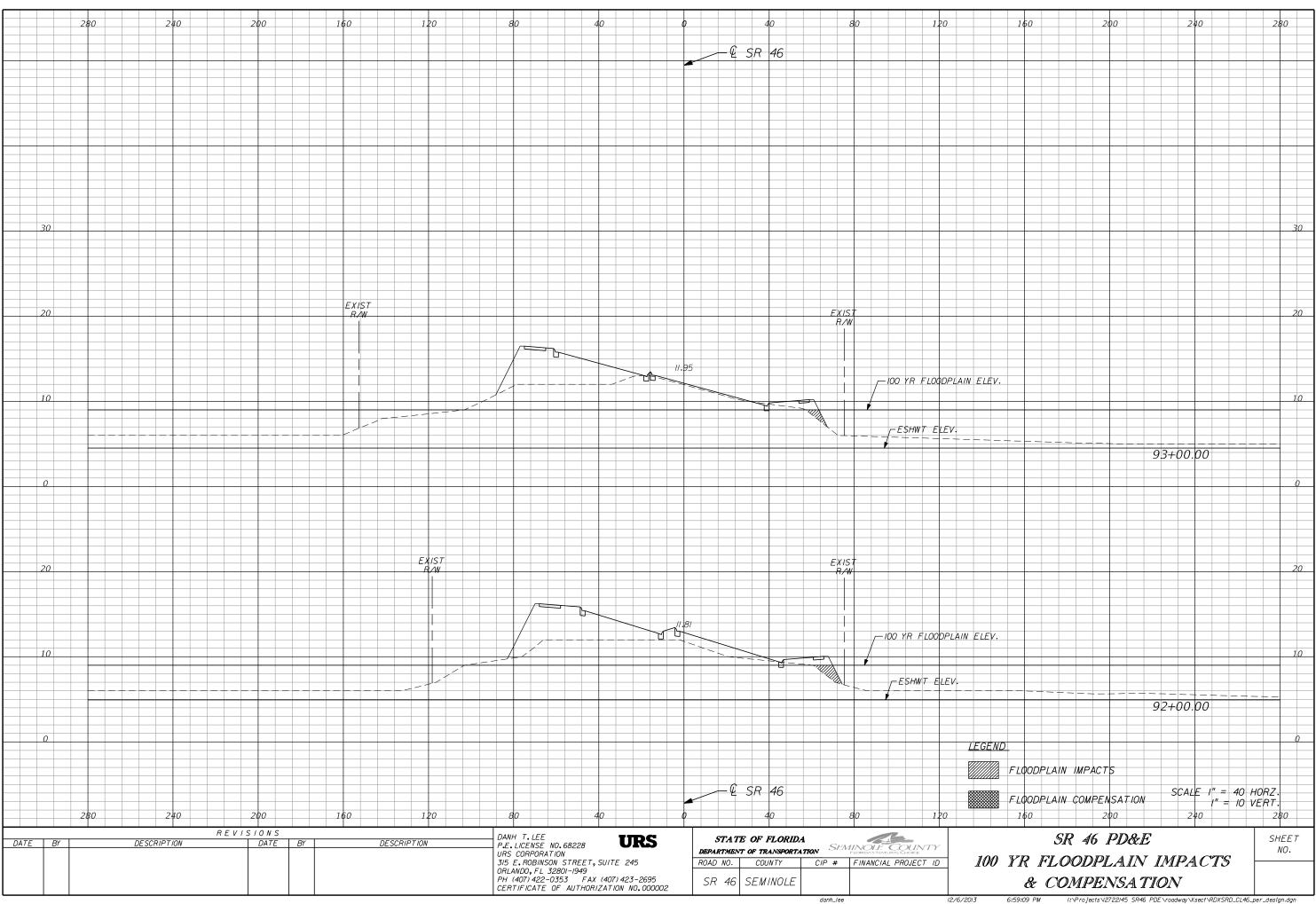


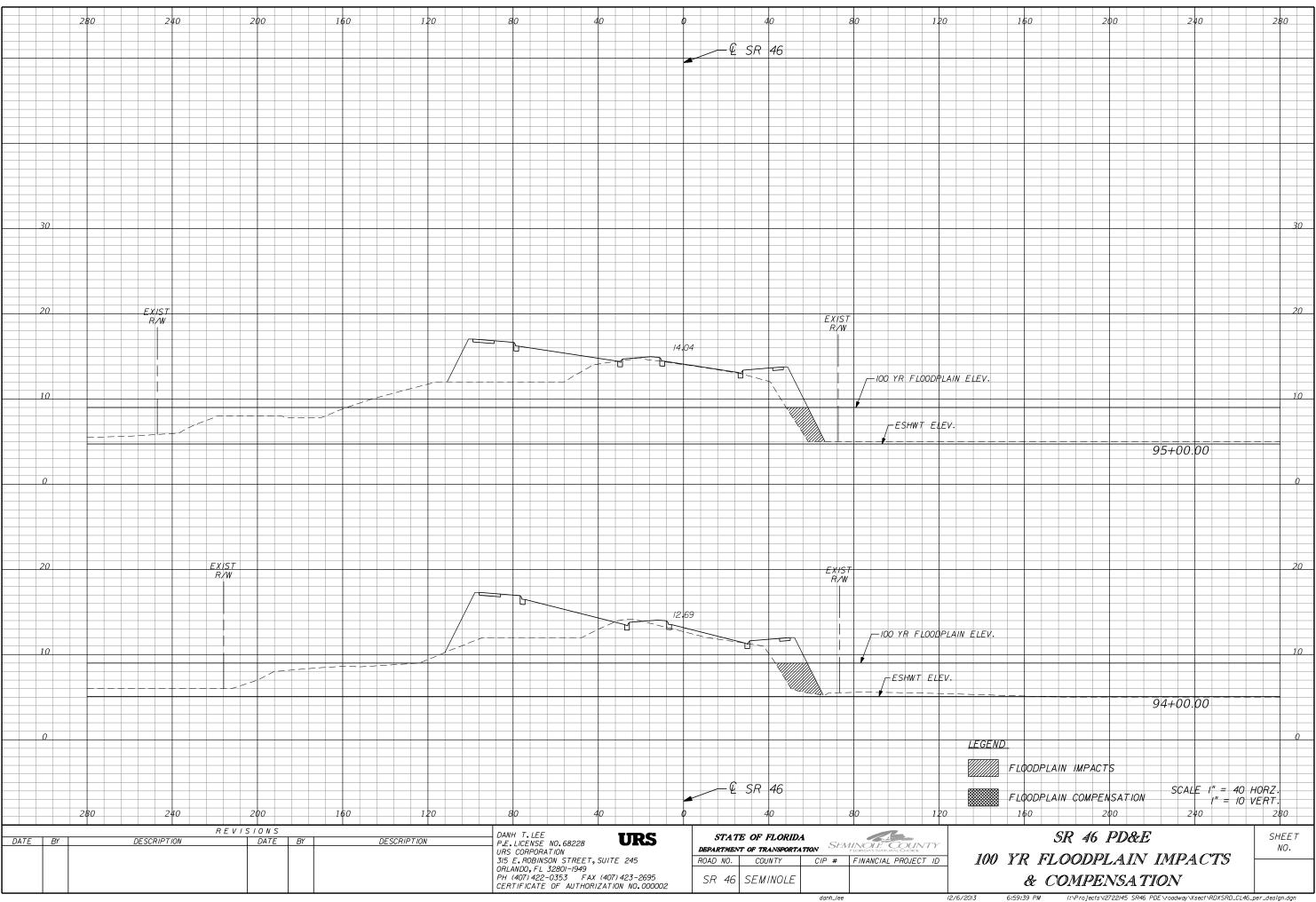


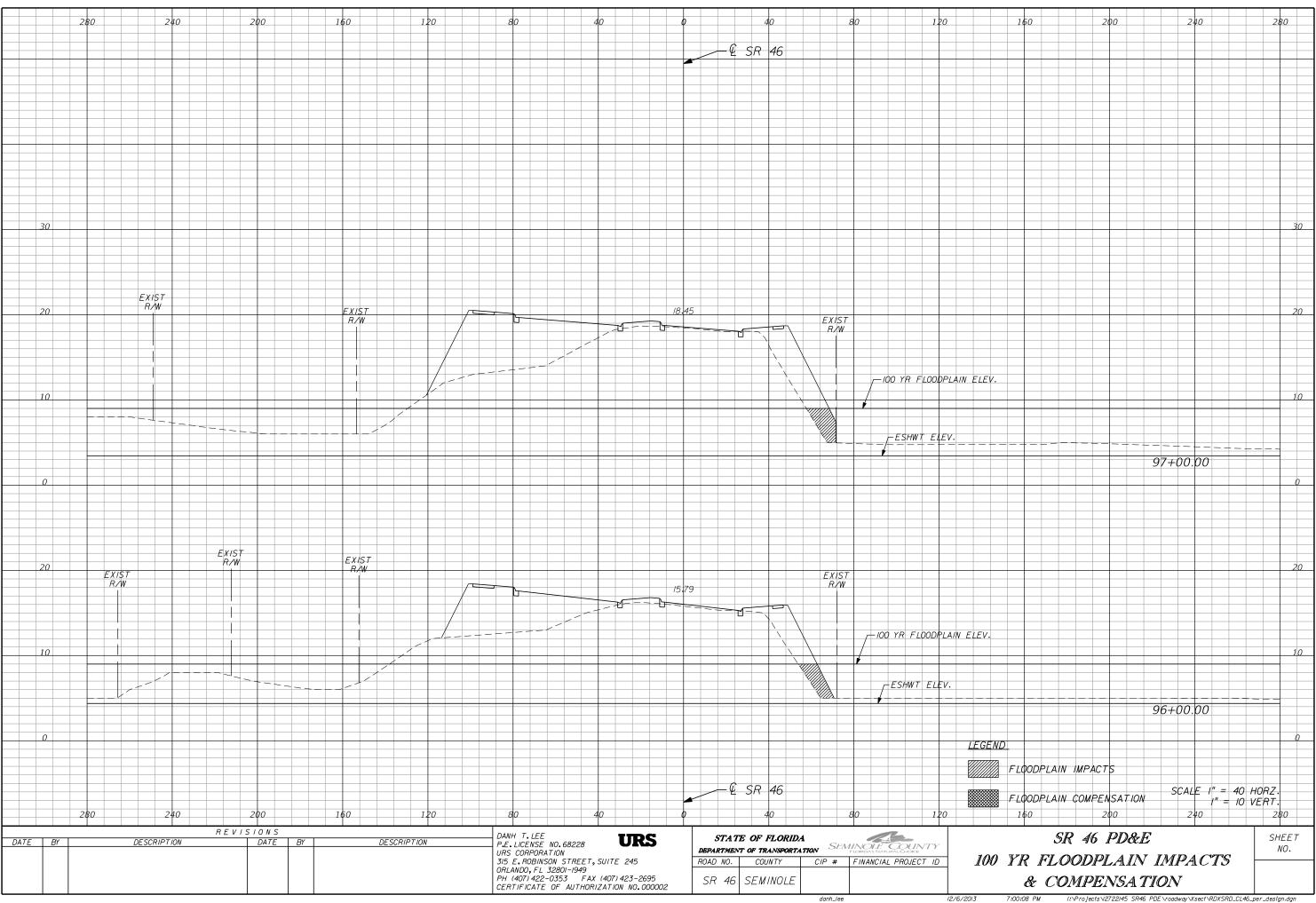


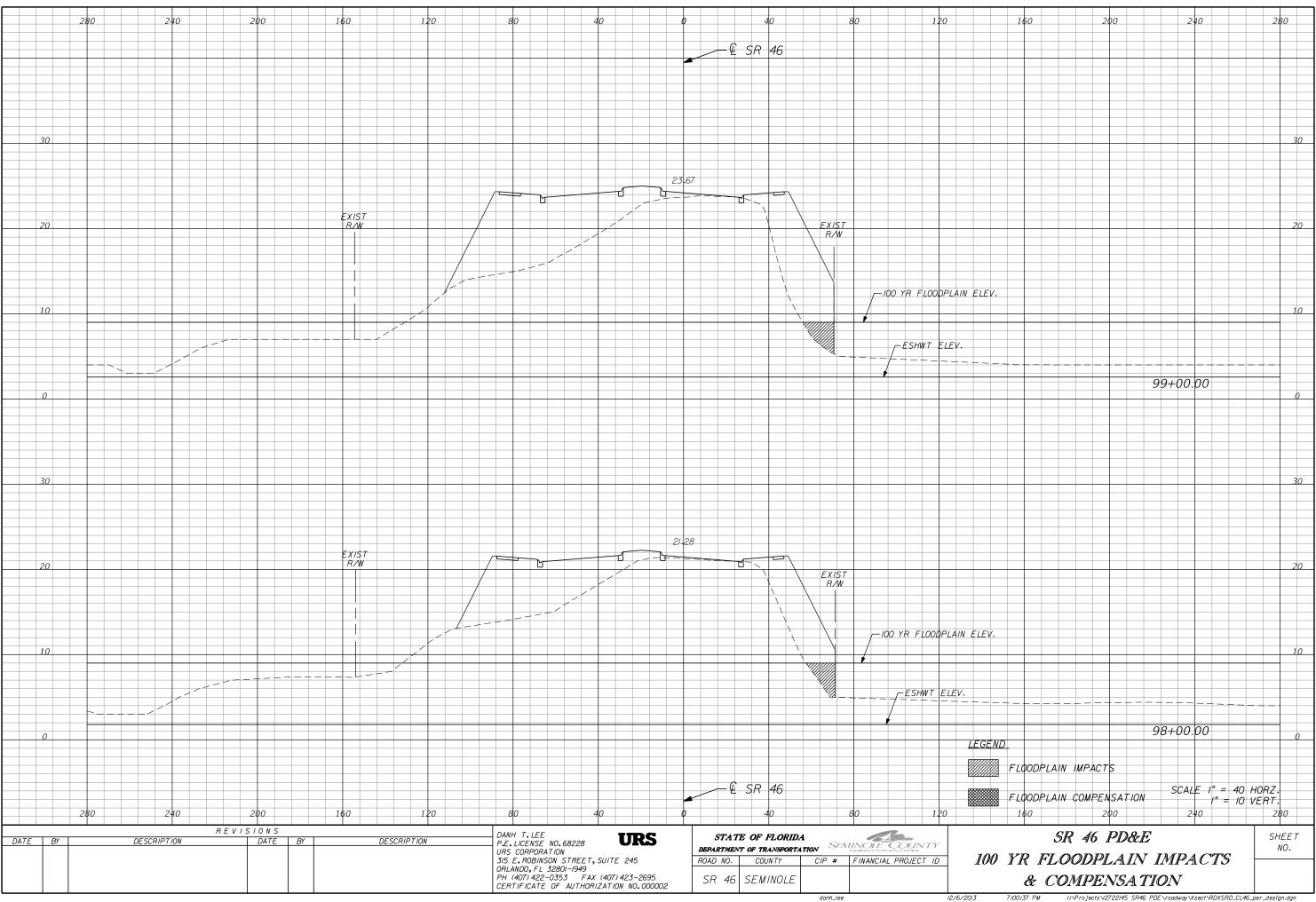


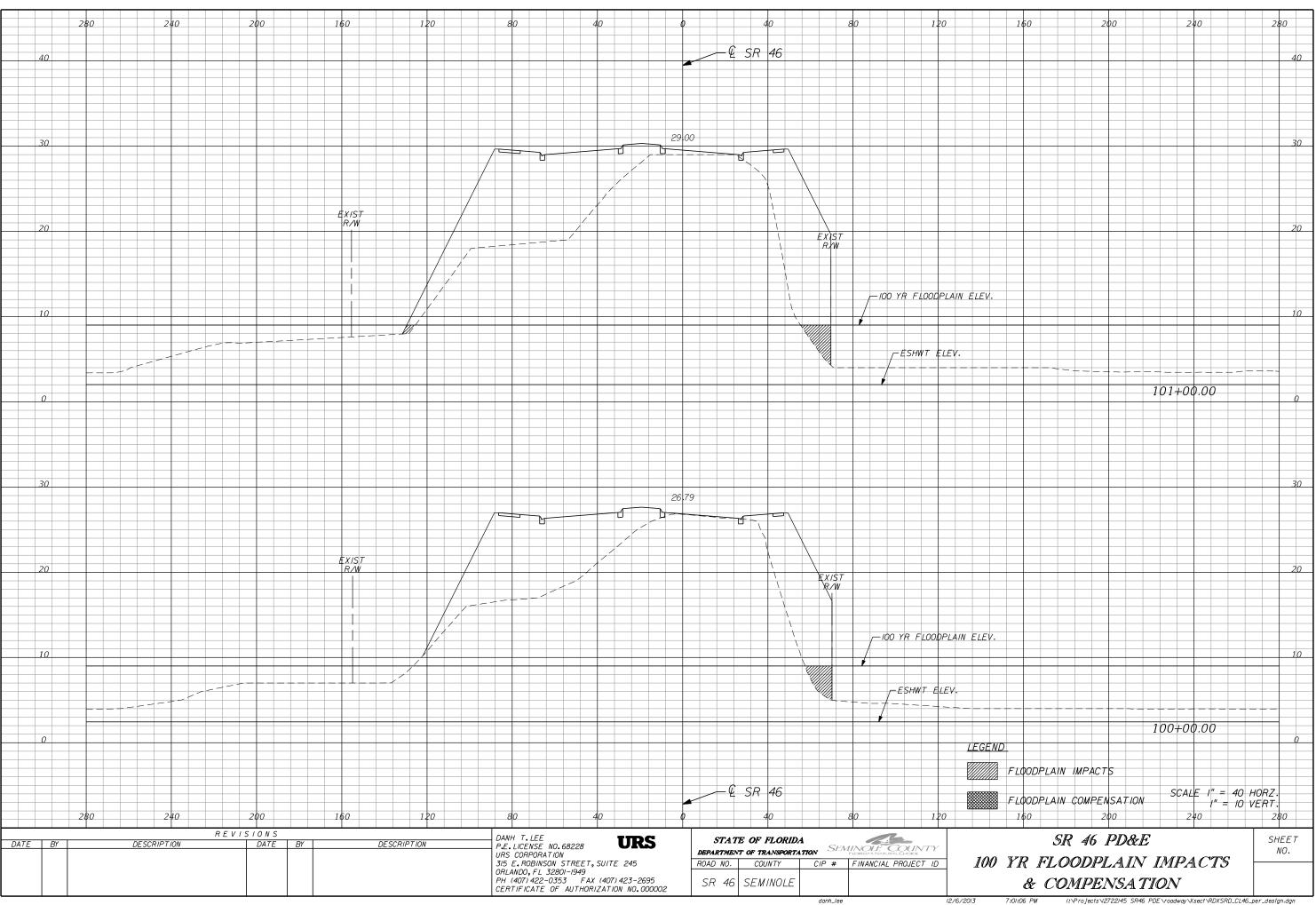


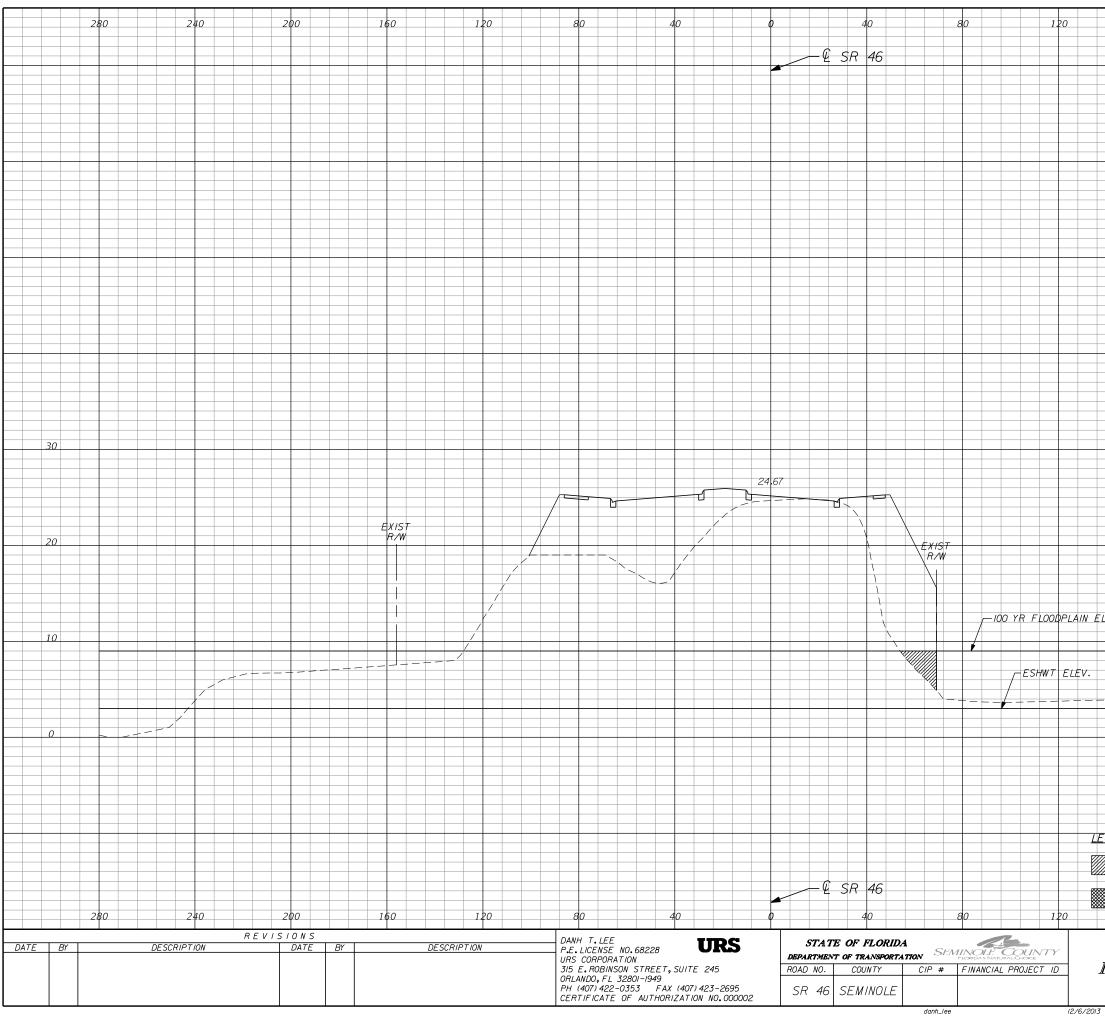






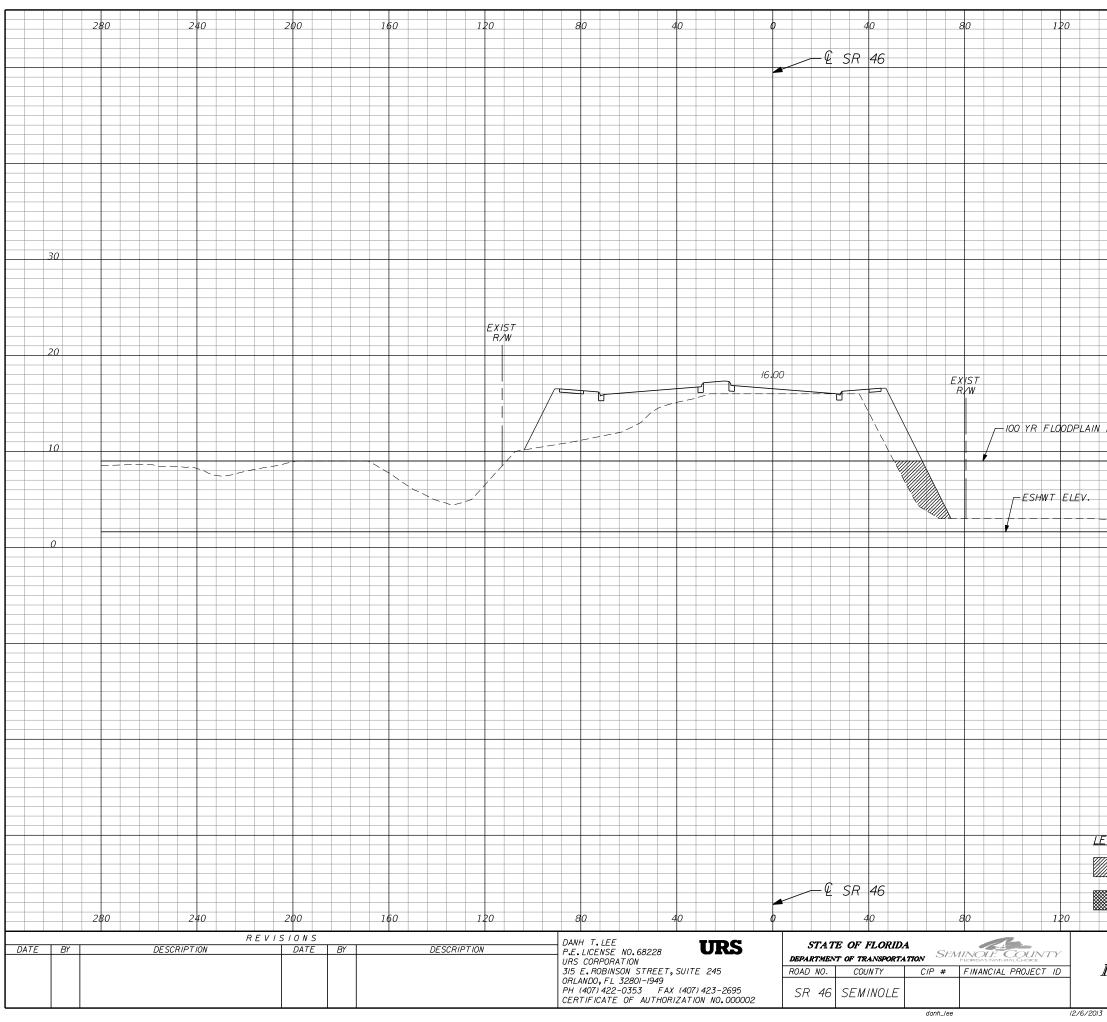






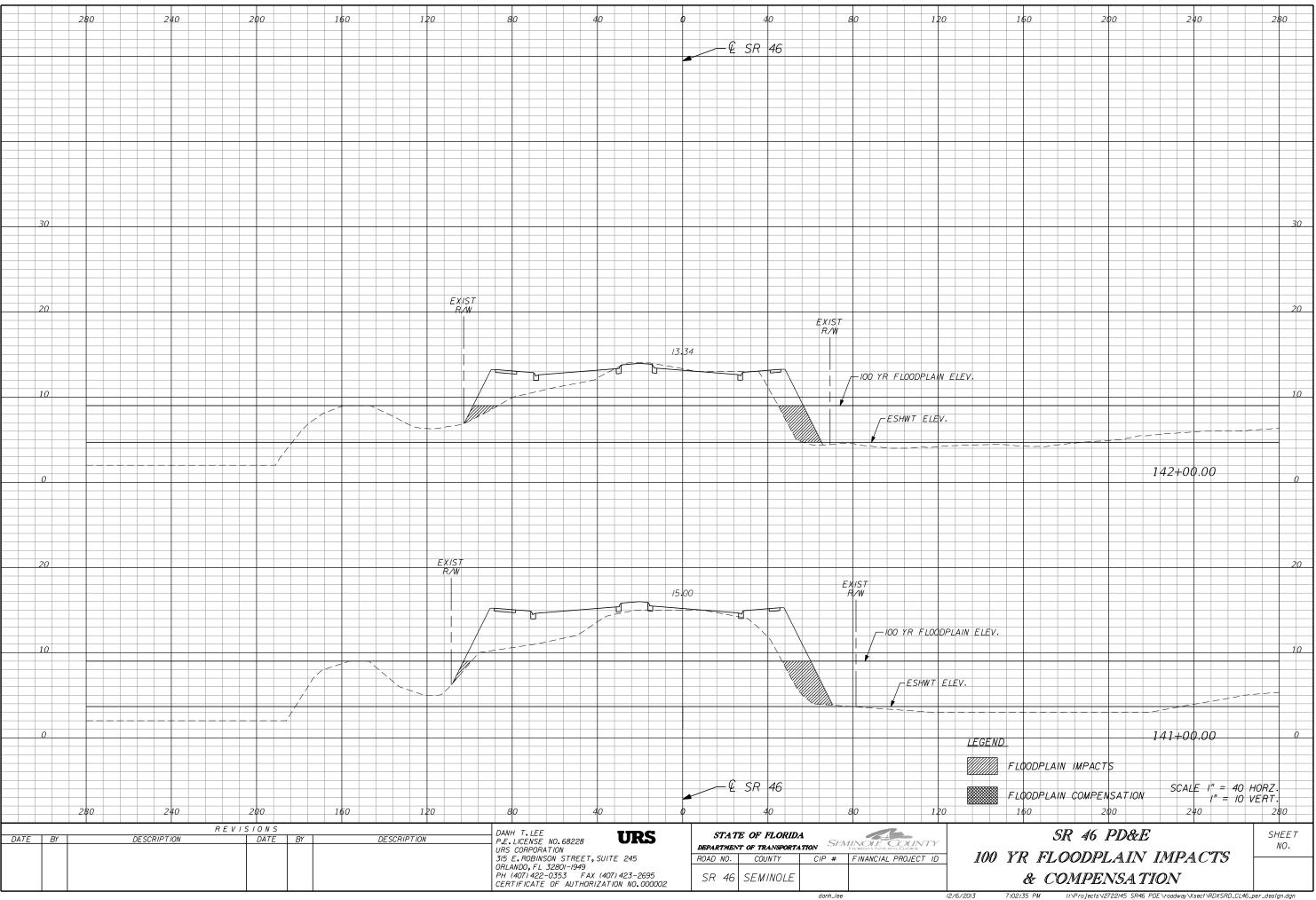
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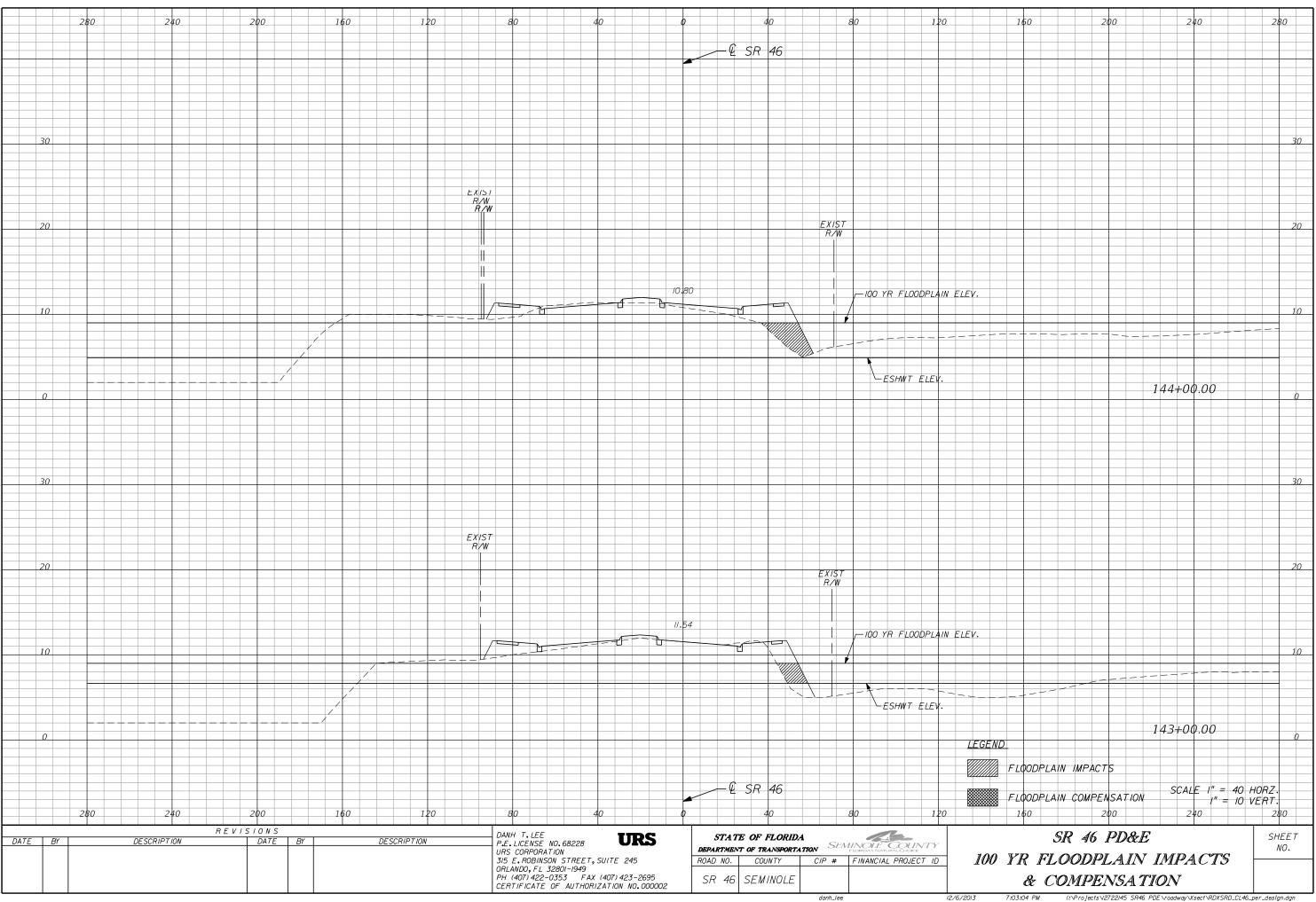
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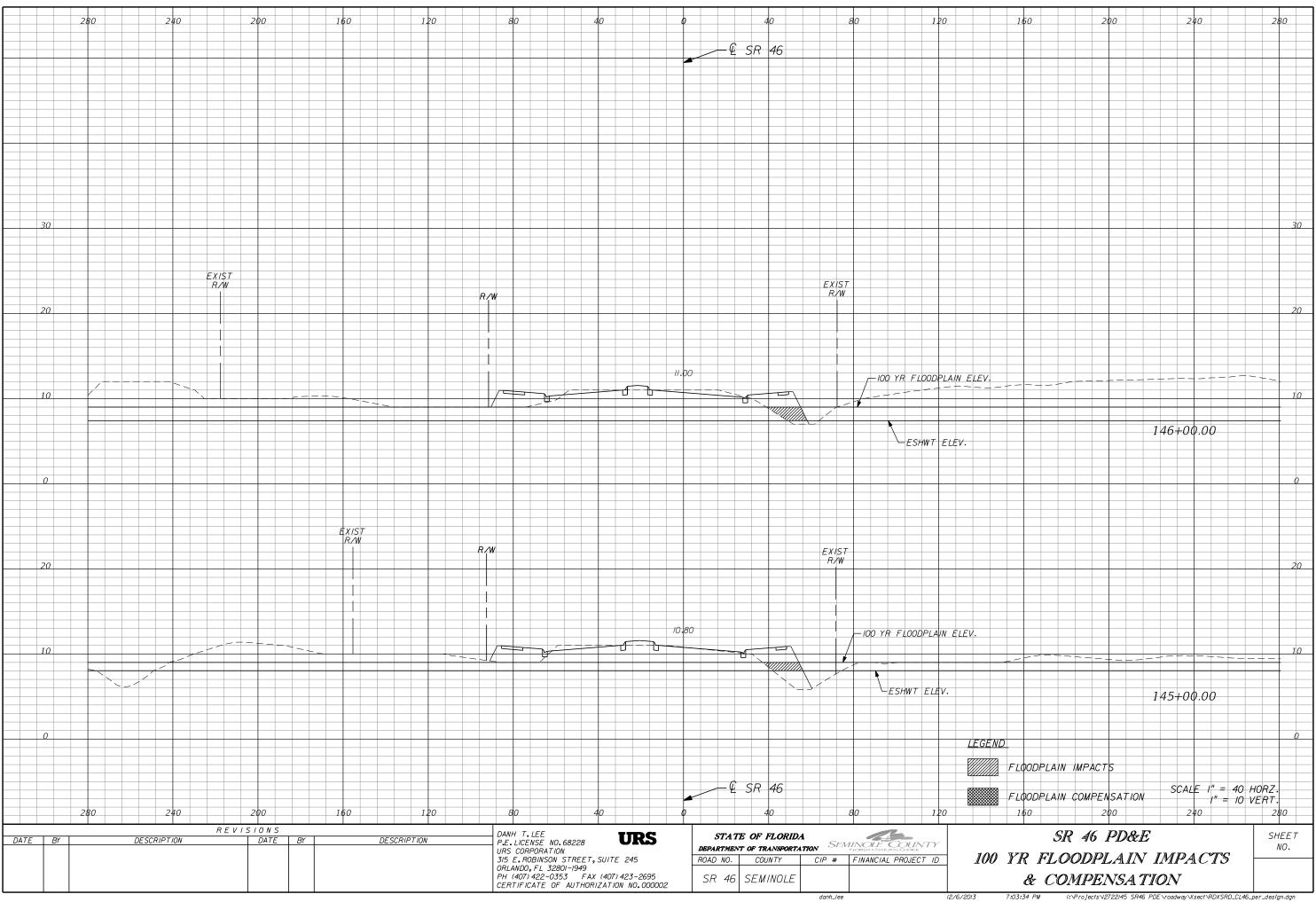


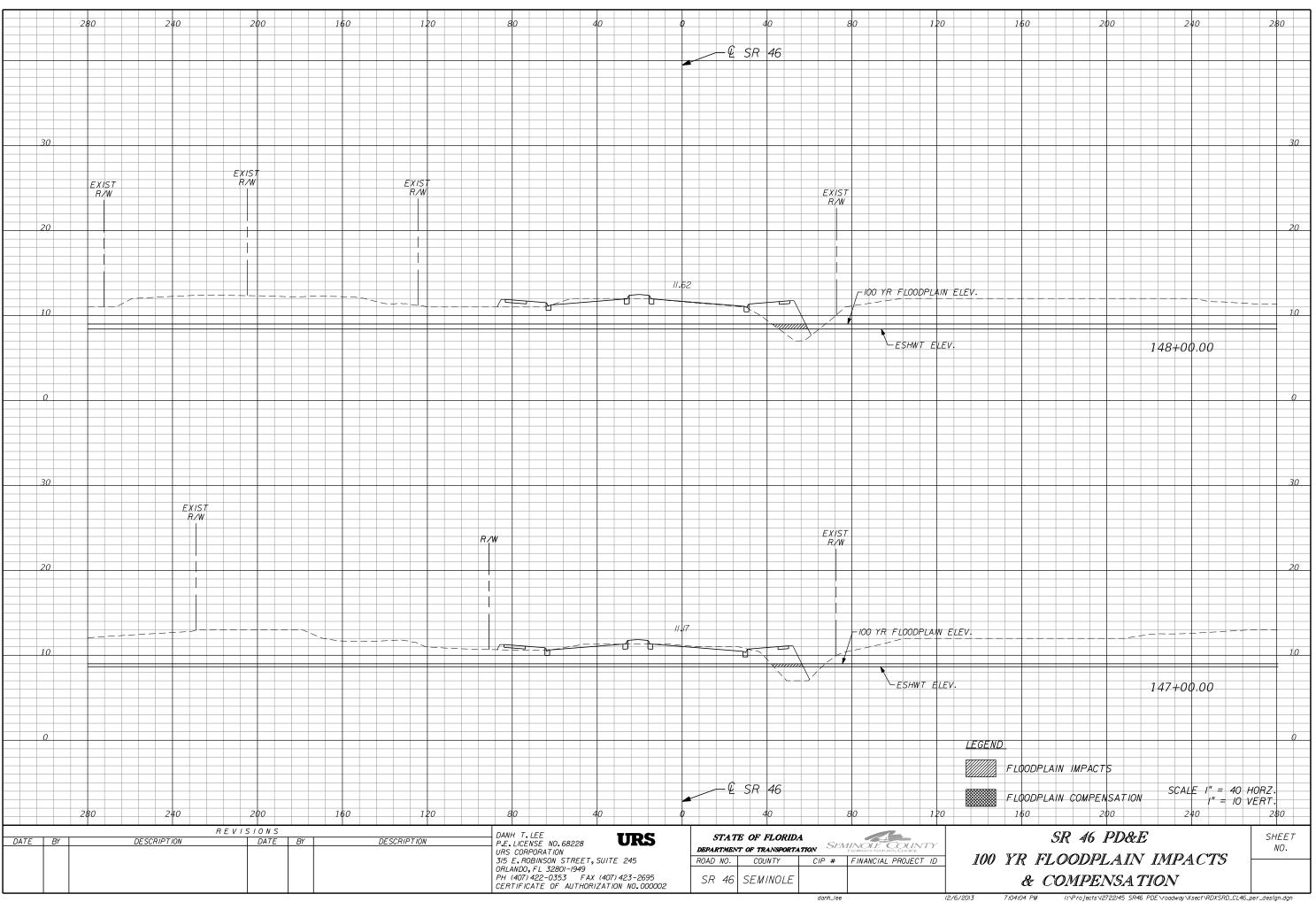
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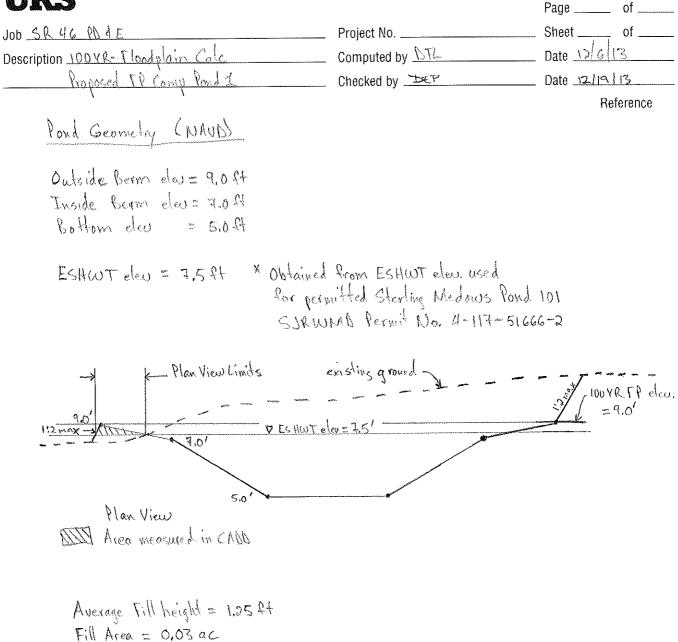




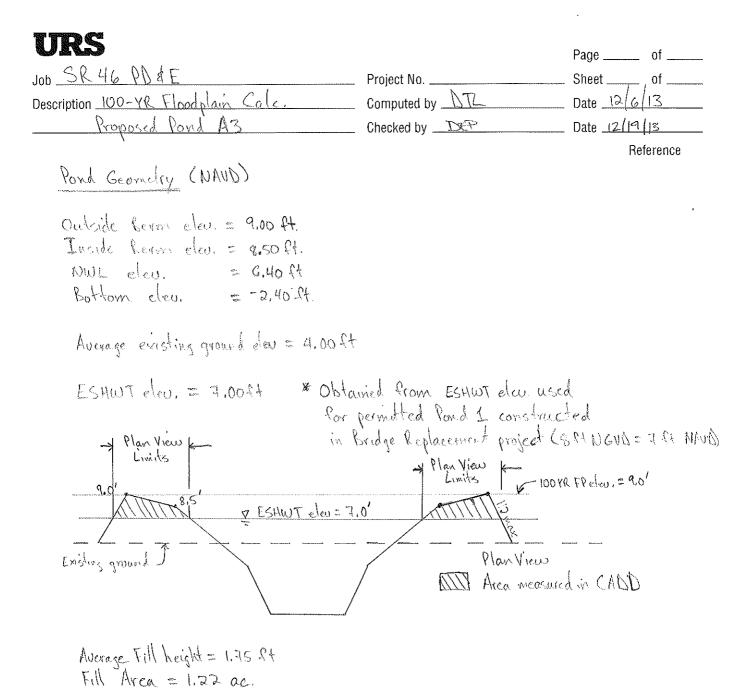




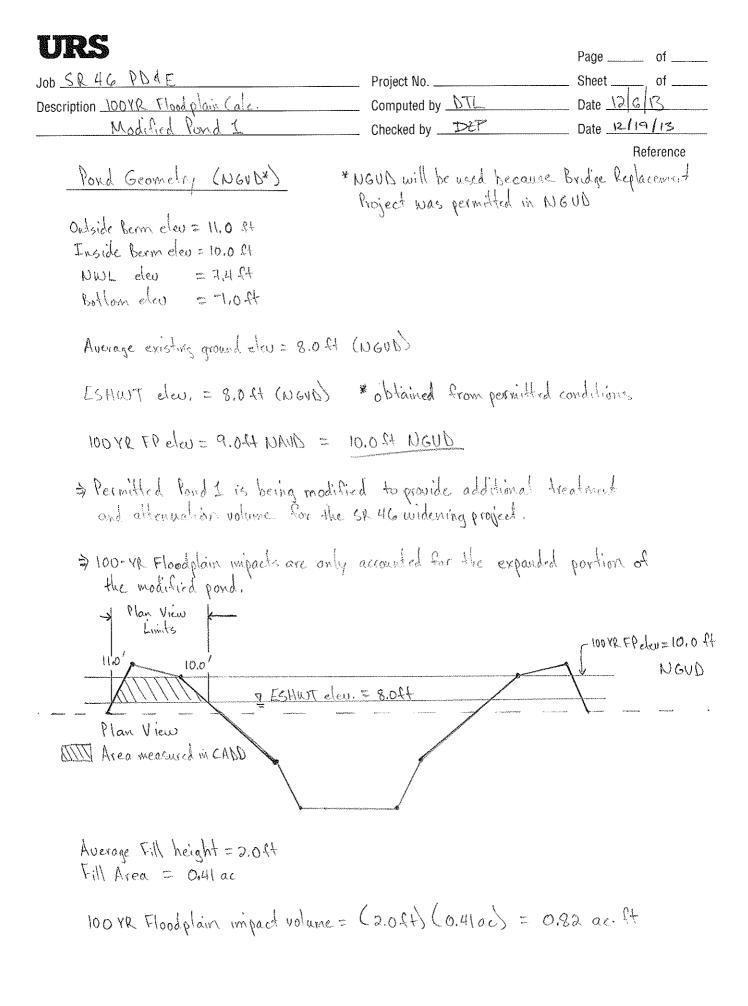




100 VR Floodplain impact volume = (1.25 ff) (0.03ac) = 0.04 ac-ff



100 VR Floodplain impact volume = (1.75 ft)(1.2200) = 2.14 ac-ft



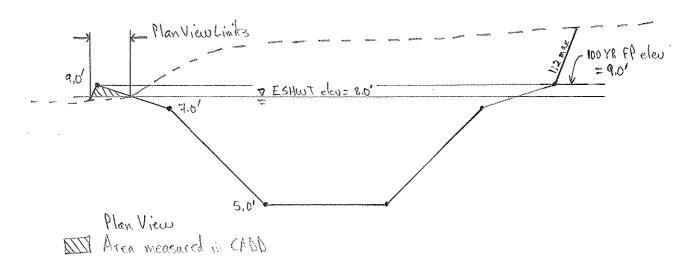


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|--------------------------------------|-----------------|---------------|
| JOB SRUG PDEE | Project No. | Sheet of |
| Description 100 VR - Floodplain Calc | Computed by DTL | Date 12/6/13 |
| Proposed FP Comp Porda | Checked by | Date 12/19/13 |
| \ \ | | |

Pond Geometry (NAUD)

Outside Bermeleu = 9.0 ft Inside Bermeleu = 7.0 ft Bothom eleu = 5.0 ft Reference

Consentative estimate of ESHENT being 1 ft below 100 YR Floodplain elevation.



Average Fill height = 0.75 ft Fill Area = 0.10 ac

10012 Floodplain impact volume = (0.75ft) (0.10ac) = 0.08ac-ft

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| MADE BY: | DTL | DATE: 11/26/13 | JOB NO. |
| CHECKED BY: | DEP | DATE: 12/19/13 | SHEET NO. |
| CALCULATIONS F | OR: SR 46 PD&E | POND: FP Comp Pond 1 | BASIN: |

Floodplain Compensation Pond 1

Stage Storage Calculations

| ELEV. (ft) | Description | AREA (ac) | AVG AREA (ac) | Delta D (ft) | Delta storage (ac-ft) | Sum Storage (ac-ft) |
|---------------|----------------|--------------|---------------------|--------------------|-----------------------------|---------------------------|
| 9.00 | Out Berm | 7.73 | | | | 11.09 |
| | 100 YR FP Elev | | 7.40 | 1.50 | 11.09 | |
| 7.50 | ESHWT Elev. | 7.06 | | | | |
| 7.00 | Inside Berm | 6.84 | | | | |
| 5.00 | Bottom | 6.41 | · · · · · | | | |

Floodplain compensation will be based on any cut volume between the 100-year floodplain elevation and the ESHWT elevation.

ESHWT elevation based on permitted conditions from Sterling Meadows subdivision Pond 101 (SJRWMD Permit No. 4-117-51666-2).

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| URS | | | |
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| MADE BY: | DTL | DATE: 11/26/13 | JOB NO. |
| CHECKED BY: | DEP | DATE: 12/19/13 | SHEET NO. |
| CALCULATIONS FOR: SR 46 PD | &E | POND: FP Comp Pond 2 | BASIN: |

Floodplain Compensation Pond 2

Stage Storage Calculations

| ELEV. (ft) | Description | AREA (ac) | AVG AREA (ac) | Delta D (ft) | Delta storage (ac-ft) | Sum Storage (ac-ft) |
|---------------|----------------|--------------|---------------------|--------------------|-----------------------------|---------------------------|
| 9.00 | Out Berm | 24.71 | | | | 24.27 |
| | 100 YR FP Elev | | 24.27 | 1.00 | 24.27 | |
| 8.00 | ESHWT Elev. | 23.83 | | | | |
| 7.00 | Inside Berm | 22.97 | | | | |
| 5.00 | Bottom | 22.11 | | s | | |

Floodplain compensation will be based on any cut volume between the 100-year floodplain elevation and the ESHWT elevation.

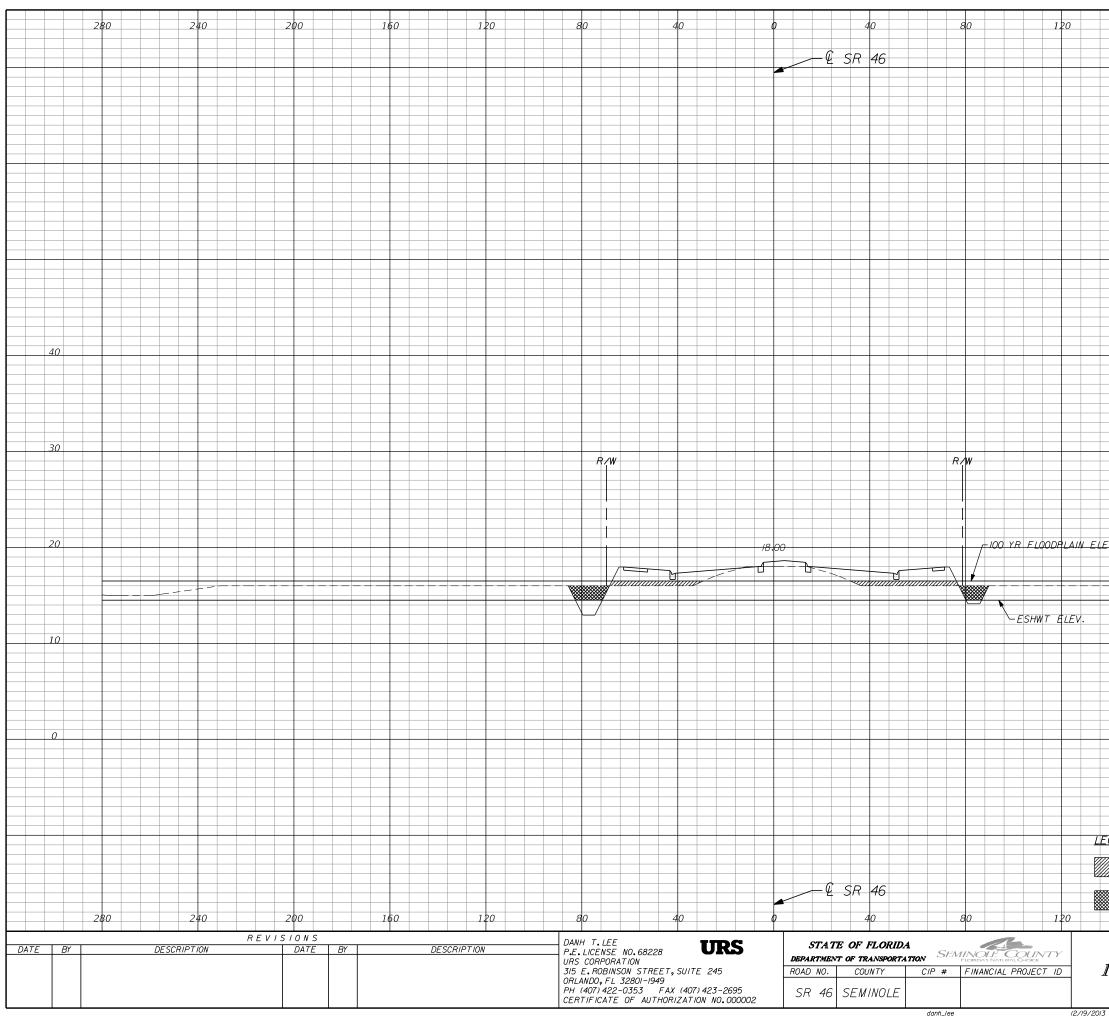
Conservative estimate of ESHWT elevation being 1 ft below 100 year floodplain elevation.

Maint. Berm Maint. Berm Existing Grnd 1:8 1:8 1:4 1:4

| URS MADE BY: CHECKED BY: CALCULATIONS FOR: | DTL DEP SR 46 PD&E Floodplai | DATE: DATE: n Impacts/Compensation | 11/26/13 12/19/13 | JOB NO. SHEET NO. |
|---|---|---|---|---|
| Roadway Cross-Section Station: | Floodplain Impact (Fill) Area (ft ²): | Floodplain Compensation (Cut) Area (ft ²): | Floodplain Impact Net Volume (ft ³): | Floodplain Compensation Net Volume (ft ³): |
| | | Center Line for SR 46 Widenii | ng | |
| 198+00 | 18.21 | 21.36 | - | |
| 199+00 | 24.55 | 20.76 | 2,137.63 | 2,105.50 |
| 200+00 | 25.69 | 22.24 | 2,511.50 | 2,149.88 |
| 201+00 | 32.08 | 22.84 | 2,888.25 | 2,254.13 |
| 202+00 | 18.70 | 29.30 | 2,538.88 | 2,606.88 |
| 203+00 | 17.30 | 24.07 | 1,799.63 | 2,668.25 |
| 204+00 | 3.79 | 20.07 | 1,054.13 | 2,206.75 |
| 205+00 | 35.06 | 19.48 | 1,942.38 | 1,977.50 |
| 206+00 | 42.80 | 22.48 | 3,893.13 | 2,097.88 |
| 207+00 | 40.24 | 24.68 | 4,152.00 | 2,357.63 |
| 208+00 | 9.27 | 23.92 | 2,475.50 | 2,429.88 |
| 209+00 | 16.72 | 23.42 | 1,299.75 | 2,367.00 |
| 210+00 | 15.68 | 23.42 | 1,620.13 | 2,342.00 |
| 211+00 | 21.21 | 28.41 | 1,844.25 | 2,591.38 |

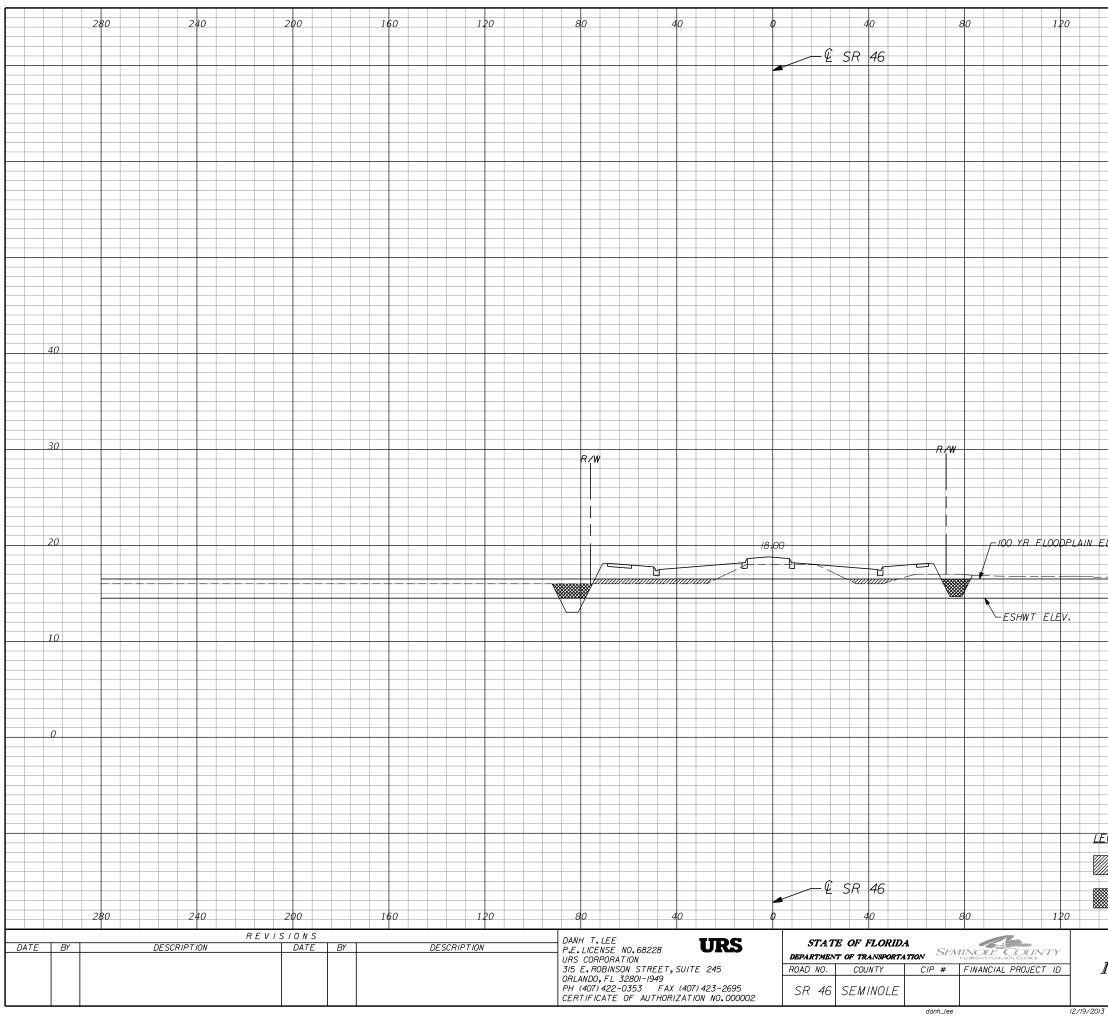
| terline SR 46 Widening - Station 198+00 to 211+00 LT | | |
|--|------|------|
| TOTAL (ac-ft): | 0.69 | 0.69 |

| MADE BY: CHECKED BY: CALCULATIONS FOR: | DTL DFP SR 46 PD&E Floodpla | DATE: DATE: in Impacts/Compensation | 11/26/13 | JOB NO. SHEET NO. |
|--|---|--|--|--|
| Roadway Cross-Section Station: | Floodplain Impact (Fill) Area (ft ²): | Floodplain Compensation (Cut) Area (ft ²): | Floodplain Impact Net Volume (ft ³): | Floodplain Compensation Net Volume (ft ³): |
| | | Center Line for SR 46 Widenin | ng | |
| 198+00 199+00 200+00 201+00 202+00 203+00 204+00 205+00 206+00 207+00 | 21.25 8.14 6.95 9.63 8.58 8.92 10.16 10.43 6.87 7.58 | 14.28 15.87 18.18 18.96 18.20 18.79 0.00 0.00 0.00 0.00 0.00 | 1,469.38 754.25 829.13 910.50 874.63 953.88 1,029.38 864.88 722.38 | 1,507.75 $1,702.50$ $1,856.63$ $1,857.50$ $1,849.00$ 939.25 0.00 0.00 0.00 |
| Centerline SR 4 | Summary 6 Widening - Station 19 | of Floodplain No. 3 Impact 98+00 to 207+00 RT | Volumes for SR 46 | Widening: |
| | | TOTAL (ac-ft): | 0.19 | 0.22 |



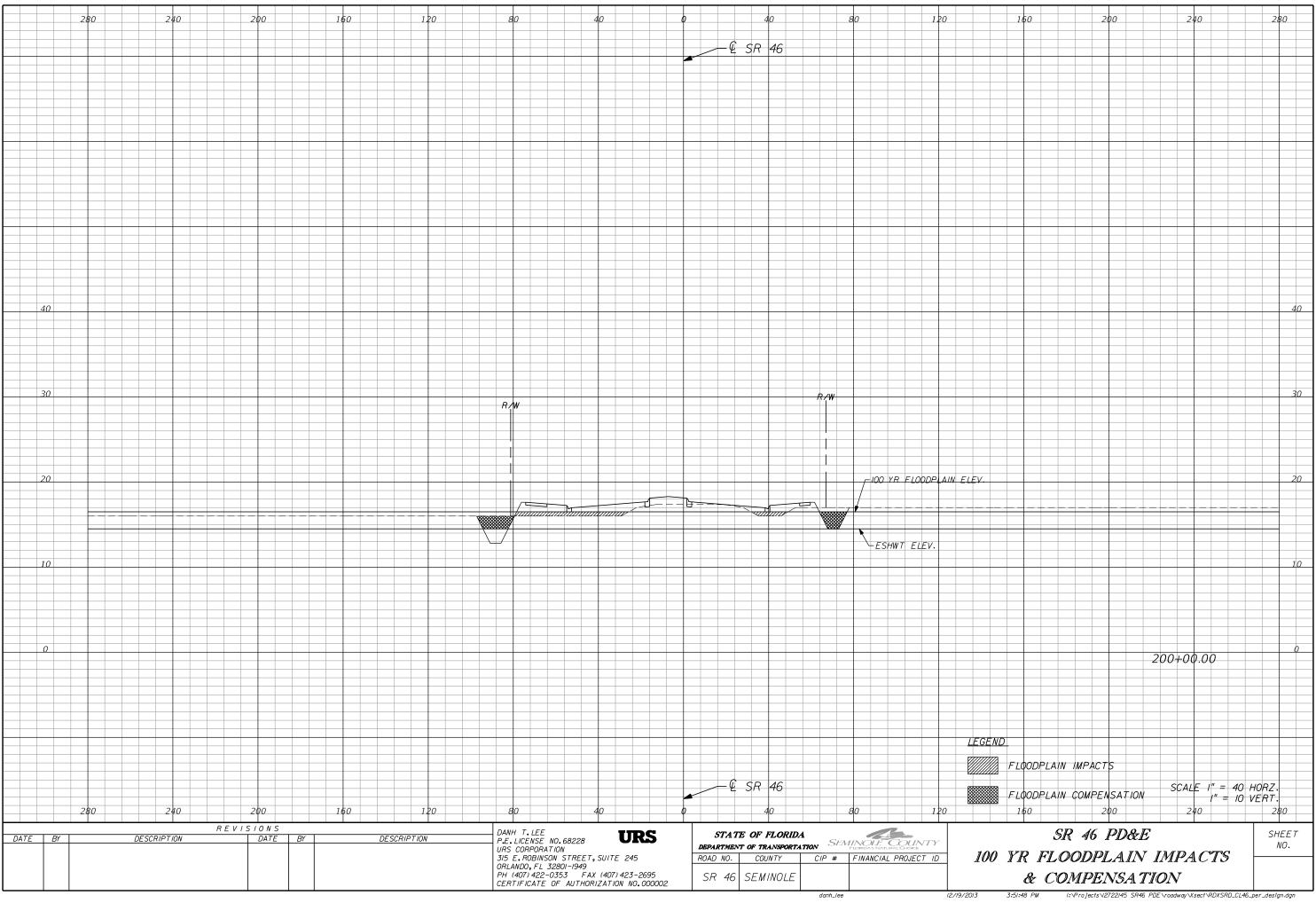
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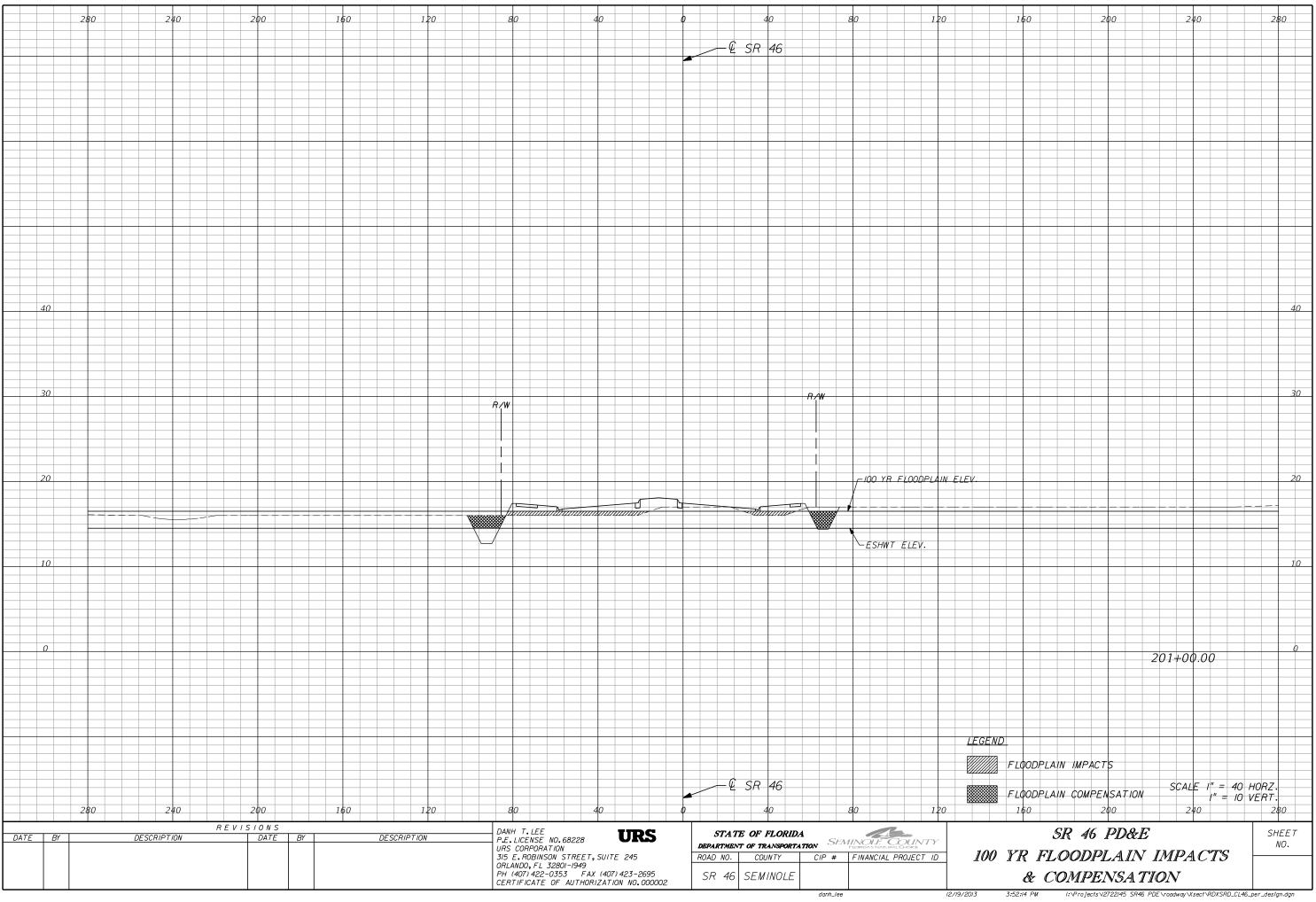
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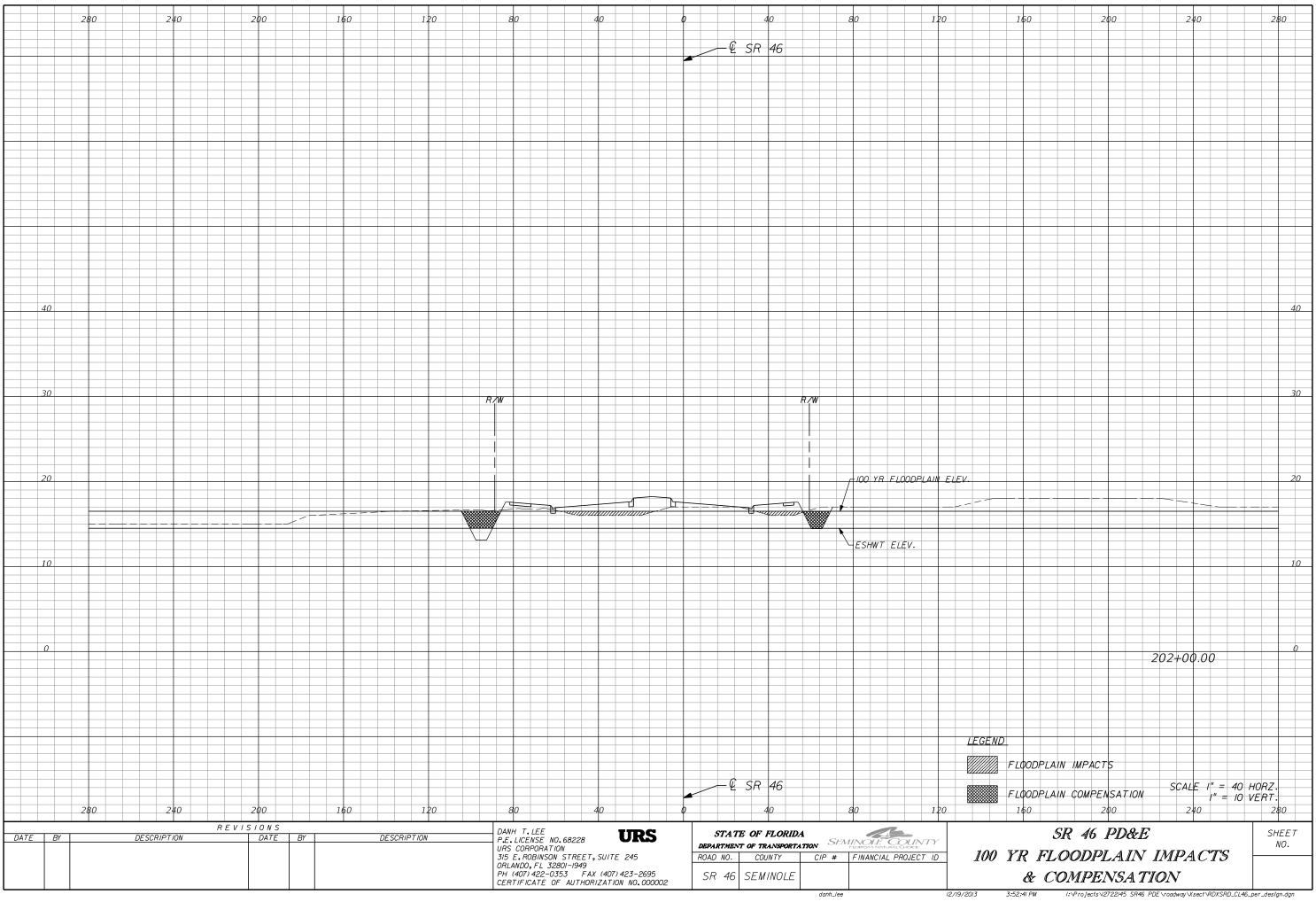


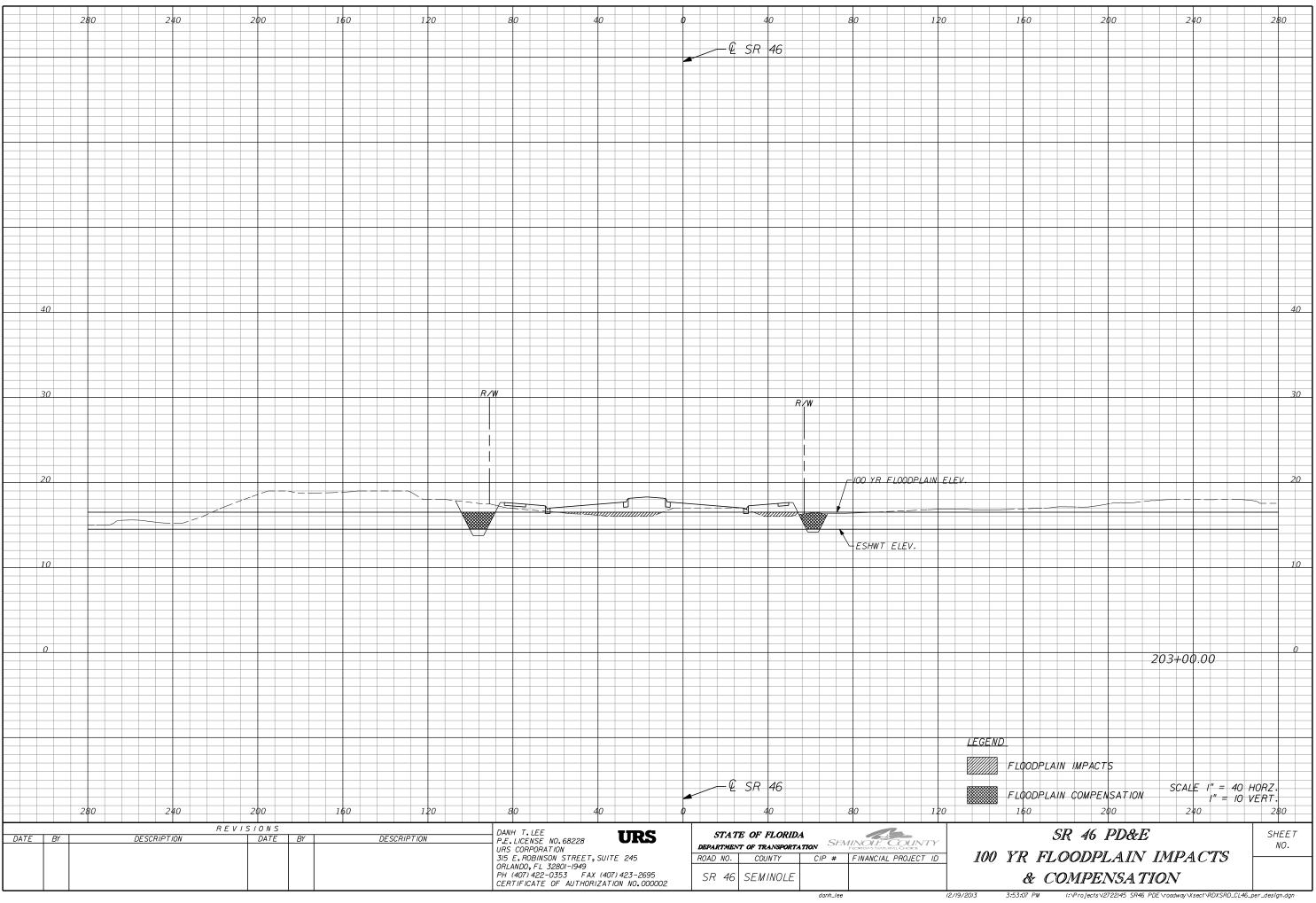
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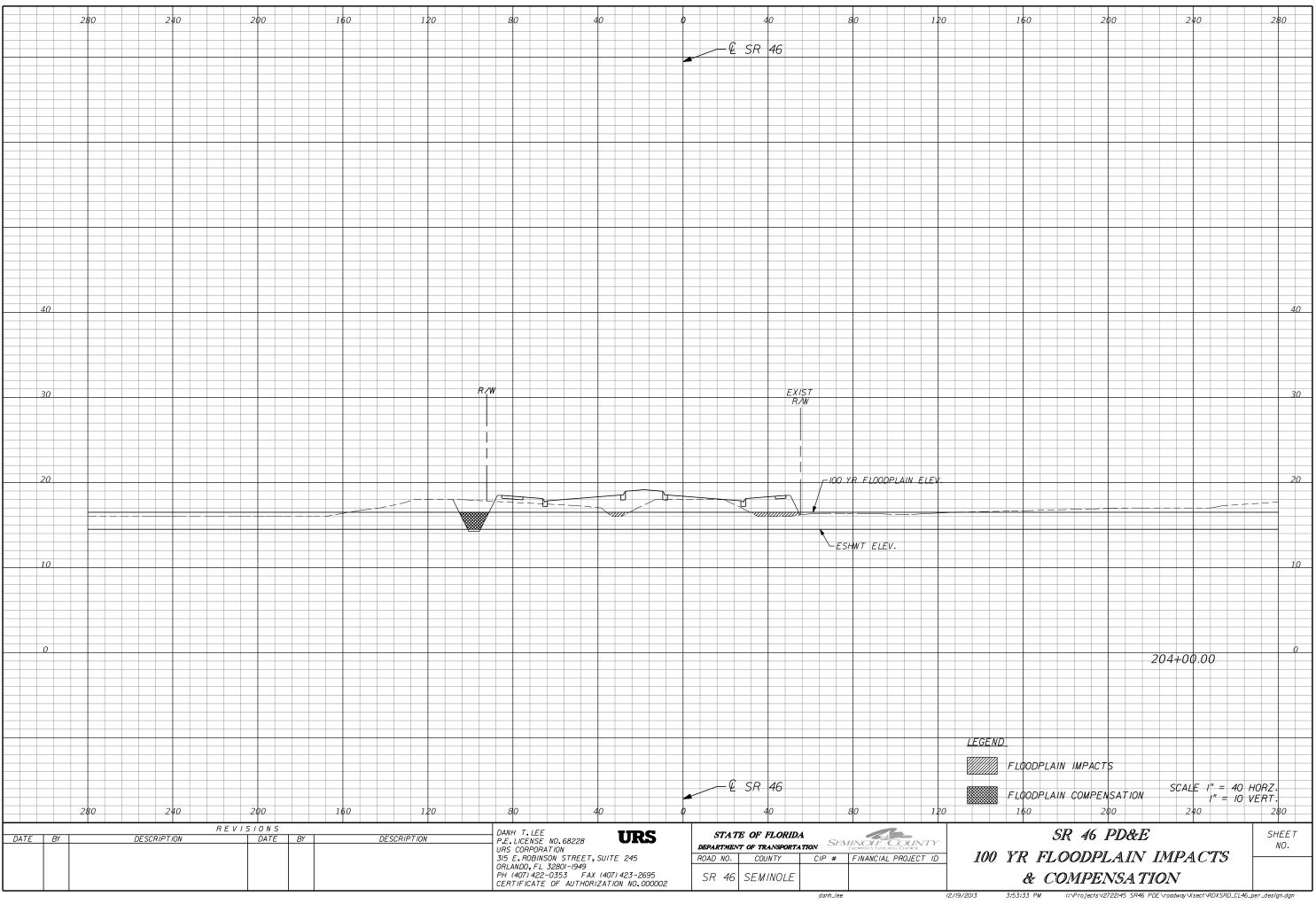
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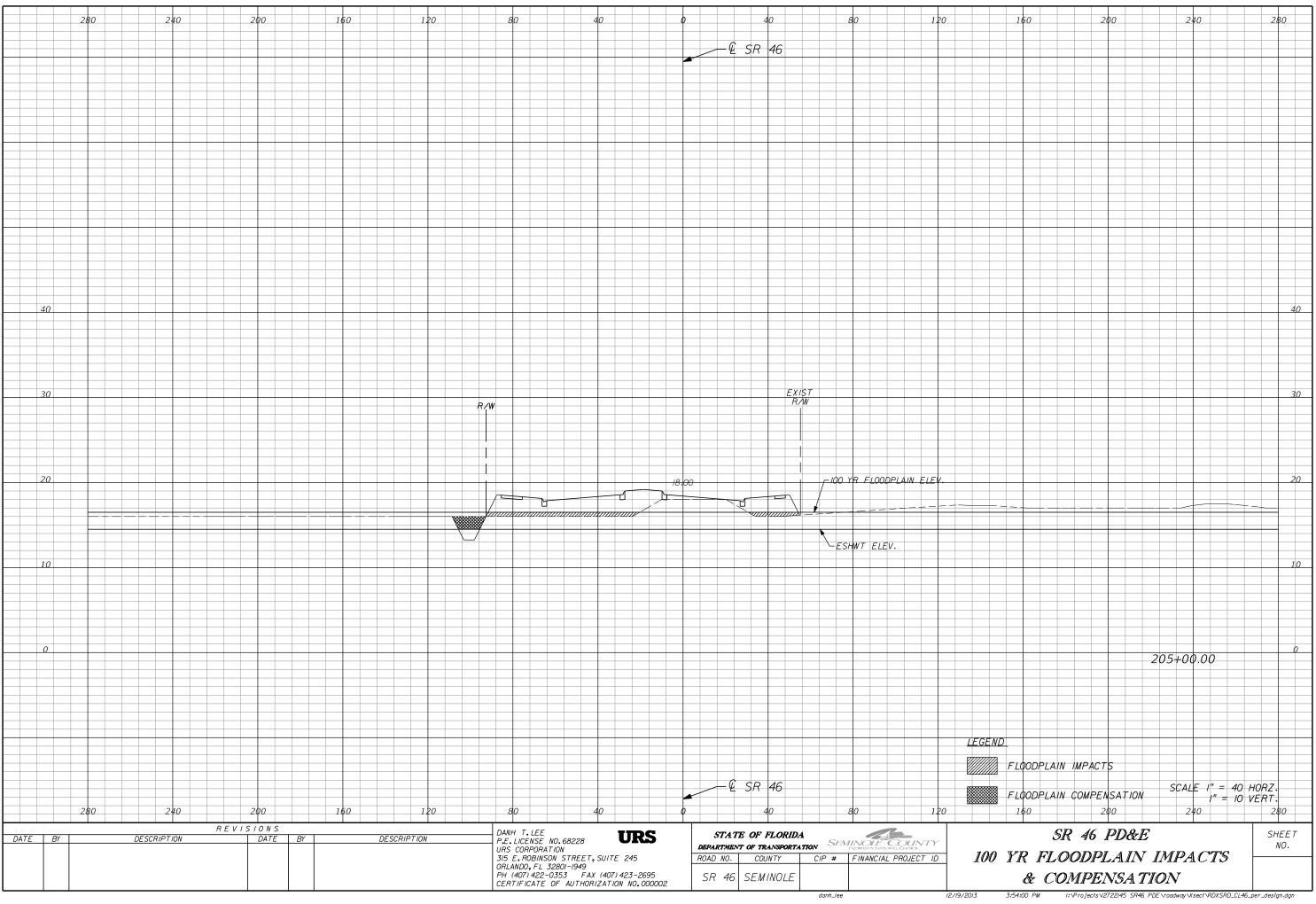


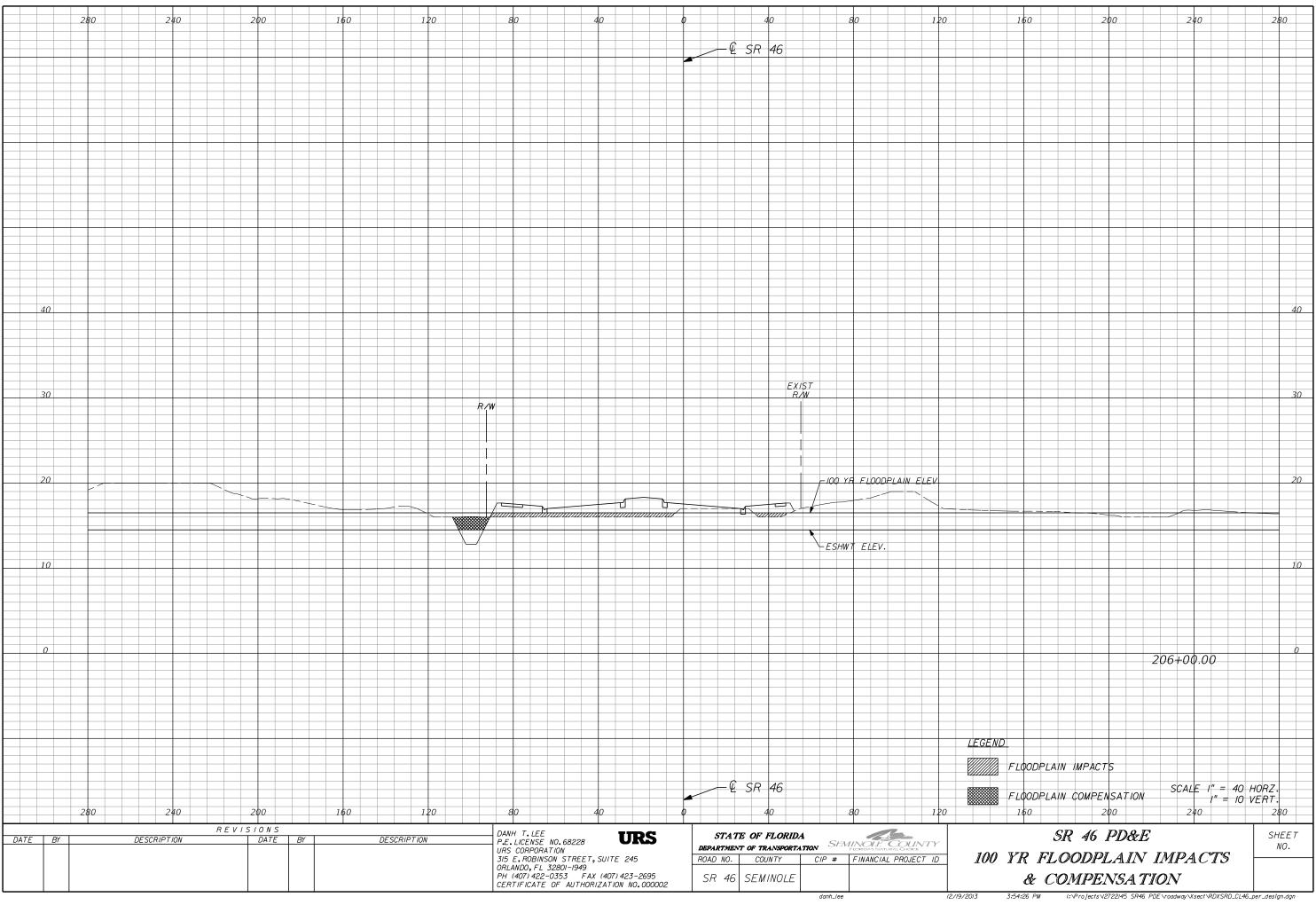


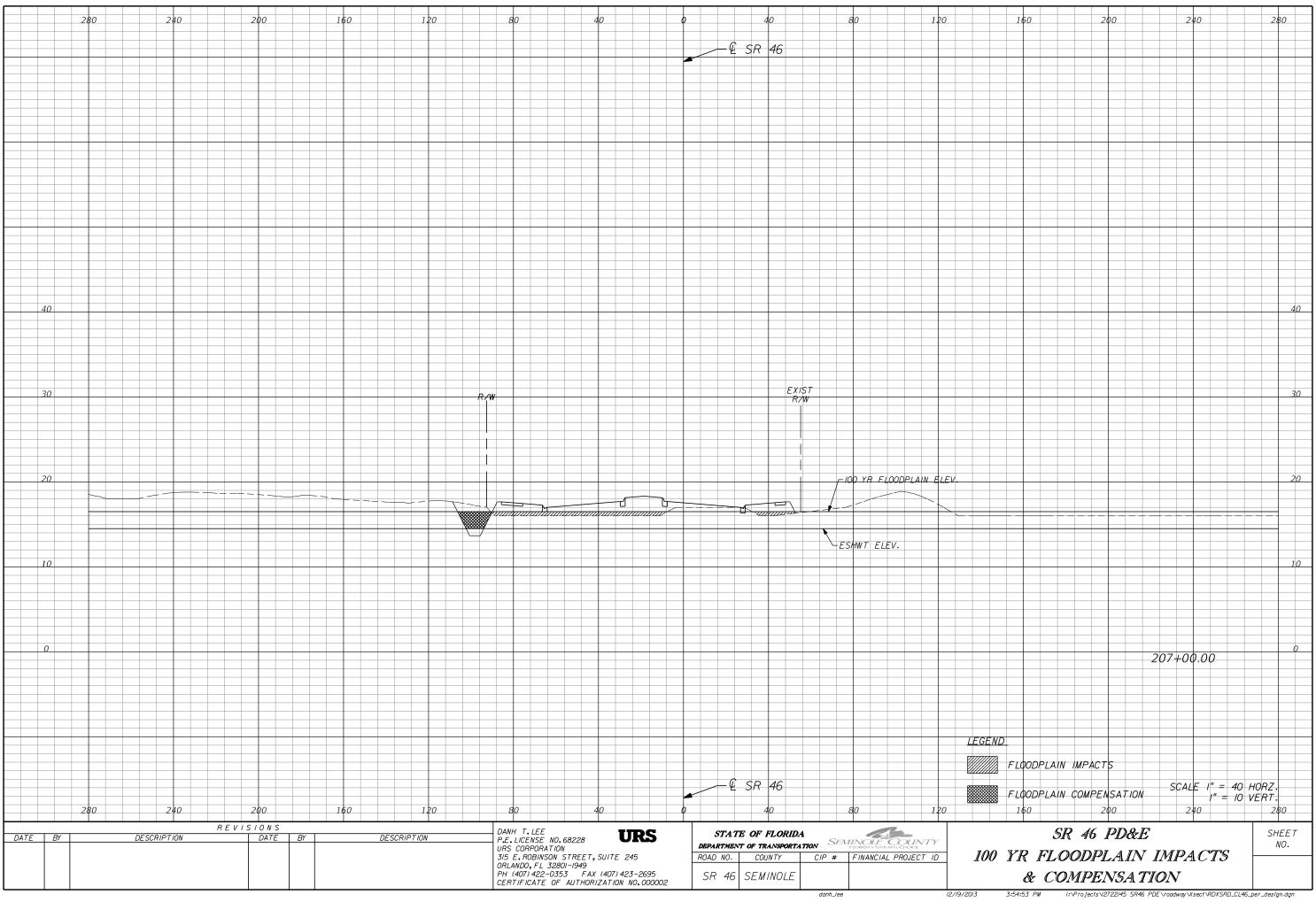


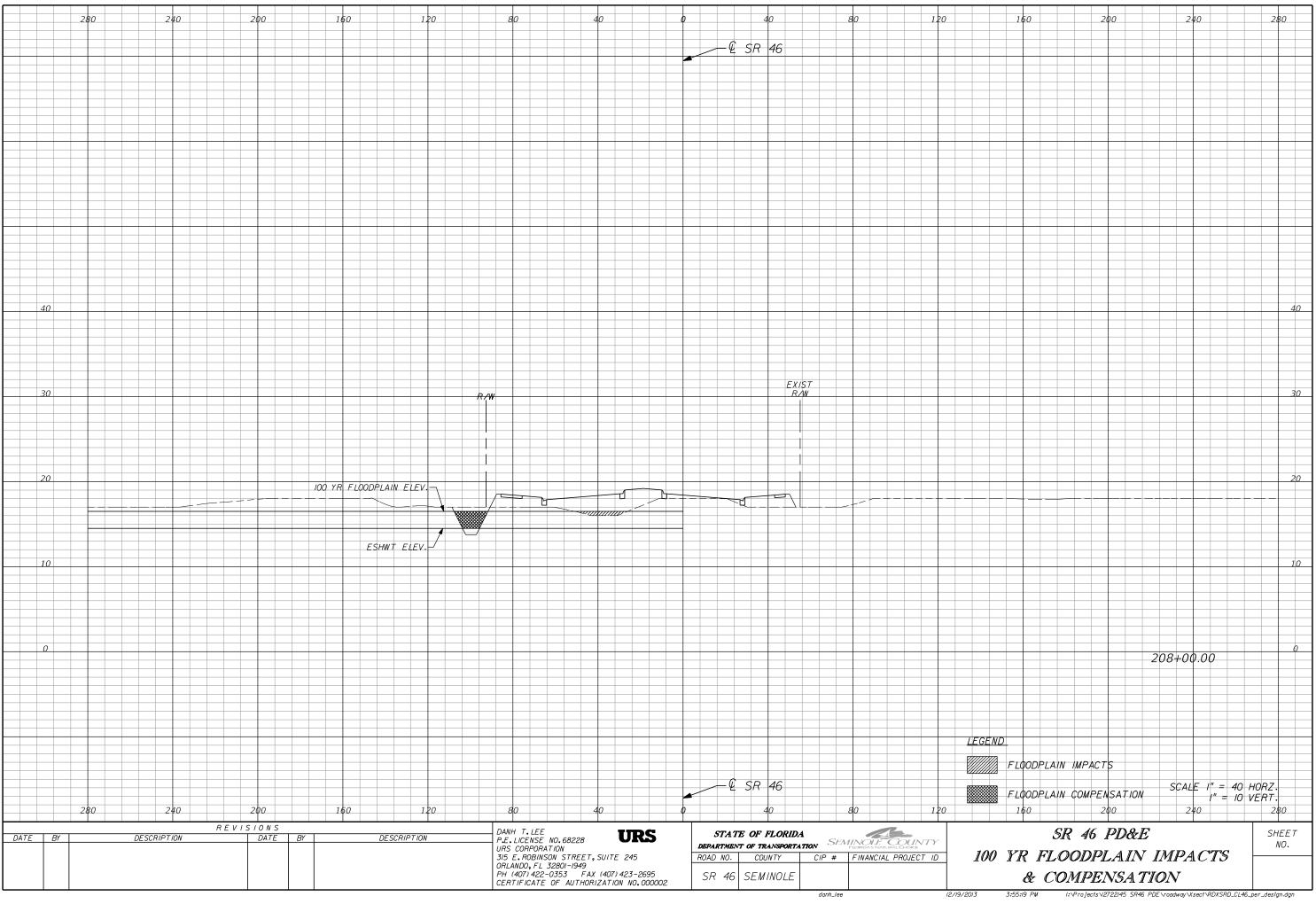


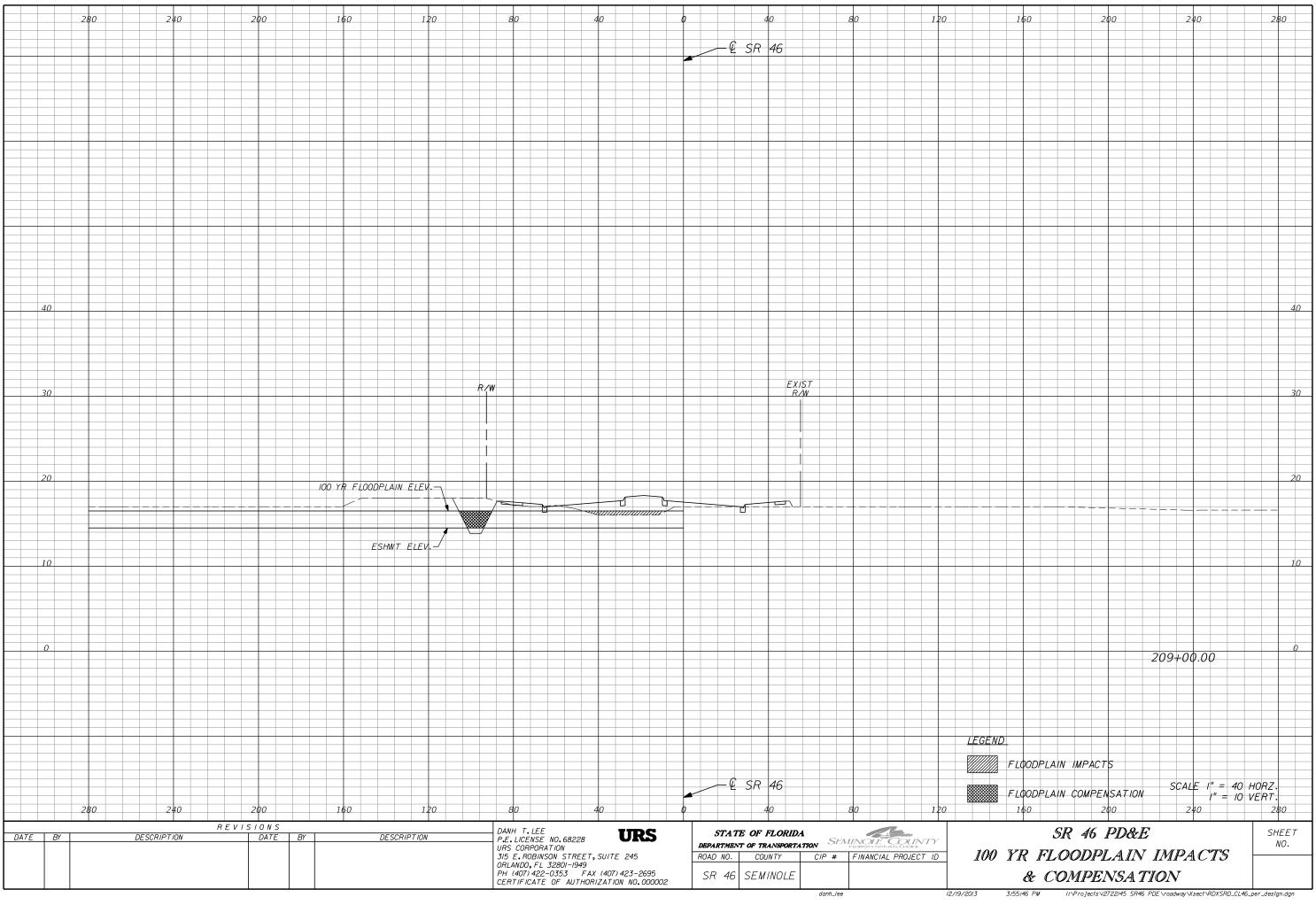


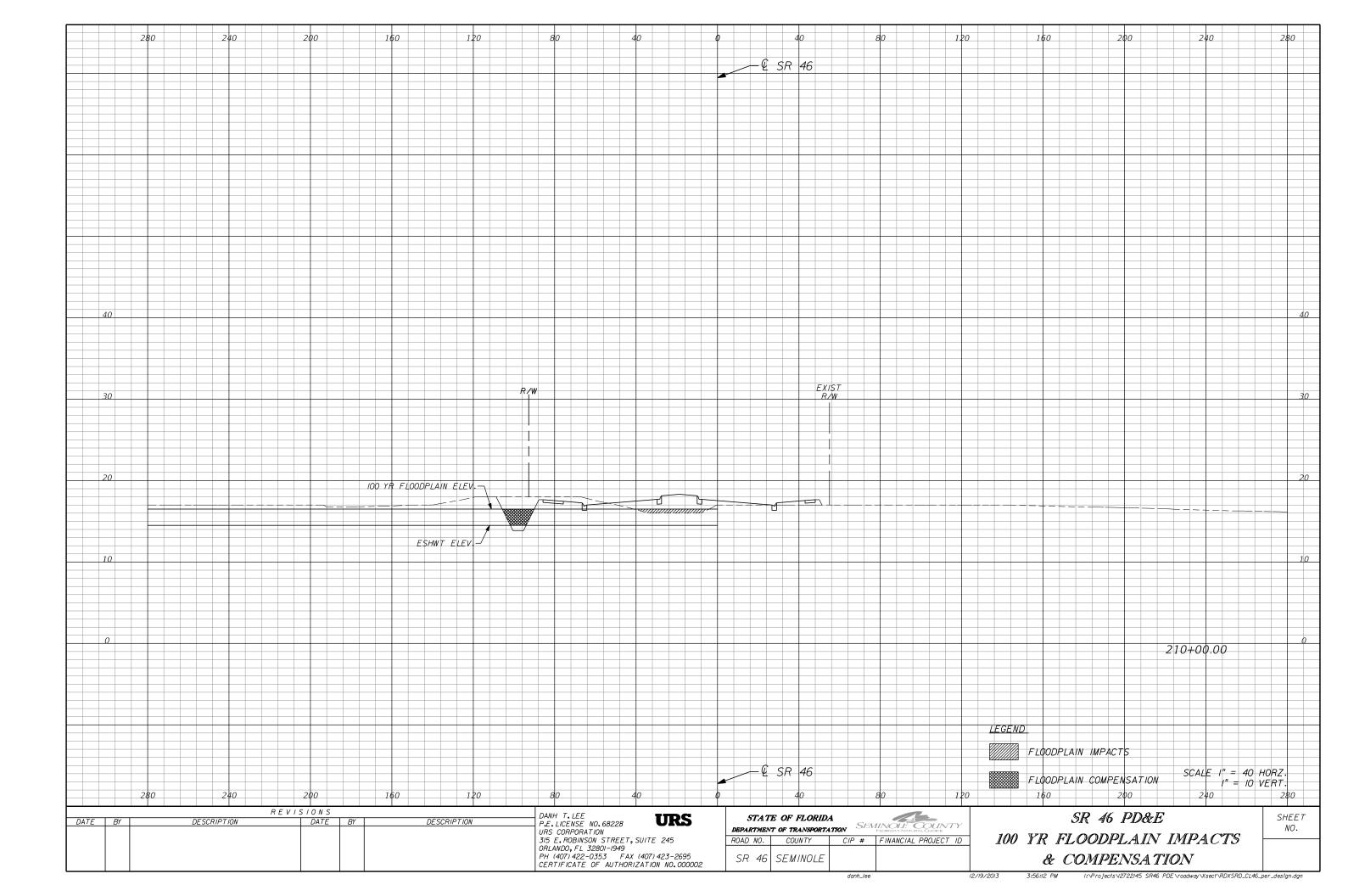


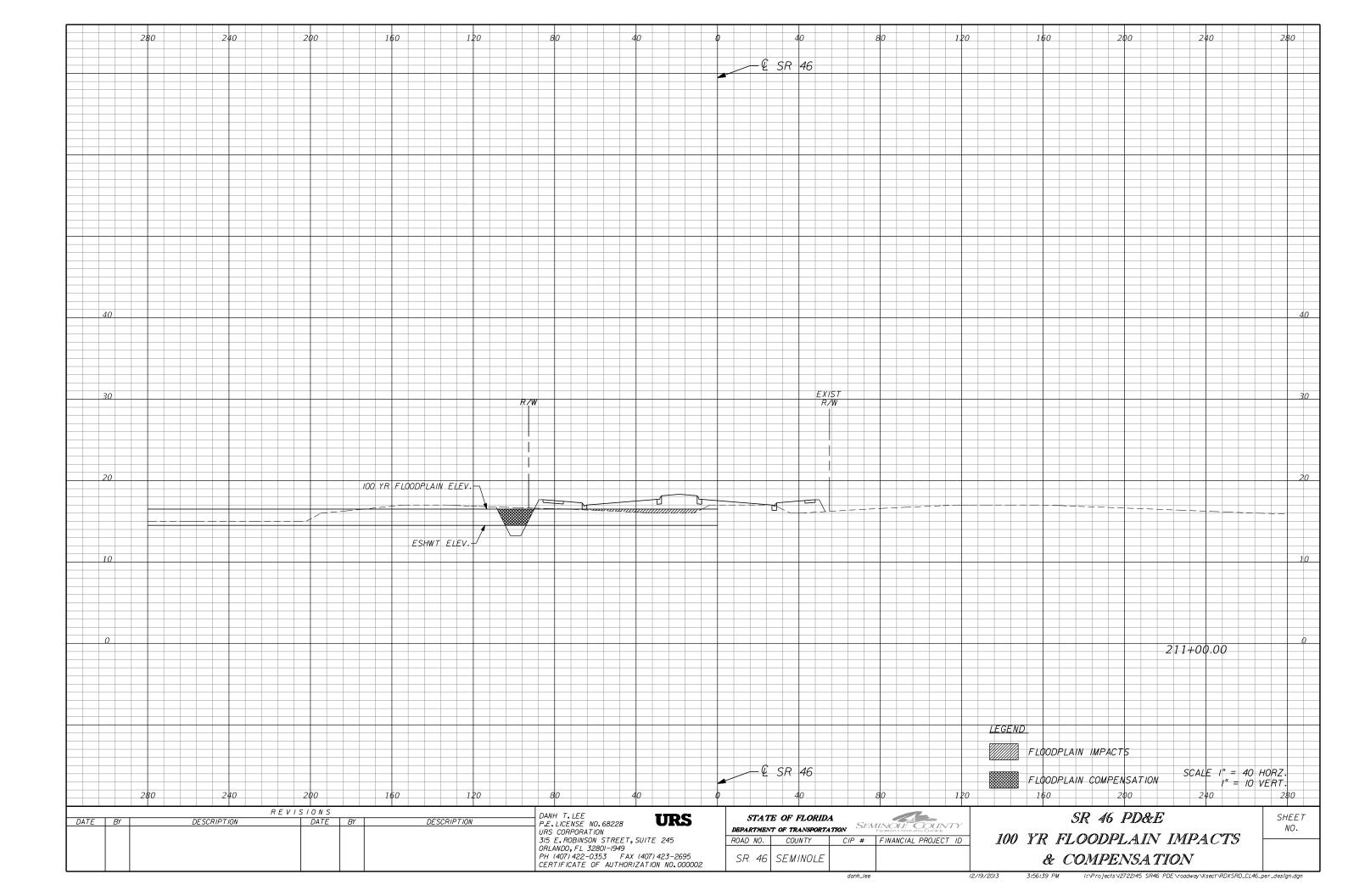












APPENDIX F Correspondence

SR 46 PD&E LOCATION HYDRAULICS REPORT

URS Corporation

RECORD OF CONVERSATION

| DATE: Feb. 7, 2012 | JOB #: <u>12721027</u> |
|-------------------------------|--------------------------------------|
| RECORDED BY: DTL FDOT | CLIENT: <u>Seminole County &</u> |
| TALKED WITH: Jim Wood | OF: FDOT Maintenance |
| NATURE OF CALL: Incoming | Outgoing 🖂 Meeting 🗌 |
| ROUTE TO: | |
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| MAIN SUBJECT OF CONVERSATION: | Drainage issues and base clearance |

Danh Lee spoke with Jim Wood of FDOT Maintenance about any possible drainage concerns within the project corridor. The first item of concern, Jim mentioned, deals with an existing cross drain (CD-5 at mile post 7.97) and the fact that there is not positive drainage at the outfall. However, the outfall drains into private property and thus has not been fixed. Jim believes that the problem exist due to the grading or lack thereof, within the private property.

The only other concern is in the area of Mullet Lake Park Road. The east side of the roadway, north of SR 46 sometimes floods. FDOT has received calls in the past regarding flooding in this area. However, since the flooding occurs outside of FDOT right of way, there is not much they can do to fix the problem. Jim believes that flooding happens due to the ultimate outfall and the conveyance system(s) leading into St. Johns River. Specifically, the water is backing up into private property due to not having positive drainage / adequate grading required within certain private properties. Also, the conveyance systems may be undersized to handle the required flow capacities which would allow for the runoff to be maintained within the appropriate limits.

The discussion continued about field observations that were made on 2/2/12. During the field visit, I noticed that two (2) endwalls for the existing cross drains

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were buried. The endwall for CD-7, on the south side of the roadway was completely buried. The top of the endwall for CD-8, on the north side was only visible and the 24" RCP was completely underground. Jim stated that no problems existed in these areas and that the maintenance crew would be sent out soon to uncover the endwalls during this current dry season.

The next item of discussion was base clearance. I asked Jim if there were any issues regarding base clearance and / or any problems with deterioration of the existing road surface. Jim stated that there were no issues that he could recall. He did state that the road surface within the project corridor was recently milled and re-surfaced so no problems are currently visible. However, he stated that before the milling and re-surfacing project, there were some areas that had "alligator" cracking.